Concrete Incorporated with Recycled HDPE

Subjects: Polymer Science Contributor: Chamila Gunasekara

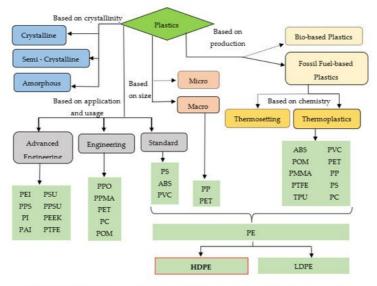
Incorporating recycled plastic waste in concrete manufacturing is one of the most ecologically and economically sustainable solutions for the rapid trends of annual plastic disposal and natural resource depletion worldwide. This paper comprehensively reviews the literature on engineering performance of recycled high-density polyethylene (HDPE) incorporated in concrete in the forms of aggregates or fiber or cementitious material. Optimum 28-days' compressive and flexural strength of HDPE fine aggregate concrete is observed at HDPE-10 and splitting tensile strength at HDPE-5 whereas for HDPE coarse aggregate concrete, within the range of 10% to 15% of HDPE incorporation and at HDPE-15, respectively. Similarly, 28-days' flexural and splitting tensile strength of HDPE fiber reinforced concrete is increased to an optimum of 4.9 MPa at HDPE-3 and 4.4 MPa at HDPE-3.5, respectively, and higher than the standard/plain concrete matrix (HDPE-0) in all HDPE inclusion levels. Hydrophobicity, smooth surface texture and non-reactivity of HDPE has resulted in weaker bonds between concrete matrix and HDPE and thereby reducing both mechanical and durability performances of HDPE concrete with the increase of HDPE.

Keywords: sustainability; recycled plastic; high-density polyethylene (HDPE); concrete; construction material

1. Introduction

About 2.01 billion tons of Municipal Solid Waste (MSW) is generated annually worldwide, and one third of MSW is openly dumped without managing in an environmentally-friendly manner [1]. Around 40% of MSW is discharged directly to landfills, 19% of it is recovered through recycling or composting and another 11% of it is incinerated [1]. With the rapid trends of urbanization, it has been predicted that 3.40 billion tons of MSW will be generated by 2050 [1]. About 12% of MSW generated are plastics, which is approximately 24.14 million tons [1]. The plastic industry began in the early 1900s in the USA [2]. During the period of 1950 to 2015, 8.3 billion tons of plastics were manufactured worldwide and 6.3 billion tons of them were discharged as waste [3]. Only 9% of plastic waste had been recycled, 12% were incinerated and the majority of 79% was discharged into landfills or openly dumped [3]. China ranks at the top in plastic manufacturing followed by Europe which accounts for 30% and 19%, respectively. Furthermore, China tops even in plastic consumption followed by Western Europe which is around 20% and 18%, respectively [4]. Plastic is one of the vastly discharged wastes to the environment which has adversely affected the wildlife, their habitats, and humans continuously over the past few decades. This emphasizes that it is high time to rethink the necessity of plastic recycling and reusing.

Today, more than 30 types of primary plastics and over thousands of different secondary plastics can be found, produced by using different combinations and proportions of primary plastics $^{[\underline{5}]}$. Plastics can also be categorized based on many aspects as illustrated in $^{[\underline{4}][\underline{5}]}$. Different plastics have different characteristics such as mechanical properties, durability resistances and diverse applications based on their compositions and chemical structures. The most commonly manufactured and applied plastics in the world are polyethylene (PE), polypropylene (PP), polyvinyl chloride (PVC), polyethylene terephthalate (PET) and polystyrene (PS) which represents 69% of the global plastic consumption $^{[\underline{4}]}$. Out of global plastic production, the polypropylene (PP) and low-density polyethylene (LDPE) account for 17% and 16%, respectively, followed by high-density polyethylene (HDPE) (13%) and polyphthalamide (PP&A) (13%). In addition, additives used in plastic products' manufacturing also have a significant share in global plastic production (6%) $^{[\underline{4}]}$. Moreover, the use of combustible claddings in high-rises significantly increase the risk of fire spread via the external façades $^{[\underline{6}]}$. Urgent work on the removal of polyethylene-based claddings is necessary to ensure the safety of the occupants and buildings but also accounts for a substantial amount of PE sent to landfill.



PEI- Polyetherimide; PPS- Polyphenylene Sulfide, PI- Polymid, PAI- Polyamide-imide, PBI- Polybenzimidazole, PSUPolysulfore, PPSU-Polyphenylsulfore, PEEK-Polyetheretherketone, PTFE-Fluoropolymer/Tedon, PPO-Polyphenylene Oxide,
PPMA- Polymethyl Methacrylate, PET- Polyethylene Terephthalate, PC- Polycarbanate, POM- Polyoxymethylene, PAPolyamide/ Nylon, PS- Polystyrene, PVC- Polyvinyl Chloride, PP- Polypropylene, ABS- Acryloritrile- Butadiene- Styrene,
PMMA- Acrylics / Polymethyl-methacrylate, TPU- Thermoplastic polyurethane, PE- Polyethelene, HDPE- High Density
Polyethelene, LDPE-Low Density Polyethelene

Figure 1. Plastic categorization.

Concrete is ranked as the topmost man-made resource utilized in the construction industry worldwide. The global aggregate requirement for concrete production accounts for about 4.5 billion tons per year which alarms the necessity of finding alternative aggregate sources required for increasing trends of concrete production ^[Z]. Incorporating recycled plastic waste in concrete production is a sustainable approach for both disposing of plastic waste and aggregate scarcity, due to its economic and ecological advantages. Concrete composites replace various types of recycled plastics in the forms of aggregate, binder, filler or fiber reinforcement in different proportions where concrete properties are optimized ^[8]. PP, PET and HDPE are the most used plastics in the construction industry. However, the application and research studies on HDPE being used with concrete is very minimal compared with PP and PET.

HDPE is a thermoplastic synthetic polymer in the subset of the PE macro plastic group. PE polymer consists of neverlasting hydrocarbon chains where each carbon molecule is bound to another two carbon molecules and two hydrogen molecules. HDPE has minimal branches in its polymer chain which results to pack liner molecular chains together regularly during crystallization. As a result, semi-crystalline HDPE polymers become much more dense, rigid, and ductile with a comparatively strong bending strength between 20 to 45 MPa due to the regular packing of polymer chains [3][4][5]. HDPE also has a low density between 950 to 970 kg/m3, a better flexibility, and a high tensile strength between 20 to 32 MPa [3][4][5]. Further, HDPE is a chemically inert [3][4][5] material and its melting point is at 130 °C while ignition temperature is at 487 °C [9].

2. Use of HDPE as an Aggregate in Concrete

2.1. Mechanical Properties of HDPE Fine Aggregate Concrete

Throughout the paper, HDPE incorporated concrete is denoted in an abbreviation form, such as 10% of HDPE inclusion as HDPE-10 and 100% of HDPE inclusion as HDPE-100, etc. <u>Table 1</u> and <u>Table 2</u> summarizes the mechanical performances of HDPE fine aggregate concrete. It was observed that the slump (workability) is decreased from 70 mm to 30 mm when HDPE is increased from 5% to 15% while keeping the w/c ratio a constant of 0.42 ^[10]. In another experiment, a constant slump of 90 mm is observed with the increase of w/c ratio as 0.45 for HDPE-0, 0.50 for HDPE-25 and HDPE-50, 0.55 for HDPE-75 and 0.6 for HDPE-100 ^[11]. These conditions have resulted in a decrease in the compressive strength by 40.2% when HDPE is increased from 0% to 50% and by 22.3% when HDPE is increased from 50% to 100% ^[11]. A decreasing trend in the compressive strength of HDPE fine aggregate concrete with the increase of HDPE percentage was observed. As illustrated in <u>Figure 2</u>a, the 28-days' compressive strength varied between 27.5 MPa to 42 MPa when HDPE is added from 0% to 20% ^{[10][12][13]}. Shanmugapriya and Santhi ^[12] observed a 3 MPa drop in compressive strength when HDPE is increased from 0% to 5%. Then the optimum compressive strength of 35 MPa was recorded at HDPE-10 ^[12]. Galupino et al. ^[13] have also observed the optimum compressive strength of 38.6 MPa at HDPE-10. Biswas ^[10] has obtained 35 MPa of compressive strength at HDPE-5 concrete but decreased by 19.3% when HDPE increased to 12.5%. Badache et al. ^[14] have observed a decreasing trend in 28-days' compressive strength with a drop of 52.4% and 57.8% when HDPE is increased from 0% to 50% and 50% to 100%, respectively.

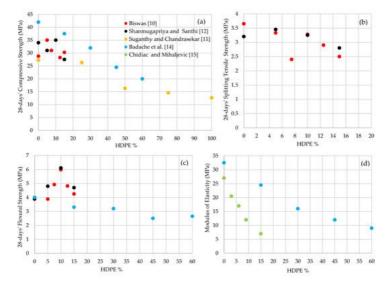


Figure 2. 28-days' (a) Compressive strength; (b) Splitting tensile strength; (c) Flexural strength and (d) Modulus of elasticity variation of HDPE fine aggregate concrete.

The 28-days' splitting tensile strength also shows a decreasing trend with the increase of HDPE content from 0% to 15%, <u>Figure 2</u>b. The HDPE-5 concrete shows the highest splitting tensile strength, 3.45 MPa, which is a 31.25% increase than the standard concrete of HDPE-0 [12]. However, a drop of 18.8% is observed with the increase of HDPE from 5% to 15% [12]. In another study, it was observed a 8.7% and 27.9% of splitting tensile strength drop when HDPE is added from 0% to 5% and from 5% to 7.5%, respectively [10]. There was a tensile strength gain of 26.8% when HDPE is increased from 7.5% to 10%, however, a drop of 23.8% was noted when HDPE is increased from 10% to 15% [10].

Similar to compressive and splitting tensile strengths, the flexural strength also decreases with the increases of HDPE fine aggregate percentage, Figure 2c. It is interesting to note that the flexural strength of concrete incorporated with HDPE up to 15% was higher than the standard concrete $\frac{[10][12]}{12}$. The flexural strength has increased by 56.4% with the increase of HDPE from 0% to 10% and obtained the optimum flexural strength of 6.1 MPa at HDPE-10 $\frac{[12]}{12}$. Then, a slight strength drop of 1.4 MPa was observed at HDPE-15 $\frac{[12]}{12}$. A similar flexural strength development was observed by Biswas et al. $\frac{[10]}{12}$ when HDPE is increased from 0% to 15%. There was no change in flexural strength in HDPE-0 and HDPE-5 concretes, and then a 54.1% strength gain was noted with the increase of HDPE from 5% to 10% and obtained optimum flexural strength of 5.98 MPa at HDPE-10 $\frac{[10]}{12}$. A drop of 28.9% was observed, when HDPE is added from 10% to 15% $\frac{[10]}{12}$.

The modulus of elasticity is decreased with the increase of HDPE percentage, Table 2. According to Figure 2d, there was a considerable elasticity modulus decrease, 74%, when HDPE content increases up to 15% $\frac{[14][15]}{[14]}$. It is observed that the density of the HDPE fine aggregate concrete is decreased with the increase of recycled HDPE content, Table 2. The density of HDPE fine aggregate concrete has varied from 2165 kg/m³ to 1825 kg/m³, when HDPE increases from 0% to 15% $\frac{[15]}{[15]}$. Badache et al. $\frac{[14]}{[15]}$ have observed a 20% density reduction with the increase of HDPE from 0% to 60% and obtained a density of 1760 kg/m³ at HDPE-60.

Table 1. Mix design and compressive strength properties of HDPE fine aggregate concrete.

	Mix Desi	gn								Mecha	anical Pr	operties
Reference	Cement	HDPE	Sand	HDPE	Sand	Coarse	Water	W/C	Admixtures/Superplasticizer	Comp	ressive \$	Strength
	(kg/m ³)	%	%	(kg/m ³)	(kg/m ³)	Aggregates (kg/m³)	(kg/m ³)	Ratio	(w%)	3 days	7 days	14 days
[<u>10</u>]	315	0	100	0	892.2	1285.5	132.3	0.42	-	-	17.77	23.09
[13]	-	0	100	-	-	-	-	-	-	-	29.65	33.49
[<u>12</u>]	320	0	100	-	848.6	1286.5	134.4	0.42	-	-	24	28
[<u>11</u>]	-	0	100	-	-	-	-	0.45	-	-	15.55	24.75
[<u>15</u>]	118 kg	0	100	-	841 kg	522 kg	32 I	-	-	19	-	-
[<u>14</u>]	400	0	100	-	-	-	200	0.5	0.8	-	34.5	-
[<u>15</u>]	118 kg	3	97	-	816 kg	522 kg	30 I	-	-	18.5	-	-
[<u>10</u>]	315	5	95	44.6	847.6	1285.5	132.3	0.42	-	-	23	27.8
[13]	-	5	95	-	-	-	-	-	-	-	15.69	18.41
[12]	320	5	95	-	806.2	1286.5	134.4	0.42	-	-	22	24.5

•	Mix Design											Mechanical Properties			
Reference	Cement	HDPE	Sand	HDPE	Sand	Coarse	Water	W/C	Admixtures/Superplasticizer		ressive S	Strength			
	(kg/m ³)	%	%	(kg/m ³)	(kg/m ³)	Aggregates (kg/m³)	(kg/m³)	Ratio	(w%)	3 days	7 days	14 days			
[<u>15</u>]	118 kg	6	94	-	790 kg	522 kg	30 I	-	-	14	-	-			
[<u>10</u>]	315	7.5	92.5	65.3	805.2	1285.5	132.3	0.42	-	-	21	25			
[<u>15]</u>	118 kg	9	91	-	765 kg	522 kg	30 I	-	-	12	-	-			
[<u>10</u>]	315	10	90	84.8	762.8	1285.5	132.3	0.42	-	-	24.2	26.8			
[13]	-	10	90	-	-	-	-	-	-	-	23.69	34.87			
[12]	320	10	90	-	763.8	1286.5	134.4	0.42	-	-	24	27.5			
[<u>10</u>]	315	12.5	87.5	103.2	722.3	1285.5	132.3	0.42	-	-	18.9	24			
[10]	315	15	85	149.6	847.6	1156.86	132.3	0.42	-	-	22.9	25			
[13]	-	15	85	-	-	-	-	-	-	-	23.76	27.48			
[12]	320	15	85	-	721.3	1286.5	134.4	0.42	-	-	18	22			
[14]	400	15	85	-	-	-	200	0.5	0.7	-	31.5	-			
[<u>15]</u>	118 kg	15	85	-	715 kg	522 kg	29 I	-	-	6.5	-	-			
[11]	-	25	75	-	-	-	-	0.5	-	-	12.44	23.852			
[14]	400	30	70	-	-	-	200	0.5	0.6	-	27.5	-			
[14]	400	45	55	-	-	-	200	0.5	0.55	-	23	-			
[11]	-	50	50	-	-	-	393.75	0.5	-	-	11.33	14.81			
[14]	400	60	40	-	-	-	200	0.5	0.5	-	18.5	-			
[11]	-	75	25	-	-	-	433.125	0.55	-	-	9.55	13.18			
[11]	-	100	0		-	-	472.5	0.6	-	-	9.1	11.55			

Table 2. Tensile strength, elastic modulus, density, and workability properties of HDPE fine aggregate concrete.

	Mecha	nical Pro	perties									
Reference	Split To	ensile St	rength	Flexur	al Streng	th (MPa)		Modulus of	Density	Slump		
	7 days	14 days	28 days	7 days	14 days	28 days	90 days	180 days	Elasticity (GPa)	(Kg/m³)	(mm)	
[10]	2.1	2.72	3.65	2.92	3.28	3.88	-	-	-	-	-	
[13]	-	-	-	-	-	-	-	-	-	-	-	
[12]	1.25	2.9	3.2	2.4	3.1	3.9	-	-	-	-	-	
[11]	-	-	-	-	-	-	-		-	-	90	
[<u>15</u>]	-	-	-	-	-	-	-	-	27	2165	-	
[14]	-	-	-	3.75	-	4	4.15	4.75	32.5	2220	-	
[<u>15</u>]	-	-	-	-	-	-	-	-	20.5	2097	-	
[10]	1.28	2.75	3.33	2.15	3.1	3.88	-	-	-	-	70	
[13]	-	-	-	-	-	-	-	-	-	-	-	
[<u>12</u>]	1.25	2.85	3.45	2.5	3.8	4.8	-	-	-	-	-	
[<u>15]</u>	-	-	-	-	-	-	-	-	17	2022	-	
[10]	1.28	1.8	2.4	2.18	2.26	4.92	-	-	-	-	65	
[<u>15</u>]	-	-	-	-	-	-	-	-	12	1930	-	
[<u>10</u>]	2.02	2.65	3.28	3.2	3.2	5.98	-	-	-		45	
[<u>13</u>]	-	-	-	-	-	-	-	-	-	-	-	

	Mecha	Mechanical Properties													
Reference	Split To	ensile St	rength	Flexur	al Streng	th (MPa)		Modulus of	Density	Slump					
	7 days	14 days	28 days	7 days	14 days	28 days	90 days	180 days	Elasticity (GPa)	(Kg/m³)	(mm)				
[12]	1.95	2.65	3.25	3.5	4.7	6.1	-	-	-	-	-				
[<u>10</u>]	1.88	2.38	2.9	2.28	2.27	4.82	-	-	-	-	40				
[<u>10</u>]	1.35	2.01	2.5	3.27	3.15	4.25	-	-	-	-	30				
[13]	-	-	-	-	-	-	-	-	-	-	-				
[12]	1.8	2.3	2.8	2.2	3.6	4.7	-	-	-	-	-				
[<u>14</u>]	-	-	-	3.25	-	3.3	3.7	4.4	24.5	2120	-				
[<u>15</u>]	-	-	-	-	-	-	-	-	7	1825	-				
[11]	-	-	-	-	-	-	-	-	-	-	90				
[<u>14</u>]	-	-	-	2.9	-	3.2	3.15	3.4	16	2000	-				
[14]	-	-	-	2.5	-	2.5	3	3.4	12	1890	-				
[11]	-	-	-	-	-	-	-	-	-		90				
[14]	-	-	-	2.35	-	2.65	2.65	3	9	1760	-				
[<u>11</u>]	-	-	-	-	-	-	-	-	-		90				
[11]	-	-	-	-	-	-	-	-	-	-	90				

2.2. Durability Characteristics of HDPE Fine Aggregate Concrete

Water adsorption of HDPE fine aggregate concrete has increased from 5% to 10.4%, when recycled HDPE content increases from 0% to 15% $^{[15]}$. Similarly an increment of 5.5 kg/m²/min has been observed in initial rate of adsorption (IRA) from 0.5 kg/m²/min to 6.0 kg/m²/min, with the increase of HDPE from 0% to 15% $^{[15]}$. It is observed that the chloride ion penetration is reduced and lies in the range of 2000–4000 Coulombs with the increase of HDPE content in concrete $^{[12]}$. For instance, when HDPE increased from 0% to 15% in concrete, the chloride permeability has reduced from 4250 to 2700 Coulombs which is a 36.5% reduction $^{[12]}$.

After 28 days of curing, the Ultrasonic Pulse Velocity (UPV) test was performed on HDPE fine aggregate concrete and it is observed that the velocity has decreased from 3880 m/s to 2720 m/s, with the increase of HDPE from 0% to 60% in 15% intervals $^{[\underline{14}]}$. Additionally, slight drops of 6 m/s, 41 m/s, 19 m/s, 118 m/s and 170 m/s were observed in UPV at HDPE-0, HDPE-15, HDPE-30, HDPE-45 and HDPE-60, respectively, over the curing period of 28 to 90 days $^{[\underline{14}]}$.

Thermal conductivity has dropped from 2 W/m·K to 1.14 W/m·K when HDPE increases from 0% to 60% at 7 days [14]. Similar readings have been observed in thermal conductivity variation for 14, 28, 90 and 365 days which are slight drops of 0.8 W/m·K, 0.81 W/m·K, 0.76 W/m·K and 0.69 W/m·K, respectively, with the increase of HDPE percentage in concrete [14]. It was also observed that thermal conductivity has dropped between 7 and 90 days, when HDPE is added from 0% to 60% in 15% intervals [14]. These reductions are recorded to be by 11%, 5.2%, 6.7%, 3.8% and 10.5% for HDPE-0, HDPE-15, HDPE-30, HDPE-45 and HDPE-60, respectively [14]. However, after 90 days, both standard and HDPE fine aggregate concretes have shown a stable conductivity as the decrease of thermal conductivity between 90 and 365 days are 2.8%, 3%, 0%, 4% and 1.9% for HDPE-0, HDPE-15, HDPE-30, HDPE-45 and HDPE-60 concrete, respectively [14].

2.3. Mechanical Properties of HDPE Coarse Aggregate Concrete

The workability (slump) of HDPE coarse aggregate concrete has reduced from 61 mm to 55 mm, and to 28 mm, when HDPE is increased from 0% to 4% in 2% intervals while keeping the water/cement (W/C) ratio at 0.55, <u>Table 3</u> [16]. HDPE-6 and HDPE-8 showed zero slump with the same W/C ratio of 0.55 [16]. Another experiment has recorded 55 mm and 13 mm slumps at HDPE-0 and HDPE-100 concretes [17]. Both experiments have observed a reduction in the workability of the HDPE coarse aggregate concrete with the increase of HDPE. Philomina and D'Mello [18] have observed that the slump has increased from 95 mm to 118 mm, an increase of 24.2%, when HDPE is added from 0% to 32%. Similarly, it has also observed an increment in the slump from 10 mm to 18 mm with the increase of HDPE from 0% to 30% in 10% intervals [19].

Similar to HDPE fine aggregate concrete, the compressive strength of HDPE coarse aggregate concrete decreases with the increases of HDPE percentage, <u>Figure 3</u>a. Lopez et al. $^{[20]}$ observed compressive strength reduction from 11.6 MPa to 2.3 MPa when HDPE is added from 0% to 30%. Authors further noted that the variation of HDPE coarse aggregate size between $^{1/2}$ " and $^{3/2}$ " has not made any significant impact on the compressive strength $^{[20]}$. Philomina and D'Mello $^{[18]}$

reported a compressive strength reduction from 42.14 MPa to 30.98 MPa with the increase of HDPE from 0% to 32% in 8% intervals. Rahim et al. $^{[19]}$ have observed that the 28-days' compressive strength has dropped from 28.4 MPa to 18.24 MPa, when HDPE is added from 0% to 30% in 10% intervals, which is a drop from 28 MPa to 15.5 MPa by Habib et al. $^{[21]}$, when HDPE is increased from 0% to 20% in 5% intervals and a drop of 15.9 MPa by Kodua $^{[16]}$ with the increase of HDPE from 0% to 8% in 2% intervals. In another study, there is no compressive strength change noted up to 10% of HDPE incorporated in concrete, but afterwards, a little strength drop (i.e., from 26.54 MPa to 22.45 MPa) was observed when HDPE is added from 10% to 30% $^{[22]}$. Similarly, the compressive strength has decreased from 34 MPa to 28.5 MPa with the increase of HDPE from 0% to 10%, an increment of 5.5 MPa during 10% to 15% increase and again, a drop of 5.5 MPa, when HDPE is increased from 15% to 20% $^{[12]}$. It is identified that optimum 28-days' compressive strength is obtained at HDPE-15 $^{[12]}$. However, Lopez et al. $^{[20]}$ suggest that optimum 28-days' compressive strength is obtained at HDPE-10.

Table 3. Mechanical properties of HDPE coarse aggregate concrete.

	Mix Desig	gn								Mechanical Properties				
eferences	Cement	HDPE	Crushed	HDPE	Crushed Stone	Sand	Water	W/C	Admixtures/ Superplasticizer	Compre	essive Str	ength (MF	a)	
	(kg/m³)	%	Stone %	(kg/m³)	(kg/m ³)	(kg/m ³)	(kg/m ³)	Ratio	(w%)	7 days	14 days	28 days	56 day	
[17]	380	0	100	0	1045	665	190	0.5	-	-	-	29.19	-	
[22]	-	0	100	-	-	-	-	0.55	-	21.32	23.68	26.54	-	
[<u>12</u>]	320	0	100	0	1286.5	848.6	-	-	-	24	28	34	-	
[<u>21</u>]	-	0	100	-	-	-	-	0.5	-	18.5	22	28	-	
[18]	-	0	100	-	-	-	-	0.45	Х	23.71	30.5	42.14	43.6	
[<u>20</u>]	-	0	100	-	-	-	-	-	Υ	11.59	-	-	-	
[<u>16</u>]	400	0	100	0	1200	800	-	0.55	-	13.9	19.5	30.6	-	
[<u>19</u>]	-	0	100	-	-	-	-	0.55	-	20.236	25.482	28.402	-	
[23]	-	0	100	-	-	-	-	0.4	-	-	-	10000 Nm/kg	-	
[<u>16</u>]	400	2	98	24	1176	800	-	0.55	-	12.6	16.1	19.8	-	
[<u>16</u>]	400	4	94	48	1152	800	-	0.55	-	12.5	14.1	18.5	-	
[<u>21</u>]	-	5	95	-	-	-	-	0.5	-	17	19	25	-	
[<u>16</u>]	400	6	94	72	1128	800	-	0.55	-	11.3	13.6	16.1	-	
[<u>18</u>]	-	8	92	-	-	-	-	0.45	х	22.5	26.3	40.23	45.3	
[<u>16</u>]	400	8	92	96	1104	800	-	0.55	-	9.4	10.3	14.7	-	
[<u>22</u>]	-	10	90	-	-	-	-	-	-	18.24	22.35	25.64	-	
[<u>12</u>]	320	10	90	128.68	1157.86	848.6	-	-	-	22	24	28.5	-	
[<u>21</u>]	-	10	90	-	-	-	-	0.5	-	14	17	22	-	
[<u>20]</u>	-	(1/2 ?) 10	90	-	-	-	-	-	- ү	4.147	-	-	-	
	-	(3/4 ?) 10	90	-	-	-	-	-	•	3.183	-	-	-	
[<u>19</u>]	-	10	90	-	-	-	-	0.55	-	18.964	22.706	26.617	-	
[23]	-	10	90	-	-	-	-	0.4	-	-	-	4500 Nm/kg	-	
[<u>22</u>]	-	15	85	-	-	-	-	-	-	17.23	20.49	23.37	-	
[<u>12</u>]	320	15	85	192.99	1093.55	848.6	-	-	-	24.5	26.5	34	-	
[<u>21</u>]	-	15	85	-	-	-	-	0.5	-	13	14	18.5	-	
[23]	-	15	85	-	-	-	-	0.4	-	-	-	3800 Nm/kg	-	
[<u>18</u>]	-	16	84	-	-	-	-	0.45	Х	21.18	24.73	37.66	43.8	
[22]	-	20	80	-	-	-	-	-	-	15.67	19.13	22.45	-	

	Mix Desi	gn								Mechan	ical Prope	erties	
eferences	Cement	HDPE	Crushed	HDPE	Crushed Stone	Sand	Water	W/C	Admixtures/ Superplasticizer	Compre	essive Stre	ength (MP	'a)
	(kg/m³)	%	Stone %	(kg/m ³)	(kg/m ³)	(kg/m³)	(kg/m³)	Ratio	(w%)	7 days	14 days	28 days	56 days
[<u>12</u>]	320	20	80	257.31	1029.23	848.6	-	-	-	21.5	23.5	28.5	-
[21]	-	20	80	-	-	-	-	0.5	-	11	13	15.5	-
[20]	-	(1/2 ?) 20	80	-	-	-	-	-	· Y	3	-	-	-
_	-	(3/4 ?) 20	80	-	-	-	-	-	1	2	-	-	-
[<u>19</u>]	-	20	80	-	-	-	-	0.55	-	14.161	18.298	22.997	-
[<u>23</u>]	-	20	80	-	-	-	-	0.4	-	-	-	3000 Nm/kg	-
[18]	-	24	76	-	-	-	-	0.45	х	16.66	22.91	35.54	42.28
[<u>23</u>]	-	25	75	-	-	-	-	0.4	-	-	-	2200 Nm/kg	-
[20]	-	(1/2 ?) 30	70	-	-	-	-	-	· Y	1.445	-	-	-
_	-	(3/4 ?) 30	70	-	-	-	-	-	•	2.3	-	-	-
[<u>19</u>]	-	30	70	-	-	-	-	0.55	-	10.835	14.037	18.244	-
[18]	-	32	68	-	-	-	-	0.45	Х	14.84	20.46	30.98	39.85
[<u>17]</u>	380	60	40	172	412	665	190	0.5	-	-	-	19.85	-
[<u>17</u>]	380	80	20	229	209	665	190	0.5	-	-	-	13.37	-
[17]	380	100	0	286	0	665	190	0.5	-	-	-	11.79	-

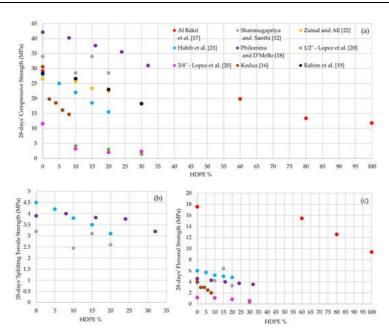


Figure 3. 28-days' (a) Compressive strength; (b) Splitting tensile strength and (c) Flexural strength variations of HDPE coarse aggregate concrete.

The splitting tensile strength also shows a decreasing trend with the increment of HDPE content, Figure 3b $^{[12][18][21]}$. A tensile strength reduction of 1.4 MPa (is observed at 28 days with the increase of HDPE from 0% to 20% $^{[21]}$. There is no tensile strength change recorded until HDPE is added up to 8%, but 0.8 MPa strength reduction was noted when HDPE increased to 32% $^{[18]}$. Shanmugapriya and Santhi $^{[12]}$ noted the contradicted behavior illustrating a significant splitting tensile strength reduction of 23.4% when incorporated with 10% HDPE in concrete. However, tensile strength gain (26.5%) was observed with the increase of HDPE content from 10% to 15% and, again, a drop of 16.1% when HDPE increased from 15% to 20% $^{[12]}$. It is identified that HDPE-15 achieves the optimum 28-days' splitting tensile strength.

Flexural strength or bending strength reduces with the increase of HDPE when incorporated as coarse aggregate in concrete Figure 3c. Bakri et al. [17] noted that the flexural strength decreased from 17.56 MPa to 15.47 MPa with the increase of HDPE content up to 60%. The flexural strength has dropped by 6.1 MPa when the HDPE is added from 60% to 100% [17]. It has also been observed that the 28-days' flexural strength of HDPE coarse aggregate concrete is dropped by 1.9 MPa (from 6 MPa to 4.1 MPa) when HDPE increases from 0% to 20% in 5% intervals [21]. A 2 MPa flexural strength drop is observed with the increase of HDPE from 0% to 8% [16][18][20]. Shanmugapriya and Santhi [12] observed the opposite trend as a 2.5 MPa flexural strength gain obtained at 28 days for HDPE-15 concrete. The same experiment has achieved the optimum 28-days' flexural strength of 6.4 MPa at HDPE-15, followed by a drop of 3.1 MPa, when HDPE is increased by another 5% [12]. It is noted that the optimum 28-days' flexural strength is attained in different HDPE percentages: for instance, 6.4 MPa at HDPE-15 (Shanmugapriya and Santhi) [12], 4.28 MPa at HDPE-8 (Philomina and D'Mello) [18] and 1.075 MPa at HDPE-10 (Lopez et al.) [20].

The density of HDPE coarse aggregate concrete is decreased with the increase of HDPE content, Table 3 [18][20][21]. It is observed that there was a 5.2% reduction in density with the increase of HDPE from 0% to 32% and a 6.1% reduction during 0% to 20% of HDPE addition [12][21]. The density of ½" HDPE coarse aggregate concrete matrix has reduced by 776.1 kg/m³ and by 675.72 kg/m³ in ¾" HDPE coarse aggregate concrete matrix only with the increase of HDPE from 0% to 30% [20]. This reveals that a greater density drop could be achieved when the aggregate size is reduced from ¾" to ½" regardless of the HDPE inclusion percentage. Another notable observation is that the rate of reduction of dry density was 0.2% per volume percent of waste polymer added in HDPE coarse aggregate concrete [23].

2.4. Durability Characteristics of HDPE Coarse Aggregate Concrete

Porosity and permeability of HDPE coarse aggregate concrete have increased with the increase of HDPE content [20]. The HDPE-0 standard concrete displayed a porosity of 22.67 and increased it up to 36.21 when HDPE was added to 30% [20]. The typical value of permeability of a pervious concrete ranges from 0.135 to 1.219 cm/s and all the HDPE coarse aggregate concretes display a higher permeability than the range specified [20]. Permeability of ½" HDPE coarse aggregate concrete has increased by 5.28 cm/s, when the HDPE increases from 0% to 30% in 10% intervals [20]. Similarly, the permeability was increased by 4.03 cm/s, when ¾" HDPE coarse aggregates are increased in the same range [20]. It can be noted that the permeability of HDPE coarse aggregate concrete of this research study has exceeded the industry standards and varies between 0.135467 to 1.2192 cm/s [20]. Moreover, the porosity of HDPE coarse aggregate concrete has increased by 65% and 59.7%, with the increase of HDPE from 0% to 30% for ½" and ¾" aggregate sizes, respectively. An extensive study carried out on sorptivity of HDPE coarse aggregate concrete results in a drop of 45.4% in sorptivity with the increase of HDPE from 0% to 32% [18].

Water absorption rate of HDPE coarse aggregate concrete is increased by 34.7%, when the HDPE increase from 0% to 20% $^{[22]}$. In another experiment, a similar gain, 35.5% in water absorption was observed with the increase of HDPE content to 8% $^{[16]}$. However, Philomina and D'Mello $^{[18]}$ have observed a 6.13% drop (from 4.4% to 4.13%) in water absorption rate of HDPE coarse aggregate concrete when HDPE is added from 0% to 32% $^{[18]}$.

At direct UPV test, the pulse velocity of HDPE coarse aggregate concrete has increased from 4200 m/s to 4650 m/s, when HDPE is added from 0% to 16% [18]. After reaching the maximum velocity, 4650 m/s at HDPE-16, a drop of 560 m/s was recorded with the increase of HDPE from 16% to 32% [18]. The same experiment has performed an indirect UPV test for HDPE coarse aggregate concrete. Initially, the velocity is increased by 560 m/s, when HDPE increases from 0% to 8% [18]. Then, an 830 m/s velocity drop during 8% to 16% HDPE addition is observed, followed by a 1030 m/s velocity gain with the increase of HDPE from 16% to 24% and, finally, a drop of 1860 m/s, when HDPE is added from 24% to 32% [18]. The same study has carried out the rebound hammer test and have obtained rebound values at 56-days' compressive strength [18]. The 56-day rebound values have increased from 40 to 42 when HDPE is added from 0% to 8% and then have dropped from 42 to 36 with the increase of HDPE from 8% to 32% [18]. Compressive strength obtained through rebound hammer test as well as through a destructive test show similar increments by 2.1 MPa and 1.71 MPa when HDPE increases from 0% to 8% and drops by 6.32 MPa and 5.47 MPa when HDPE is added from 8% to 32%, respectively [18].

When considering the sulphate attack test, the compressive strength of HDPE coarse aggregate concrete (with the increase of HDPE from 0% to 32%) is increased when immersed with Na2SO4 apart from the standard concrete matrix (HDPE-0) [18]. Compressive strength is observed to be dropped by 1.48 MPa in the standard concrete matrix (HDPE-0) after immersion in Na2SO4 [18]. Compressive strength is increased by 0.33 MPa, 0.51 MPa, 0.58 MPa and 1.63 MPa at HDPE-8, HDPE-16, HDPE-24 and HDPE-32 concretes, respectively [18]. This has further displayed a 6.25% of weight loss due to a sulphate attack test in HDPE coarse aggregate concrete with the increase of HDPE from 0% to 32% [18].

An acid attack test was carried out through a comparison of compressive strength values obtained after immersing HDPE coarse aggregate concrete mixes in both water and hydrochloric (HCl) acid after curing for 28 days [18]. When the HDPE is increased from 0% to 32% in 8% intervals, the compressive strength has reduced by 12.21 MPa and 12.45 MPa after immersion in HCl acid and water, respectively. When comparing the compressive strength drop of each HDPE coarse aggregate concrete matrix: HDPE-0, HDPE-8, HDPE-16, HDPE-24 and HDPE-32 due to immersion in HCl acid is recorded to be 2.7%, 5.0%, 4.1%, 3.31% and 2.97%, respectively [18]. The least compressive strength drop was recorded

in HDPE-0 concrete matrix and, however, it can be observed that the compressive strength drop has reduced significantly with an increase of HDPE. The same experiment has observed an increase of 54.5% in weight loss percentage, with the increase of HDPE from 0% to 32% $^{[\underline{18}]}$. According to Kodua $^{[\underline{16}]}$, when concrete mixes are immersed in nitric (HNO3) acid solution, compressive strength of HDPE coarse aggregate concrete is decreased by 53.9% with the increase of HDPE from 0% to 8%. An increase in weight loss of 34.1% was also observed, after immersing in HNO3, when HDPE is increased from 0% to 8% $^{[\underline{16}]}$. Therefore, the effects imposed due to acids on HDPE coarse aggregate concrete are very minimal and can withstand the chemical reactions within the concrete $^{[\underline{18}]}$.

3. Use of HDPE as a Fiber Reinforcement in Concrete

3.1. Mechanical Properties of HDPE Fiber Reinforced Concrete

Table 4 illustrates that the workability (slump) of HDPE fiber reinforced concrete was reduced by 73.8% when adding 1.25% of HDPE fibers having a diameter of 0.25 mm and a length of 23 mm while maintaining the same w/c ratio of 0.62 $\frac{[24][25]}{[25]}$. Pešić et al. $\frac{[24]}{[25]}$ reveal that varying the fiber diameter from 0.25 mm to 0.4 mm and length from 23 mm to 30 mm, has reduced the slump by 3 mm at HDPE-0.4 and by 4 mm at HDPE-0.75 and HDPE-1.25. It also suggests that increasing the water content used in HDPE concrete matrix and adding water-reducing agents can prevent segregation of plastic fibers in the reinforced concrete mixes $\frac{[26]}{[26]}$. As a result, Dehydol LS-12 (LS-12) nonionic surfactant is used to increase the wettability of plastic materials $\frac{[26]}{[26]}$. With the addition of the Dehydol LS-12, it was observed that the slump values are decreased from 130 mm to 20 mm when w/c ratio is increased from 0.5 to 0.6 and the HDPE fiber are increased from 0% to 30% $\frac{[26]}{[26]}$.

Table 4. Mechanical properties of HDPE fiber reinforced concrete.

	Mix Desig	gn								Mecha	ınical Pı	operties	5			
eference	Cement (kg/m³)	HDPE			HDPE (kg/m³)	Crushed Stone	Sand (kg/m³)	Water Content	W/C Ratio	-	ressive jth (MPa	u)	Split T Strenç	ensile jth (MPa	ı)	Flexi Strei (MPa
	(kg/iii)	L (mm)	d (mm)	%	(kg/iii)	(kg/m ³)	(kg/iii)	(kg/m³)	Ratio	7 days	28 days	90 days	7 days	28 days	90 days	7 days
[24]	380	-	-	0	0	860	780	235	0.62	-	33.2	38.1	-	2.79	3.32	-
[<u>25</u>]	-	-	-	0	0	-	-	-	-	-	33.2	38.1	-	2.79	3.32	-
[27]	-	-	-	0	0	-	-	-	0.42	25	37	-	3	3.75	-	1.7
[26]	33 kg	-	-	0	0	-	66 kg	16.5 kg	0.5	-	26	-	-	3	-	-
[24]	380	23	0.25	0.4	-	860	780	235	0.62	-	34.3	40.1	-	3.08	3.47	-
[24]	380	30	0.4	0.4	-	860	780	235	0.62	-	31	37.2	-	3.03	3.4	-
[25]	-	23	0.25	0.4	-	-	-	-	-	-	34.3	40.1	-	3.08	3.47	-
[27]	-	-	-	0.5	-	-	-	-	-	29	37	-	2.9	3.8	-	1.75
[24]	380	23	0.25	0.75	-	860	780	235	0.62	-	31.1	38.4	-	2.95	3.49	-
[24]	380	30	0.4	0.75	-	860	780	235	0.62	-	31	37.7	-	2.93	3.47	-
[25]	-	23	0.25	0.75	-	-	-	-	-	-	31.1	38.4	-	2.95	3.49	-
[27]	-	-	-	1	-	-	-	-	-	29.5	37.5	-	3.2	3.85	-	1.9
[24]	380	23	0.25	1.25	-	860	780	235	0.62	-	32.3	37.7	-	2.96	3.43	-
[24]	380	30	0.4	1.25	-	860	780	235	0.62	-	30.5	38.7	-	2.88	3.53	-
[25]	-	23	0.25	1.25	-	-	-	-	-	-	32.3	37.7	-	2.96	3.43	-
[27]	-	-	-	1.5	-	-	-	-	-	30	38	-	3.3	3.9	-	2
[27]	-	-	-	2	-	-	-	-	-	30.5	38.5	-	3.4	4.1	-	2.1
[27]	-	-	-	2.5	-	-	-	-	-	31	39	-	2.4	4.25	-	2.1
[27]	-	-	-	3	-	-	-	-	-	32	39	-	3.6	4.3	-	2.2
[27]	-	-	-	3.5	-	-	-	-	-	33	40	-	3.7	4.4	-	2.25
[27]	-	-	-	4	-	-	-	-	-	30.5	38.5	-	3.6	4.2	-	2.2
[27]	-	-	-	4.5	-	-	-	-	-	30	37.5	-	3.55	4.1	-	2.1
[27]	-	-	-	5	-	-	-	-	-	29.5	36.5	-	3.5	3.9	-	2.05

	Mix Desi	gn								Mechanical Properties							
eference	Cement	HDPE			HDPE	Crushed Stone	Sand	Water Content	W/C		ressive gth (MPa	ı)	•	Tensile gth (MPa	a)	Flexu Strer (MPa	
	(kg/m³)	L (mm)	d (mm)	%	- (kg/m³)	(kg/m³)	(kg/m³)	(kg/m ³)	Ratio	7 days	28 days	90 days	7 days	28 days	90 days	7 days	
[26]	30.12 kg	-	-	5	0.14	-	60.24 kg	15.06	0.5	-	16.5	-	-	1.8	-	-	
[27]	-	-	-	5.5	-	-		-	-	29	36	-	3.4	3.8	-	2	
[27]	-	-	-	6	-	-		-	-	27.5	34.5	-	3.3	3.7	-	1.9	
[26]	30.12 kg	-	-	10	0.28	-	60.24 kg	15.05kg	0.5	-	12	-	-	1.9	-	-	
[26]	30.12 kg	-	-	15	0.42	-	60.24 kg	16.57 kg	0.55	-	9	-	-	1.3	-	-	
[26]	30.12 kg	-	-	20	0.56	-	60.24 kg	18.07 kg	0.6	-	5.5	-	-	0.7	-		
[26]	30.12 kg	-	-	30	0.84	-	60.24 kg	18.07 kg	0.6	-	-	-	-	-	-		

As illustrated in Figure 4a, the compressive strength has decreased by 8.13% when HDPE fibers with a diameter of 0.4 mm are added from 0% to 1.25% $^{[24]}$. Moreover, when the HDPE fiber diameter is 0.25 mm, the compressive strength has increased by 3.3% with the increase of HDPE fibers from 0% to 0.4% and, again, dropped by 5.8% when fibers are added from 0.4% to 1.25% $^{[24][25]}$. Malagavelli and Patura $^{[27]}$ showed that the optimum compressive strength of 40 MPa was achieved by HDPE-3.5 concrete when the fiber content is varied between 0% and 6%. When the fibers are added by 5% intervals from 0% to 20%, the compressive strength has significantly dropped from 26 MPa to 20 MPa $^{[26]}$. However, it has been identified that the large volume fraction of HDPE fibers often lowers the compressive strength of concrete $^{[26]}$. Poonyakan et al. $^{[26]}$ have suggested that all concrete used for precast wall panels (non-structural load carrying) must have a minimum compressive strength of 16 MPa which can be fulfilled by adding HDPE fibers up to 5% $^{[26]}$.

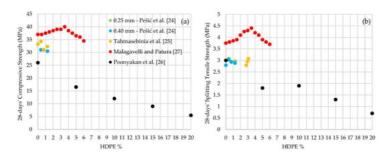


Figure 4. 28-days' (a) Compressive strength and (b) Split tensile strength variations of HDPE fiber reinforced concrete.

The 28-days' splitting tensile strength of HDPE fiber reinforced concrete has increased by 10.4%, when fibers with 0.25 mm diameter are added from 0% to 0.4% and again a 3.9% drop is observed, when fibers are added from 0.4% to 1.25%, Figure 4b $^{[24][25]}$. Similarly, the splitting tensile strength has increased from 2.79 MPa to 3.03 MPa, when fibers with 0.40 mm diameter are added from 0% to 0.4%, and a drop of 0.15 MPa is observed, when HDPE fibers are added from 0.4% to 1.25% $^{[24]}$. Similar to compressive strength observations, Malagavelli and Patura $^{[27]}$ have observed the optimum splitting tensile strength of 4.4 MPa at HDPE-3.5, when the fiber content varied between 0% and 6%. In another experiment, the splitting tensile strength has dropped by 40% with the increase of HDPE from 0% to 5%, followed by a slight gain of 5.6% at HDPE-10 and then, again, tensile strength has dropped by 63.2%, when HDPE fibers are added from 10% to 20% $^{[26]}$. On the other hand, the 28-days' flexural strength of HDPE fiber reinforced concrete is always greater than the standard concrete (HDPE-0) regardless of the HDPE fiber percentage being added, $^{[27]}$. It is observed that, the flexural strength has increased from 3.4 MPa to an optimum of 4.9 MPa when the HDPE fibers are added from 0% to 3% in 0.5% intervals and then the flexural strength has dropped by 1.3 MPa when the HDPE fibers are added from 3% to 6% in 0.5% intervals $^{[27]}$.

A slight increase (1.0 GPa) is observed in the elastic modulus of HDPE fiber reinforced concrete with the increase of 0.25 mm diameter HDPE fibers from 0% to 1.25%, Table 4 [24]. The same experiment shows that the elastic modulus has increased by 1.3 GPa, when the 0.4 mm diameter HDPE fibers are added from 0% to 1.25% $^{[24]}$.

3.2. Durability Characteristics of HDPE Fiber Reinforced Concrete

When considering the water permeability after 45 days, it has been identified that, the height of water penetration in HDPE fiber reinforced concrete has reduced from 43 mm to 26 mm, when HDPE fibers with 0.4 mm diameter are added from 0% to 1.25% $\frac{[24]}{}$. Similarly, HDPE fibers with 0.25 mm diameter have reduced the height of water penetration from 43 mm to

28 mm in similar HDPE percentages [24]. HDPE fiber reinforced concrete has contributed in reducing the water intake from 35% to 80% with the increase of HDPE fibers from 0.40% to 1.25% compared to HDPE-0 standard concrete [24]. Poonyakan et al. [26] have observed that the porosity of the HDPE fiber reinforced concrete has increased by 45% when HDPE is added from 0% to 30%. Hence, it has been identified that the recycled HDPE fibers greatly improve the durability of concrete.

It has been observed that the overall number of cracks and the widths of cracks were reduced in HDPE fiber reinforced concrete when compared with the standard concrete [24]. Average crack width and the maximum crack width of 0.25 mm HDPE fiber reinforced concrete have been reduced by 83.63% and 81.8%, respectively when HDPE fibers are added from 0% to 1.25% [24]. Similarly, average crack width and the maximum crack width of 0.4 mm HDPE fiber reinforced concrete have been reduced by 76.4% and 77.3% when HDPE fibers are added from 0% to 1.25% [24]. Crack reduction ratio of 0.25 mm and 0.4 mm HDPE fiber reinforced concrete increased from 34.5% to 83.6%, and from 54.5% to 76.4% when HDPE fibers are increased from 0.4% to 1.25%, compared with the standard concrete matrix (HDPE-0) [24].

4. Use of HDPE as a Cement Binder

Aattache et al. $\frac{[28]}{}$ investigated the cement replacement using HDPE up to 6%. It is observed that the 28-days' compressive strength has decreased from 37 MPa to 22 MPa, which is a 40.5% drop, when HDPE is added from 0% to 6% $\frac{[28]}{}$. Similarly, the 7-day and 90-day compressive strength variations display decreasing trends with a strength drop of 46.7% and 28.6%, respectively, with the increase of similar HDPE percentages $\frac{[28]}{}$. Similar to compressive strength, the splitting tensile strength also decreases with the increase of HDPE from 0% to 6% in 2% intervals over 7, 28 and 90 days $\frac{[28]}{}$. They have observed tensile strength decrease of 1.7 MPa, 3.9 MPa and 3.2 MPa at 7, 28 and 90 days, respectively, with the use of HDPE in 6% $\frac{[28]}{}$.

HDPE has a comparatively low thermal conductivity of 0.33 W/m·K compared with the concrete $^{[28]}$. It was observed that the thermal conductivity of cement replaced HDPE concrete is decreased with the increase of HDPE $^{[28]}$. At 20 °C, the 28-days' thermal conductivity of cement replaced HDPE concrete is decreased by 15.6%, when HDPE is increased from 0% to 6% in 2% intervals $^{[28]}$. Similar observations are recorded for 28-days' thermal conductivity for 140 °C, 250 °C and 350 °C which reduce by 15.8%, 22.2% and 12%, respectively. Thermal conductivity of cement replaced HDPE concrete is decreased with an increase of temperature from 20 °C to 350 °C, when HDPE is added up to 6% $^{[28]}$. It was also observed that concrete mixes with a superplasticizer have a higher thermal conductivity in comparison with the standard concrete matrix (HDPE-0) since the 28th day $^{[28]}$.

On the other hand, Naik et al. $^{[29]}$ investigated the use of HDPE as a filler material in concrete, where HDPE is added up to 2% in 0.5% intervals. It was observed that the 28-days' compressive strength of HDPE filler concrete was increased by 2.5%, when HDPE is added from 0% to 0.5% $^{[29]}$. Then, a drop of 46.3% has been observed in compressive strength with the increase of HDPE from 0.5% to 2% in 0.5% intervals $^{[29]}$. Similar gains of 3.2% and 13% were observed for 3-day and 7-day compressive strengths, respectively, when HDPE is increased from 0% to 0.5% $^{[29]}$. Additionally, 25% and 42.3% drops in 3-day and 7-day compressive strength were observed when HDPE increased from 0.5% to 2% $^{[29]}$.

References

- 1. Kaza, S.; Yao, L.; Bhada-Tata, P.; Van Woerden, F. What a Waste 2.0: A Global Snapshot of Solid Waste Management t o 2050; The World Bank: Washington, DC, USA, 2018.
- 2. Tiseo, I. Plastic Waste Worldwide-Statistics and Facts. Available online: (accessed on 4 September 2020).
- 3. Geyer, R.; Jambeck, J.; Law, K.L. Production, use, and fate of all plastics ever made. Sci. Adv. 2017, 3, 1207–1221.
- 4. Andersen, L.; Wejdling, A.; Neidel, T.L. Plastic Waste–Background Report; Nordic Council of Ministers: Beau Vallon, Se ychelles, 2015.
- 5. Lukkassen, D.; Meidell, A. Advanced Materials and Structures and Their Fabrication Processes; Narrik University Colle ge: Hin, Norway, 2003.
- 6. Nguyen, K.T.; Navaratnam, S.; Mendis, P.; Zhang, G.K.; Barnett, J.; Wang, H. Fire safety of composites in prefabricated buildings: From fibre reinforced polymer to textile reinforced concrete. Compos. Part B. Eng. 2020, 187, 107815.
- 7. Gunasekara, C.; Setunge, S.; Law, D.W.; Willis, N.; Burt, T. Engineering Properties of Geopolymer Aggregate Concrete. J. Mater. Civ. Eng. 2018, 30, 04018299.
- 8. Saikia, N.; de Brito, J. Use of plastic waste as aggregate in cement mortar and concrete preparation: A review. Constr. Build. Mater. 2012, 34, 385–401.
- 9. Alauddin, M.; Choudhury, I.; El Baradie, M.; Hashmi, M. Plastics and their machining: A review. J. Mater. Process. Tech nol. 1995, 54, 40–46.
- 10. Biswas, S. Determination of strength characteristics of concrete by partial replacement of aggregates with e waste and hdpe granules. J. Xian Univ. Archit. Technol. 2020, 12, 90–108.

- 11. Suganthy, P.; Chandrasekar, D. Utilization of pulverized plastic in cement concrete as fine aggregate. Int. J. Res. Eng. Technol. 2013, 2, 1015–1019.
- 12. Shanmugapriya, M.M. Helen Santhi. Strength and chloride permeable properties of concrete with high density polyethyl ene wastes. Int. J. Chem. Sci. 2017, 15, 108–116.
- 13. Galupino, J. Response Surface Modelling of Concrete mixed with Fly Ash and Recycled HDPE. 2019. Available online: (accessed on 1 June 2021).
- 14. Badache, A.; Benosman, A.S.; Senhadji, Y.; Mouli, M. Thermo-physical and mechanical characteristics of sand-based lightweight composite mortars with recycled high-density polyethylene (HDPE). Constr. Build. Mater. 2018, 163, 40–52.
- 15. Chidiac, S.; Mihaljevic, S. Performance of dry cast concrete blocks containing waste glass powder or polyethylene aggregates. Cem. Concr. Compos. 2011, 33, 855–863.
- 16. Kodua, J. Influence of recycled waste high density polyethylene plastic aggregate on the physico-chemical and mecha nical properties of concrete. Int. J. Sci. Eng. Sci. 2018, 2, 22–28.
- 17. Al Bakri, A.M. Investigation of HDPE plastic waste aggregate on the properties of concrete. J. Asian Sci. Res. 2011, 1, 340–345.
- 18. Philomina, S.; D'Mello, M. An Experimental Investigation to Produce a Cost Effective Concrete by Partial Replacement of Coarse Aggregate with High Density Polyethylene (HDPE) Waste And Cement with Alccofine. Int. Res. J. Eng. Techn ol. 2017, 4(7), 2712–2717.
- 19. Rahim, N.L.; Sallehuddin, S.; Ibrahim, N.M.; Amat, R.C.; Ab Jalil, M.F. Use of Plastic Waste (High Density Polyethylen e) in Concrete Mixture as Aggregate Replacement. Adv. Mater. Res. 2013, 701, 265–269.
- 20. Lopez, N.; Collado, E.; Diacos, L.A.; Morente, H.D. Evaluation of Pervious Concrete Utilizing Recycled HDPE as Partial Replacement of Coarse Aggregate with Acrylic as Additive. In Proceedings of the MATEC Web of Conferences, EDP S ciences, Yogyakarta, Indonesia, 5–7 September 2018.
- 21. Habib, M.Z.; Alom, M.M. and Hoque, M.M. Concrete production using recycled waste plastic as aggregate. J. Civ. Eng. IEB 2017, 45, 11–17.
- 22. Zainal, S.H.; Ali, S. Effect of Fly Ash and HDPE on Concrete Strength. Politeknik & Kolej Komuniti. J. Eng. Technol. 201 8. 3. 81–89.
- 23. Rahman, M.; Islam, A.; Ahmed, M.; Salam, A. Recycled Polymer Materials as Aggregates for Concrete and Blocks. J. C hem. Eng. 2013, 27, 53–57.
- 24. Pešić, N.; Živanović, S.; Garcia, R.; Papastergiou, P. Mechanical properties of concrete reinforced with recycled HDPE plastic fibres. Constr. Build. Mater. 2016, 115, 362–370.
- 25. Tahmasebinia, F.; Niemelä, M.; Sepasgozar, S.M.E.; Lai, T.Y.; Su, W.; Reddy, K.R.; Shirowzhan, S.; Sepasgozar, S.; Ma rroquin, F.A. Three-Dimensional Printing Using Recycled High-Density Polyethylene: Technological Challenges and Fut ure Directions for Construction. Buildings 2018, 8, 165.
- 26. Poonyakan, A.; Rachakornkij, M.; Wecharatana, M.; Smittakorn, W. Potential Use of Plastic Wastes for Low Thermal C onductivity Concrete. Materials. 2018, 11, 1938.
- 27. Malagavelli, V.; Patura, N.R. Strength characteristics of concrete using solid waste an experimental investigation. Int. J. Earth Sci. Eng. 2011, 4.
- 28. Aattache, A.; Mahi, A.; Soltani, R.; Mouli, M.; Benosman, A.S. Experimental study on thermo-mechanical properties of Polymer Modified Mortar. Mater. Des. 2013, 52, 459–469.
- 29. Naik, T.; Singh, S.; Huber, C.; Brodersen, B. Use of post-consumer waste plastics in cement-based composites. Cem. Concr. Res. 1996, 26, 1489–1492.

Retrieved from https://encyclopedia.pub/entry/history/show/25053