# **CO2 Storage in Shale Reservoirs**

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As a new "sink" of  $CO_2$  permanent storage, the depleted shale reservoir is very promising compared to the deep saline aquifer. To provide a greater understanding of the benefits of  $CO_2$  storage in a shale reservoir, a comparative study is conducted by establishing the full-mechanism model, including the hydrodynamic trapping, adsorption trapping, residual trapping, solubility trapping as well as the mineral trapping corresponding to the typical shale and deep saline aquifer parameters from the Ordos basin in China. The results show that  $CO_2$  storage in the depleted shale reservoir has merits in storage safety by trapping more  $CO_2$  in stable immobile phase due to adsorption and having gentler and ephemeral pressure perturbation responding to  $CO_2$  injection. The effect of various  $CO_2$  injection schemes, namely the high-speed continuous injection, low-speed continuous injection, huff-n-puff injection and water alternative injection, on the phase transformation of  $CO_2$  in a shale reservoir and  $CO_2$ -injection-induced perturbations in formation pressure are also examined. With the aim of increasing the fraction of immobile  $CO_2$  while maintaining a safe pressure-perturbation, it is shown that an intermittent injection procedure with multiple slugs of huff-n-puff injection can be employed and within the allowable range of pressure increase, and the  $CO_2$  injection rate can be maximized to increase the  $CO_2$  storage capacity and security in shale reservoir.

Keywords: CO2 geological storage; shale; phase transformation; pressure perturbation; injection schemes

## 1. Introduction

The capture of anthropogenic carbon dioxide (CO<sub>2</sub>) from industrial or other emission sources and its long-term storage in geological formations to limit its emission into the atmosphere is referred as geological carbon storage (GCS) <sup>[1]</sup>. GCS is regarded as one of the most effective technologies to reduce the greenhouse gas emissions from the combustion of fossil fuels. Besides the conventional  $CO_2$  storage sites in the deep saline aquifers, depleted oil and gas reservoirs, and unminable coal seams <sup>[2][3]</sup>, the depleted shale reservoir is also rapidly becoming a new and potentially promising  $CO_2$  storage option because of the booming production of the unconventional shale gas <sup>[4][5]</sup>.

Interest in  $CO_2$  storage in shale reservoirs has grown recently because shale is widely reported to possess higher affinity to  $CO_2$  than  $CH_4$  and has huge potential for  $CO_2$  adsorption trapping. For example, Heller and Zoback  $^{[\underline{G}]}$ , Kang et al.  $^{[\underline{I}]}$ , and Zhang  $^{[\underline{B}]}$  all tested the  $CO_2/CH_4$  adsorption capacity of shale from different places in the world and demonstrated that the  $CO_2$  adsorption capacity to shale was greater than that of  $CH_4$  under surface condition. Several feasibility studies for  $CO_2$  storage in shale reservoirs have demonstrated that  $CO_2$  can be trapped in the shale matrix and at the same time can significantly enhance the methane recovery by  $CO_2/CH_4$  competitive adsorption  $^{[\underline{Q}]}$ . Liu et al.  $^{[\underline{I0}]}$  indicated that 95% of injected  $CO_2$  can be permanently sequestered in the Devonian and Mississippian New Albany shale with gas adsorption being the dominant storage mechanism. A large storage capacity of  $CO_2$  in shale reservoirs has also been evaluated and it was estimated that the  $CO_2$  storage capacity of the Marcellus shale in the eastern United States alone could store between 10.4 and 18.4 Gt of  $CO_2$  between now and 2030  $^{[\underline{I1}]}$ .

In GCS, it is very important to study the  $CO_2$  plume evolution and migration as well as different phase transformations due to various trapping mechanisms for the sake of security. In a shale reservoir, there is one more trapping mechanism for  $CO_2$  compared to those in the deep saline aquifers, and that is the adsorption trapping of  $CO_2$  to the surface of the host rock simultaneously promoting the desorption of the in-place  $CH_4$  [12]. It is important to recall here the other well-known trapping mechanisms, namely the hydrodynamic trapping, solution trapping, mineral trapping and residual or capillary trapping. Furthermore, although all these trapping mechanisms may take effect within a given reservoir, they occur at different time scales. Moreover, only a few of these mechanisms contribute significantly to plume immobilization in time scales comparable to the injection times or arguably even over the duration of the site stewardship. On shorter time scales, hydrodynamic trapping, residual, and adsorption trapping are the dominant mechanisms that play an important role in plume immobilization in the reservoir [13][14][15][16]. In the long-term, a significant amount of  $CO_2$  will be trapped

through dissolving into the formation water (solubility trapping) and finally being permanently stored in mineral phase by reacting with the host rock (mineral trapping), which gradually begins to contribute to  $CO_2$  plume immobilization in shale reservoirs [12].

# 2. Results and Discussion

Table 1 shows the simulation cases considered and analyzed in this paper.

Table 1 Description of simulation cases

Case description	Gas adsorption	CO <sub>2</sub> injection rate/(m <sup>3</sup> /day)*	CO <sub>2</sub> injection period /(year)	CO <sub>2</sub> injection scheme	Lithology
Case 1	1	4000	30	Continuous injection	LJG sand
Case 2	R	4000	30	Continuous injection	YC shale
Case 3	R	2000	60	Continuous injection	YC shale
Case 4	R	4000	30	Huff-n-puff injection	YC shale
Case 5	R	4000	30	Water alternating gas injection	YC shale

<sup>\*</sup>  $4000 \text{ m}^3/\text{day} \approx 0.09 \text{ kg/s}$ 

#### 2.1. Comparison of CO<sub>2</sub> Storage in Shale and Deep Saline Aquifer

The cumulative levels of  $CO_2$  trapped with different mechanisms for the Yanchang (YC) shale and Liujiagou (LJG) sand from Shenhua saline aquifer in Ordos basin in China at the same  $CO_2$  injection rate are compared and plotted in Figure 1. It can be observed that with a total amount of 1861.55 Mmoles (1861.55 ×  $10^6$  moles) of  $CO_2$  injected in 30 years, 656.59 Mmoles was in the free phase, 474.66 Mmoles was adsorbed, 102.03 Mmoles was trapped in residual phase, 179.12 Mmoles was dissolved in the formation water, and the remaining 458.06 Mmoles was trapped as mineralized  $CO_2$  in shale at 500 years. For sand, 1075.36 Mmoles was in the free phase, 279.44 Mmoles was trapped through hysteresis, 155.88 Mmoles was in dissolution phase, and the rest 353.82 Mmoles was stored through  $CO_2$ —water—shale reactions. Within a timescale of <200 years, sand reservoir possesses priority in trapping  $CO_2$  not only in the free gas phase and residual phase but also in the dissolution phase as well as the mineral phase. As time goes on, the superiority of sand trapping of  $CO_2$  in the stable chemical phase is overwhelmed by shale.

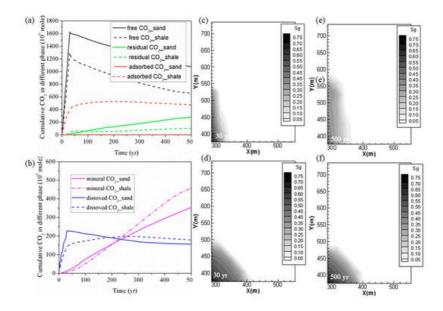


Figure 1. (a,b) Cumulative  $CO_2$  storage under different mechanisms in shale and sand; (c,e) free  $CO_2$  distributions for case 1 (YC shale) at 30 years and 500 years; (d,f) free  $CO_2$  distributions for case 2 (LJG sand) at 30 years and 500 years.

Figure 1 also displays the  $CO_2$  plume distribution at 30 years and 500 years for the sand and shale reservoir. Due to the high permeability of LJG sand compared to the YC shale, both  $CO_2$  and pressure migrate faster along the horizontal plane, and this phenomenon is discussed in detail later. However, the pressure perturbation induced by  $CO_2$  injection in the shale reservoir was constrained close to the stimulation zone. Once injection stopped, the in-place groundwater invaded the gas in the pores and micro-fractures and created the accumulation of  $CO_2$  in residual phase. The larger  $CO_2$  plume in the sand reservoir increases the interfacial area for subsequent residual trapping, dissolution and even the reaction with minerals (Figure 1(a, b)).

Although both reservoirs experience a pressure reduction response to injection stoppage, the pressure variation is neglected within the  $CO_2$  plume for the sand reservoir and the fluid flow is dominated by diffusion in horizontal plane. However, there is nearly a 17-MPa pressure difference between the injection site and the margin of the  $CO_2$  plume in shale; both advection and diffusion control the  $CO_2$  migration. As a result, the  $CO_2$  plume still expands outward for the shale but remains nearly unchanged for the saline aquifer after injection stops. It leads to wider  $CO_2$  plume at 500 years for shale than for the sand reservoir. The pressure perturbation caused by  $CO_2$  plume evolution combined with the transformation of the adsorbed phase into the dissolved phase causes the phenomenon of shale having more chemical trapping of  $CO_2$  in the longer term.

The various  $CO_2$  storage mechanisms have different operating time frames, among which the hydrodynamic and adsorption trapping take effect immediately after the  $CO_2$  injection, while the residual gas, dissolution and particularly the mineral trapping mechanisms are a slow process, and can occur over a time scale of centuries to millennia. Instead, these three mechanisms play an essential role in increasing the security and safety of  $CO_2$  geological storage [3]. In addition, different trapping mechanisms are strongly coupled and are competitive with each other, and different phases of  $CO_2$  in the reservoir inter-convert dynamically. To improve  $CO_2$  storage security as well as efficiency, the  $CO_2$  injection strategy should be optimized based on the idea of expanding  $CO_2$  plume and decrease in the percentage of  $CO_2$  in the free gaseous phase.

### 2.2. Effect of CO<sub>2</sub> Injection Rate on CO<sub>2</sub> Storage in Shale

As stated previously, to enhance the  $CO_2$  storage security in a shale reservoir by constraining the capacity of free and mobile-phase  $CO_2$  and to maintain a relatively gentle pressure perturbation, the  $CO_2$  injection strategy should be precisely designed and optimized. The effects of the  $CO_2$  injection rate on the overall performance of the sequestration project are investigated first. We do so by comparing case 2 and case 3. The same amount of  $CO_2$  is injected in both cases, but over a period of 30 years in case 2 and over a period of 60 years in case 3.

The cumulative  $CO_2$  in different phases for both cases (case 2 and case 3) is shown in Figure 2 (a,b). By comparing the deviation of the cumulative  $CO_2$  stored in different phases for case 2 and case 3 at 500 years shown in Table 2, the change in residual trapping is most dramatic with the change in the injection rate. It can be seen from Table 2 that there was a 19.52% reduction in the residual trapping of  $CO_2$  due to a decrease in the  $CO_2$  injection rate. In addition, case 3 also has more  $CO_2$  in the mobile free phase than case 2; the deviation is 38.56 Mmoles at 500 years. More  $CO_2$  exists in

the free phase to promote its horizontal migration. This result is also supported by the profile of the gas saturation in the fractures of the shale reservoir as shown in <u>Figure 2 (c-h)</u>. This profile clearly shows that the free-phase  $CO_2$  migrates further horizontally at higher  $CO_2$  injection rate especially during the period of  $CO_2$  injection.

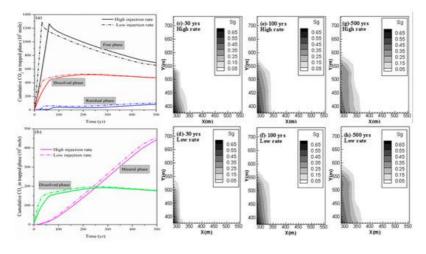


Figure 2. (a,b) Cumulative  $CO_2$  storage under different mechanisms at different  $CO_2$  injection rates; (c,e,g) free  $CO_2$  distributions for case 2 at 30 years, 100 years and 500 years; and (d,f,h) free  $CO_2$  distributions for case 3 at 30 years, 100 years and 500 years.

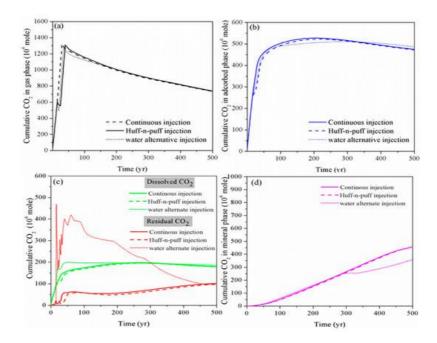
Table 2. Comparison of CO<sub>2</sub> amount in different phases for case 2 and case 3.

	Cumulative CO <sub>2</sub> Trapped under Different Mechanisms/(10 <sup>6</sup> moles)							
Case	Hydrodynamic Trapping	Adsorbed Trapping	Residual Trapping	Dissolution Trapping	Mineral Trapping			
Case2	656.59	474.66	102.03	179.12	458.06			
Case3	695.15	472.18	82.11	177.39	443.53			
Deviation	5.87%	-0.52%	-19.52%	-0.97%	3.17%			

#### 2.3. Effect of Huff-N-Puff Injection and Water Alternating Gas Injection

Finally, we investigate the performance of the  $CO_2$  sequestration project using the huff-n-puff injection scheme and the injection of alternating slugs of water and  $CO_2$  scheme, which are widely used in the oil/gas industry to enhance oil and gas production. We compare the results of case 2, case 4 and case 5. In all the three cases,  $CO_2$  is injected at a rate of 4000 m<sup>3</sup>/day over a period of 30 years. In case 2, the injection of  $CO_2$  is continuous. In case 4,  $CO_2$  is first injected for 15 years, then the well is shut-down and soaked for five years, and finally the well is opened again and injected for another 15 years. In case 5, the injection scheme is as follows:  $CO_2$  is first injected at a rate of 4000 m<sup>3</sup>/day for 15 years, water is then injected at a rate of 50 m<sup>3</sup>/day for 5 years, and finally the  $CO_2$  is injected at the rate of 4000 m<sup>3</sup>/day for another 15 years.

As shown in Figure 3, for the huff-n-puff injection scheme, the addition of  $CO_2$  soaking time has a limited impact on the performance of  $CO_2$  storage in a shale reservoir compared to the continuous injection, especially for long-term  $CO_2$  storage. However, at the beginning, the amount of free  $CO_2$  increases while the immobile  $CO_2$  in residual as well as the dissolved phase decreases for the huff-n-puff injection scheme, which is not beneficial for the storage safety of  $CO_2$ . On the other hand, the water alternating gas injection scheme can somehow reduce the free-phase  $CO_2$  as well as the adsorbed-phase  $CO_2$  by enhancing the  $CO_2$  dissolution into the formation water and trapping it in the micro-pores in the residual phase within the timescale of 300 years. However, with the continual ex-solution of  $CO_2$  from formation water in the longer term, the  $CO_2$  reaction with the host rock is also prohibited.



**Figure 3.** Cumulative  $CO_2$  storage in different storage mechanisms using various  $CO_2$  injection schemes. (a): gas phase; (b): adsorbed phase; (c): dissolved and residual phase; (d): mineral phase)

<u>Figure 4</u> shows the free-phase  $CO_2$  distributions for case 2, case 4 and case 5 at 30 years, 100 years and 500 years. It can be observed that, for case 2 and case 4, although the addition of soaking time for  $CO_2$  injection can hinder the gaseous  $CO_2$  migration in the horizontal direction, once injection stops, the migration rate is accelerated and the mobile  $CO_2$  can even move faster than in the case of the continuous injection scheme. The gaseous  $CO_2$  front in Y direction at 500 years arrives at 600 m for the huff-n-puff scenario but only at nearly 580 m for the continuous injection scenario. On the other hand, the water alternating gas injection scheme (case 5) can apparently decrease the capacity of mobile  $CO_2$  during the whole period of  $CO_2$  storage.

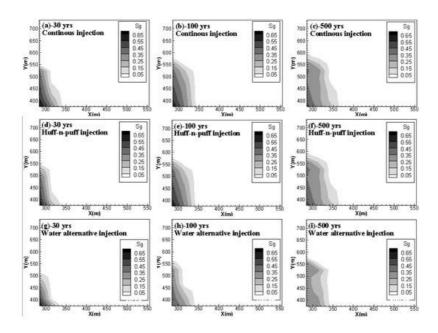


Figure 4. Free  $CO_2$  distributions for case 2, case 4 and case 5 at 30, 100 and 500 years. (**a**,**b**,**c**) compare the gas phase  $CO_2$  distribution of continuous injection scenario at 30 yrs, 100 yrs and 500 yrs, respectively; (**d**,**e**,**f**) show the gas phase  $CO_2$  distribution of huff-n-puff injection scenario at 30 yrs, 100 yrs and 500 yrs; (**g**,**h**,**i**) give gas phase  $CO_2$  distribution of water alternative injection scenario at 30 yrs, 100 yrs and 500 yrs.).

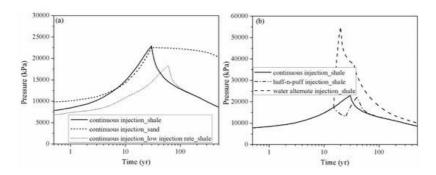
#### 2.4. Pressure Perturbation Induced by CO<sub>2</sub> Injection

The performance of  $CO_2$  storage in the subsurface is highly dependent on the pressure evolution in the formation. The adsorptive behavior of gas onto an organic substrate is largely dependent on pressure. Although there are different types of adsorption models that can be used to describe the  $CO_2$  adsorptive behavior to shale, for example the Langmuir model used for the New Albany shale [17] and the Devonian shale from the Kentucky [5], and the BET-type adsorption of  $CO_2$  onto Barnett shale [18], they all show that the  $CO_2$  adsorption capacity is a function of ambient pressure. The  $CO_2$  dissolution into the formation water is also largely impacted by pressure. Xu et al. [19] indicate that the pressure variation

in the reservoir can affect the dissolution of  $CO_2$  into the formation brine. As the volume of dissolved  $CO_2$  changes, the original chemical equilibrium between  $CO_2$  (aq.),  $H_2CO_3$ , and  $HCO_3^-$  can be re-established and the mineral reactions will also change accordingly.

Furthermore, pressure variation is also a cause for the change in residual trapping. The non-wetting gas to invade the smaller pores is driven by the higher formation pressure, and the snap-off also results in the increase in macroscopic trapping that occurs readily in smaller pores during imbibition. On the other hand, the gravity effect impacts the displacement pattern of water by  $CO_2$  for low capillary entry pressure. Compared with high-viscosity fluid, the low-viscosity gas can form more stable paths when penetrating the high permeability regions of the porous medium, and only the largest pores can be invaded to lead to reduced snap-off during an eventual imbibition process [15].

<u>Figure 5</u> shows the pressure variation at observation point #1 (X = 275 m, Y = 375 m), which is located at the injection site for case 1, case 2, case 3, case 4 and case 5. The drastic pressure build-up induced by  $CO_2$  injection in the LJG sand is larger and more lasting compared with the YC shale, which displayed with a rapid speed of pressure up and down (<u>Figure 5a</u>). The higher permeability not only enhances the fluid penetration into the rock pores and fractures, but also increases the pressure transmission through the reservoir. The pressure perturbation was constrained within the stimulation zone for the shale reservoir; however, the pressure variation was extended to the whole simulation domain for the sand cases and decreased very slowly responding to the injection well shut-in. The significant pressure deviation between the injection site and the surrounding area was the cause of  $CO_2$  plume expansion within the shale reservoir and also increased the interfacial area for subsequent  $CO_2$  dissolution and mineral trapping.



**Figure 5.** Pressure evolution at observation point # 1 (X = 275 m, Y = 375 m) for different cases. (a) compares the pressure perturbation of continuous injection scenario of shale and sand also the influence of injection rate; (b) shows the pressure build-up of continuous injection scenario, huff-n-puff injection scenario and water alternate injection scenario of shale reservoir).

The pressure build-up in case 3 at the injection point is smaller than in case 2, which significantly weakens the residual trapping, as shown in <u>Table 2</u>. The pressure decrease also leads to the release of  $CO_2$  from the formation water, which combined with gas desorption causes more  $CO_2$  to exist in the free phase. Considering pressure perturbation induced by the three  $CO_2$  injection schemes (as shown in <u>Figure 5</u>b), although the water alternating gas injection scheme can increase the  $CO_2$  storage security in a shale reservoir by trapping more  $CO_2$  in the immobile phase, it induces large pressure build-up during water injection.

### 2.5. Implication to CO<sub>2</sub> Storage Safety and Stability

Due to the high diffusivity of gaseous or supercritical  $CO_2$ , the free-phase  $CO_2$  is generally believed to be in the unstable phase, which can easily migrate into the preferential pathways such as natural or artificial fracture, unfolded fault and abandoned wells and leak from the storage site. Bachu et al. [3] state that the residual-gas trapping, dissolution, and mineralization of  $CO_2$  are essential mechanisms in increasing the security and safety of geological storage of  $CO_2$  in a saline aquifer after cessation of injection as less and less  $CO_2$  remains in the free, mobile phase over time. It is similar for  $CO_2$  storage in a shale reservoir. Figure 6 compares the  $CO_2$  storage security evolution with time for LJG sand and YC shale. It can be seen that the  $CO_2$  storage security increases with time both for shale and sand because more and more  $CO_2$  gets stored as a trapped phase over time. Although LJG sand possesses the advantage in trapping more  $CO_2$  in the residual, dissolution as well as mineral phase in the short term, this merit is overwhelmed by YC shale as time goes on. Besides, more than 20% of gaseous  $CO_2$  is trapped in the adsorbed phase; the overall unstable mobile-phase  $CO_2$  in the YC shale reservoir is significantly less than the LJG sand, which indicates that shale shows superiority in security of  $CO_2$  storage over saline aquifer.

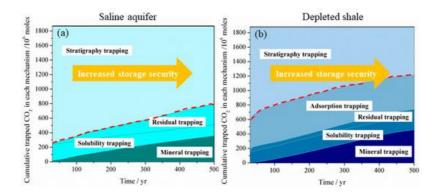


Figure 6. Storage security of CO<sub>2</sub> in (a) a deep saline aquifer and (b) in a depleted shale reservoir.

# 3. Conclusions

This study presents a comprehensive analysis of the potential of  $CO_2$  storage in a shale reservoir based on the geological parameters of Yang Chang (YC) shale in the Ordos basin of China by taking into account the Darcy and diffusive flow, gas sorption/desorption, hysteresis effects,  $CO_2$  dissolution, and  $CO_2$ -water-shale reactions. The advantage and disadvantage of  $CO_2$  storage in YC shale are analyzed by comparing them with the  $CO_2$  storage in LJG sand (saline aquifer) from the Shenhua GCS project in China. To enhance  $CO_2$  storage security in shale by constraining the capacity of free and mobile-phase  $CO_2$  and to maintain a relatively gentle pressure perturbation, different injection strategies, including the low rate continuous injection, high rate continuous injection, huff-n-puff injection and the water alternate injection are compared. The results can be summarized as follows:

- From the point of view of CO<sub>2</sub> phase transformation, CO<sub>2</sub> storage in shale can be safer than in saline aquifer by trapping more CO<sub>2</sub> in immobile phases, including adsorbed, residual, dissolution and mineral phase with lesser percentage remaining in free mobile phase in longer-term. Although, the saline aquifer has the advantage in trapping more CO<sub>2</sub> in the residual, dissolution and mineral phase in the short term.
- The pressure perturbation induced by CO<sub>2</sub> injection in the saline aquifer is longer lasting and generally larger than in the shale reservoir. The pressure build-up in shale can be rapidly released when CO<sub>2</sub> injection is stopped.
- Although the water alternating injection scheme can significantly increase the dissolution and residual phase of CO<sub>2</sub> in short to middle term, the pressure build-up caused by water injection is more drastic than other schemes. For the aim of increasing the fraction of immobile CO<sub>2</sub> while maintaining a safe pressure-perturbation, the intermittent injection procedure with multiple slugs of huff-n-puff injection can be employed to replace the continuous CO<sub>2</sub> injection. Within the allowable range of pressure increase, the CO<sub>2</sub> injection rate can be maximized to increase the CO<sub>2</sub> storage capacity and security in a shale reservoir.

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