Influence of Plasticizer´s Polarity on Mechanical Stability

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Compared with an styrene butadiene rubber (SBR) sample without plasticizer, the conductivity of mechanically unloaded oil-extended SBR samples decreases by an order of magnitude. The polarity of the plasticizer shows hardly any influence because the plasticizers only affect the distribution of the filler clusters. Under static load, the dielectric properties seem to be oil-dependent.

plasticizer mechanical stability

1. Introduction

Plasticizers are a widely used additive in rubber compounds ^{[1][2][3][4]}. They are particularly important and, as the third-highest ingredient in terms of content level, come in right after rubber and fillers. As processing aids, the plasticizers are added in different concentrations in order to impart rubber products with the desired elastic properties in the operating temperature range ^{[5][6][7][8][9][10]}.

As a fluid component, the plasticizer migrates in the rubber matrix and its macromolecules are integrated into the polymer chains through intermolecular interactions. Consequently, the intermolecular forces of the polymer chains and the number of free valences in the three-dimensional structure are reduced. The internal space between the polymer chains is thus larger, and the free volume that allows the polymer chains to flow above their glass transition temperature increases [11][12][13][14][15]. This new conformation of the polymer chains, in turn, increases their mobility and enhances the filler distribution in the rubber mixture [16][17][18][19][20][21]. Above a certain percolation threshold, a filler network is formed that reinforces the rubber compounds and provides the necessary mechanical stability [16][17]. This applies to both the carbon-based fillers such as carbon black and silica [18][19][20][21]. Indeed, the plasticizer type strongly affects the mechanical properties of rubber products due to a shift in the glass transition temperature. Consequently, the strain, the mechanical stress, the modulus of elasticity and the damping behavior change [22][23][24].

Furthermore, the dielectric properties of rubber samples filled with electrically conductive filler depend on the structure of its filler network ^{[25][26][27][28][29][30][31][32]}. This applies to filler networks made of electrically conductive fillers such as carbon-based carbon black or hybrid filler networks, provided that at least one electrically conductive filler is present ^{[25][26][27][28]}. The non-conductive component is mainly used because of its excellent mechanical reinforcement, as is the case with silica used in dynamic systems such as car tires ^{[29][30][31][32]}. Aloui et al. have shown that mechanically induced changes in the structure of the electrically conductive filler network have a direct

impact on dielectric mechanisms such as charge transport and polarization ^{[33][34]}. These, in turn, have consequences for the dielectric constant and the dielectric conductivity of rubber samples ^{[35][36][37][38][39]}.

The direct relationship between mechanical and dielectric properties makes simultaneous mechanical and dielectric analysis of rubber samples filled with electrically conductive filler an outstanding technique for opening up new horizons in evaluating the microstructure dynamics of rubber materials under mechanical load and hence reproducing authentic situations from operation modes ^{[40][41][42][43]}. In addition to quality measurements on test samples, examinations on installed end products can also be guaranteed if sensors are installed to record the current material properties during use and to monitor them in the subsequent step. Mainly the dielectric properties are used as a response to the mechanical load ^[44].

2. Excursus: Dielectric Relaxation in Elastomers

Dielectric relaxation describes the build-up of the electric polarization of a dielectric medium after application of an external electric field. The characterization of the dielectric relaxation is based on the measurement of the variation of the permittivity as a function of frequency. The permittivity stems from dipole orientation and transport of free charge carriers under the action of an electric field. The measuring method uses capacitance measurements as a function of frequency for a sample placed between two electrodes. An extensive explanation of the phenomenon and the measurement technology can be found in ^[45].

The permittivity $\varepsilon *$ is a complex function with the real part ε' and the imaginary part ε'' , also known as dielectric loss. As is typical for elastomers, not all dipoles have the same relaxation time, but different relaxation times, which exhibit a distribution with a relaxation peak. In order to describe these types of relaxation correctly, there are various empirical models derived from the Debye equation. In the case of symmetrical frequency response, the Cole–Cole approach is mainly used for amorphous dielectrics ^[46]. According to the Cole–Cole equation,

$$\varepsilon^*(\omega) = \varepsilon_{\inf} + \frac{\Delta \varepsilon}{1 + (i\omega\tau)^{\alpha}} \text{ with } 0 < \alpha \le 1$$
(1)

where ϵ inf is the infinite frequency dielectric permittivity, $\Delta\epsilon$ is the relaxation strength, α is the broadness parameter and τ is the Cole–Cole relaxation time. $\omega=2\pi$ fel is the angular frequency and fel is the electrical frequency. The expressions of ϵ' and ϵ'' take the following form:

$$\varepsilon'(\omega) = \varepsilon_{\inf} + \Delta \varepsilon \cdot \frac{1 + (\omega\tau)^{\alpha} \cos\left[\alpha \frac{\pi}{2}\right]}{1 + 2(\omega\tau)^{\alpha} \cos\left[\alpha \frac{\pi}{2}\right] + (\omega\tau)^{2\alpha}}$$
(2)

And

$$\varepsilon''(\omega) = \frac{\sigma_{dc}}{\omega\varepsilon_0} + \Delta\varepsilon \cdot \frac{(\omega\tau)^{\alpha} \sin\left[\alpha\frac{\pi}{2}\right]}{1 + 2(\omega\tau)^{\alpha} \cos\left[\alpha\frac{\pi}{2}\right] + (\omega\tau)^{2\alpha}} \tag{3}$$

where σdc is the direct current conductivity or DC conductivity [33][34].

3. Compound Preparation

Four carbon black filled SBR based compounds were prepared at Hansen and Rosenthal KG in Hamburg, Germany. The carbon black N 330 was used at a filler concentration of 60 phr. For a reference sample, no plasticizer was added. The three other samples each contain 20 phr of one plasticizer grade, which differ by polarity. Of course, the good miscibility of the plasticizers in the rubber matrix must be taken into account. Therefore, the following plasticizers are used: The plasticizers used are a paraffinic base oil (SN400), mild extraction solvate (MES) and distillate aromatic extract (DAE). **Figure 1** shows the structural formula of the plasticizers with different polarities used ^[47].



Figure 1. Structural formula of plasticizers SN400, MES and DAE.

Plasticizers SN400, MES and DAE have an aniline point in accordance with DIN ISO 2977 at 101 °C, 84 °C and 43 °C ^[47]. The aniline point is the temperature at which a homogeneous mixture of equal volumes of aniline and plasticizer separates into 2 phases during the cooling process. The degree of miscibility of aniline with the plasticizer estimates the aromatic content in the plasticizer. The lower the aniline point, the more polar the plasticizer.

The solubility parameter δ is an indicator of the miscibility quality of the various plasticizers within the SBR matrix. SN400, MES and DAE have a solubility parameter δ of 16 MPa^{1/2}, 16.7 Mpa^{1/2} and 18.5 Mpa^{1/2}. With a value of 17.2 Mpa^{1/2}, the solubility parameter δ for SBR is in the same range as for the plasticizers, implying a good compatibility ^[47].

The aniline point and the solubility parameter are shown in Figure 2.



Figure 2. Aniline point and solubility parameter of the plasticizers.

The compound formulation is shown in **Table 1**.

Table 1. Compound formulation in phr.

	No Oil	SN400	MES	DAE
SBR 1502	100	100	100	100
N 330	60	60	60	60
SN400	-	20	-	-
MES	-	-	20	-
DAE	-	-	-	20
ZnO	2.5	2.5	2.5	2.5
Stearic acid	1	1	1	1
TMQ	1	1	1	1
6PPD	1	1	1	1
CBS	1.8	1.8	1.8	1.8
DDTD	0.2	0.2	0.2	0.2
Sulphur	1.5	1.5	1.5	1.5

The antioxidants 2,2,4-Trimethyl-1,2-dihydrochinolin (TMQ) and N-(1.3-Dimethylbutyl)-N'-phenyl-pphenylenediamine (6PPD) were added at a concentration of 1 phr. The samples were sulfur-vulcanized. In addition **Beferences**e vulcanization accelerators N-cyclohexyl-2-benzothiazolesulfenamide (CBS) and Dimethyldiphenylthiuram disulfide (DDTD) were used. 1. Ni, Y.; Yang, D.; Wei, Q.; Yu, L.; Al, J.; Zhang, L. Plasticizer-induced enhanced electromechanical

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