PowderMEMS

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PowderMEMS is a powder-based microfabrication technology for substrate-level integration of three-dimensional functional microstructures into MEMS devices. The PowderMEMS process solidifies micron-sized particles via atomic layer deposition (ALD) in pre-processed cavities on planar substrates from a wide variety of materials. Low process temperatures and the absence of organic components enable back-end-of-line compatibility. The process offers numerous degrees of freedom for the design of functional MEMSs, such as a wide choice of different material properties and the precise definition of 3D volumes at the substrate level, with a defined degree of porosity. Examples of application are the integration of rare-earth magnets and porous microfluidic structures into MEMS on wafer-level.

MEMS integration	three-dime	nsional microstructu	res	integrated micromagnets
powder-based micro	ofabrication	porous MEMS	organ	ic free

1. The PowderMEMS Process

1.1. General Description of the Process and Its Features

The PowderMEMS process comprises three key steps: dry filling of molds with microfine powder, subsequent solidification of the powder via ALD, and conditioning of the substrate for further processing ^[1]. **Figure 1** schematically depicts these steps. Starting materials are planar substrates—e.g., silicon or glass wafers—with pre-structured micro-molds and a dry powder of micron-sized particles of the filling material of choice.



Figure 1. Illustration of the PowderMEMS process ^[1] by schematic drawings (**top**) and corresponding SEM micrographs of real samples, obtained from NdFeB powder (**bottom**): (**a**) Dry-filled micro-molds with particles. (**b**) Solidification of the powder bed via ALD. The blue layer in the drawing represents the ALD layer (not to scale). The surrounding substrate is not shown for clarity. In the SEM micrograph the particles (NdFeB) appear bright grey, while the surrounding ALD layer (75 nm Al_2O_3) is dark grey. (**c**) Removal of excess particles from the substrate surface to enable post-processing in a cleanroom environment.

In the first step, the molds are filled with the dry particles, as illustrated in **Figure 1**a. The utilization of dry particles in combination with a dedicated filling technique ^[2] ensures a dense and reproducible filling of molds with lateral dimensions from 20 μ m up to 4000 μ m, and a depth of up to 1000 μ m. However, due to its particulate nature, it is not possible to produce structures with a fill factor of 100% using PowderMEMS. Depending on the application, this might either be an advantage (e.g., microfluidics) or a drawback when compared to bulk material (e.g., mechanical stability).

In the second step, the loose particles are subjected to a low-temperature ALD process, as depicted in **Figure 1**b. Since the gaseous ALD precursors penetrate the voids between neighboring particles, the growing ALD layer homogeneously coats all particles in the particle bed, as well as the inner and outer surfaces of the mold. Neighboring particles are thus connected to one another at the points of contact, forming a mechanically stable porous 3D microstructure throughout the entire mold volume. Note that at this point in the process the structure remains embedded within the substrate, but can be released from the mold using an appropriate etching method (**Figure 1**b).

In the third and final step, the substrate with the integrated PowderMEMS structures is conditioned to enable further post-processing in a (MEMS-) cleanroom environment. The conditioning comprises the removal of excess particles from the surface of the substrate, as depicted in **Figure 1**c.

Since ALD is performed at comparatively low temperatures, the PowderMEMS procedure can be applied to a broad variety of powders. Solidification with AI_2O_3 is, for example, possible at temperatures between 75 °C and 300 °C via thermal ALD, using TMA and H_2O as precursors ^[3]. Apart from AI_2O_3 , solidification has already been demonstrated with SiO₂ at 300–350 °C using SIBDEA and ozone ^[4]. High-aspect-ratio thermal ALD is available for other metal oxides—such as TiO₂, V₂O₅, and ZnO—nitrides, and metals ^[5], yielding numerous ALD/powder material combinations for functional PowderMEMS structures.

Another advantage is that substrates incorporating PowderMEMS microstructures are compatible with common BEOL and MEMS production environments, and can be post-processed using standard processes of MEMS and semiconductor technology ^{[1][6]}. As solidification via ALD is performed at comparatively low temperatures, the stresses between the substrate and the 3D microstructures remain low compared to high-temperature processes such as sintering. Since no pressure is applied to the particle bed during solidification, the mold dimensions are reproduced with high precision, without shrinkage of the PowderMEMS structure. The ALD layer envelops each particle, thus protecting them efficiently from the surrounding process or application environment. Since no organic materials are involved in the PowderMEMS procedure, the 3D microstructures exhibit excellent thermal stability, surviving temperatures up to 425 °C without degradation ^[2]. To illustrate the integrability of the PowderMEMS procedure in MEMS processes, **Figure 2** displays a piezoelectric vibrational energy harvester featuring an array of permanent micromagnets fabricated from NdFeB powder at the wafer level.



Figure 2. (a) Top side of a piezoelectric energy harvester with permanent wafer-level integrated NdFeB magnets (black pixels). (b) Bottom of the silicon cantilever exhibiting the magnetic PowderMEMS structures. Each magnetic pixel is $180 \times 180 \times 500 \ \mu\text{m}^3$ in size.

1.2. Implementation of the PowderMEMS Process at Fraunhofer ISIT

Successful utilization of PowderMEMS structures in industrially relevant microsystems requires a sufficiently high level of technological maturity. For the PowderMEMS process, this especially demands the following:

• That all processes are automated, and allow for a sufficient throughput for mass production;

- That the processes are reproducible, with low variation across individual substrates, as well as from substrate to substrate;
- That non-destructive and fast characterization and process control methods are available at the substrate level;
- That the substrates can be appropriately conditioned to allow for post-processing in a common BEOLcompatible cleanroom environment after embedding the 3D microstructures.

Figure 3 illustrates how PowderMEMS microstructures are currently integrated on 8-inch silicon substrates at Fraunhofer ISIT. After creating the micro-mold pattern via DRIE in the MEMS cleanroom, the substrates are transferred into a dedicated laboratory. Here, the dry-filling procedure, the solidification via ALD, and part of the substrate conditioning are performed. The photoresist mask used for mold etching remains on the wafer as a sacrificial layer.



Figure 3. Schematic illustration of the realization of embedded functional 3D microstructures on 8-inch Si substrates, as implemented at Fraunhofer ISIT. All process steps are carried out using automated equipment, enabling industrially relevant manufacturing.

For filling of the micro-molds with particles, a novel automated procedure has been developed ^[2]. The powder is dry-filled into the cavities using a combination of low-frequency and ultrasound vibration, in conjunction with mechanical compacting of the powder. With this procedure, molds with dimensions down to 10 micrometers can be filled reproducibly. Excess powder is removed from the wafer surface with an automated squeegee.

Subsequently, the substrates are transferred into the ALD tool (Picosun R3000B), in which the loose particles are agglomerated into rigid microstructures. The wafers are placed horizontally within the reaction chamber to prevent the loose powder from falling out of the molds before solidification. Currently, six 8-inch wafers can be processed in a single batch. Deposition of 75 nm Al_2O_3 at 75 °C has proven to be a suitable solidification layer for various applications ^[1].

As the corresponding cross-sections in **Figure 3** illustrate, some excess particles remain on the substrate surface on the front side of the substrate, as well as on its backside, after mold filling. During the subsequent agglomeration process, these particles are fixed firmly to the substrate surface by the ALD solidification layer. Therefore, substrate conditioning is carried out after the ALD process. Bottom-side cleaning is performed by grinding and polishing with an automatic grinder (Disco DFG8540), as previously described in ^[6]. Approximately 25 μ m of silicon is typically removed from the bottom side of the substrates. For front-side conditioning, the photoresist mask left after DRIE is used as a sacrificial layer. After transfer of the substrates into the cleanroom, the photoresist is removed by O₂ plasma etching (Tepla barrel asher), followed by lift-off in an organic solvent and a final highvelocity spray clean (SSEC 3000 automatic spin etcher) ^[6].

After surface conditioning, the substrates can be further processed in the cleanroom if required. As already mentioned, wafers with embedded PowderMEMS microstructures are BEOL-compatible, i.e., wafer processing can be implemented on common cleanroom equipment without major process changes at process temperatures up to 425 °C. For example, to finalize the piezoelectric vibrational energy harvester shown in **Figure 2** after micromagnet integration, post-processing includes various thin-film depositions as well as wet and dry etching of metals, dielectrics, and silicon ^[8].

For magnetization of integrated magnetic structures, a custom-built wafer-level magnetization tool (MAGSYS, Dortmund, Germany) is available, which provides magnetic fields of up to 3.5 T across a whole 8-inch wafer. After loading the wafer to the tool, the substrate is automatically positioned within a coil. Subsequently, a current of up to 5.6 kA is passed through the coil for generation of the magnetic field.

1.3. Process Control

Appropriate methods to control process quality and to support process development are central to the successful use of PowderMEMS for innovative microsystems in both research and production. NdFeB-based micromagnets

have proven to be suitable as test structures for process characterization. Vibrating-sample magnetometer (VSM) measurements can be utilized to monitor the reproducibility of the PowderMEMS processes—i.e., micro-mold filling and agglomeration ^[2]—as well as for overall process development ^[Z][^{G]}. Since NdFeB is very sensitive to oxygen and water vapor, the magnetic properties precisely reflect degradation effects pertaining to the particles or the $Al_2O_3 ALD$ layer during post-processing. Of particular interest are the remanence B_r and the intrinsic coercivity H_{ci} . Since B_r depends on the amount of magnetic material, this value represents a measure of the mold-filling quality. H_{ci} is an intrinsic material property, and does not depend on the volume of a magnet. Deviating values of B_r and H_{ci} indicate an incomplete solidification of the particles or a degradation of the magnetic material due to manufacturing processes ^[Z].

However, VSM measurements are comparatively slow, and necessitate dicing of the substrate into chips. For inline process monitoring, non-destructive test methods are needed. Qualitative magnetic field measurements with sufficient lateral resolution at the wafer level can be performed by means of magneto-optical microscopy. With this measurement technique, an optical contrast based on the local magnetization is generated due to the Faraday effect. In this way, a non-destructive, fast, and automated optical and magnetic quality control within the process chain can be realized. **Figure 4**a,b display optical and magneto-optical images, respectively, of integrated NdFeB PowderMEMS microstructures. The images were acquired after wafer-level magnetization at 3.5 T. The resolution in magneto-optical mode is sufficient to resolve magnetic structures with lateral dimensions of 125 µm, as shown in **Figure 4**c. The qualitative magnetic contrast and optical inspection, including 3D topologies, enable automated and rapid quality control within the process chain, along with identification of defective magnetic microstructures.



Figure 4. (a) Optical image of NdFeB microstructures embedded in a silicon substrate. (b) The same structures imaged with a magneto-optical sensor based on the Faraday effect. The contrast corresponds to the strength of the out-of-plane component of the magnetic field. (c) Magneto-optical image of the ROI marked by a dashed frame in (b), acquired at higher magnification with a different lens.

Depending on the application requirements, and to ensure process stability, quantitative characterization of magnetic microstructures at the substrate level can be necessary. For this case, a Hall sensor setup was developed that can scan across the wafer surface at close distance. In this way, magnetic fields of test structures can be quantitatively characterized with sufficient lateral resolution to map features with dimensions of 500 µm, as shown in **Figure 5**.



Figure 5. (a) Microscope image of NdFeB microstructures embedded in a silicon substrate. (b) Scan of the same area with a 3D Hall sensor. The color code represents magnetic flux perpendicular to the substrate surface. (c) Detailed scan of the 4 × 4 array marked in red in (a), consisting of (500 × 500) μ m² magnets. The vertical distance between the Hall sensor and the substrate surface was 120 μ m.

2. Morphology of the PowderMEMS Microstructures

The 3D microstructures fabricated using the PowderMEMS technology represent a novel composite material consisting of three phases: a framework of particles that are in mutual contact, an open network of interconnected voids (pores) filled with a gas or fluid, and a continuous ALD layer separating the first two phases from one another.

Figure 6 displays SEM micrographs of an empty micro-mold pattern formed in a silicon substrate, and an identical pattern of molds with 3D microstructures agglomerated from NdFeB powder (D50 = 5 μ m) by 75 nm of ALD-Al₂O₃ at 75 °C.



Figure 6. (a) SEM micrograph of a micro-mold pattern etched into a silicon substrate with DRIE. The mold cavities are ~400 μ m deep and 125 μ m × 125 μ m in size. (b) SEM micrograph of 3D microstructures agglomerated from NdFeB powder with 5 μ m mean particle size by 75 nm ALD-Al₂O₃, using the mold shown in (a).

To visualize their morphology, a sample similar to the one shown in **Figure 6**b was exposed to XeF_2 vapor to remove the surrounding substrate material. Since XeF_2 etches silicon isotopically, the substrate material is simultaneously removed on both the top and the bottom, as illustrated in **Figure 7**a, exposing the 3D microstructures. SEM micrographs of the exposed structures are displayed in **Figure 7**b,c. From the bottom, only the ALD-Al₂O₃ layer is visible, since it covers not only the particles, but also the inner surfaces of the Si molds. At higher SEM acceleration voltages, the Al₂O₃ shell is penetrated by the electron beam, and the framework of particles beneath becomes visible (see **Figure 7**d).



Figure 7. (a) Schematic illustration of the isotropic etching in XeF_2 vapor, applied to expose 3D microstructures that are embedded in a silicon substrate. The black dotted frame on the right-hand cross-section indicates the initial dimensions of the silicon chip. SEM micrographs of the (b) top and (c) bottom sides of the NdFeB 3D microstructures shown in **Figure 6** after release etch by XeF_2 vapor. Both micrographs were obtained with an acceleration voltage of 2 kV. (d) SEM micrograph of the area within the yellow dashed frame in (c), obtained with an acceleration voltage of 20 kV.

The continuous ALD layer encloses the individual particles entirely throughout the whole volume of the particle bed, keeping them in place and providing considerable mechanical stability to the porous 3D microstructure. **Figure 8** illustrates this in more detail, displaying SEM micrographs of a focused ion beam (FIB) cross-section through a NdFeB-based 3D microstructure. In **Figure 8**b, the ALD-Al₂O₃ layer around the particles is especially apparent.



Figure 8. SEM micrographs of an FIB cut through a porous 3D microstructure agglomerated from NdFeB powder with 5 μ m mean particle size by 75 nm ALD-Al₂O₃: (a) FIB preparation overview. (b) Detailed side view of the FIB cut area within the yellow frame in (a).

To verify that neighboring particles within the framework were in mechanical point contact with one another, 3D microstructures were agglomerated from Si powder. The top surface of the substrate was then dry-polished to remove a few micrometers of both the substrate material and the solidified structure, as indicated by the blue dashed line of the left-hand cross-section in **Figure 9**a. During subsequent etching in XeF₂ vapor, both the silicon of the substrate and the particles, exposed by the polishing, were attacked. The right-hand cross-section in **Figure 9**a illustrates this principle, while the SEM micrographs in **Figure 9**b,c show the results. Within a zone of 5 μ m from the surface, the Si particles were removed, leaving the continuous ALD layer as an empty, free-standing Al₂O₃ shell. The contact points between neighboring particles remained free of Al₂O₃, as observed in ^[1]. Through those "bottlenecks", the XeF₂ proceeded from particle to particle during etching. From a depth of approximately 5 μ m below the surface, Si particles were still present that had not been etched during the limited exposure time to XeF₂ vapor.



Figure 9. (a) Schematic illustration of the procedure applied to investigate the contact points between neighboring particles. (b) SEM micrograph of an FIB cut through a 3D microstructure that has been agglomerated from Si particles with 1 μ m mean size by 75 nm ALD-Al₂O₃. After dry-polishing at the wafer level and dicing into chips, the 3D microstructure was exposed to isotropic etching in XeF₂ vapor. (c) Micrograph of the area within the dashed yellow frame in (b).

Figure 10 presents SEM micrographs of structures agglomerated from different powders using 75 nm ALD-Al₂O₃; the particles are arranged randomly. Since no mechanical pressure is applied during agglomeration, they remain unchanged in shape and size, and the pores in between the particles are preserved. As the micrographs indicate, all pores are interconnected, forming an open network of voids throughout the structure. The mean pore size and the fill factor mainly depend on the shape and size of the particles. The impact of the nanometer-thin ALD layer on the pore volume is negligible considering the micron-sized particles.



Figure 10. SEM micrographs of porous 3D microstructures solidified by 75 nm ALD-Al₂O₃ and made of powders from different materials, with varying mean particle size d: (**a**) d = 9 μ m Al₂O₃, (**b**) d = 5 μ m NdFeB, (**c**) d = 1 μ m carbonyl iron, (**d**) d = 5 μ m diamond, (**e**) d = 10 μ m oxidized silicon beads, (**f**) d = 14 μ m phosphor. Between the particles empty voids form a network of pores.

The specific morphological features of the PowderMEMS microstructures without doubt strongly impact their properties. Material parameters such as thermal or electrical conductance, mechanical stability, or the coefficient of thermal expansion cannot be simply derived from the corresponding properties of the bulk material and the ALD. Since suitable simulation models are not yet established, the material parameters must be obtained experimentally. In past research, the main attention has been paid to the durability of PowderMEMS microstructures and their integrability into MEMS processes. The evaluation of application-related properties is subject to both ongoing and future work.

3. Application of PowderMEMS

The MDPI special issue "<u>The Fabrication of Microstructures from Powders and Their Applications in Microsystems</u>" collects several works focussing on PowderMEMS fabrication and application.

3.1 Example: Integrated Permanent Rare-Earth Magnets

PowderMEMS can be utilized to fabricate high-performance, organic-free rare-earth micromagnets for magnetic MEMS. For instance, NdFeB micromagnets can be integrated into MEMS energy harvesting devices as depicted in Figure 11. The device is created in nine lithography levels combining PowderMEMS with epi-poly silicon and a piezoelectric AIN stack. In this case, the PowderMEMS process is conducted after the seventh lithography. After the integration of the magnets, 2 more lithography levels are processed in the clean room, demonstrating the back-end-of-line compatibility of the PowderMEMS process.

In general, the PowderMEMS integration can be carried out anywhere within a conventional microfabrication flow, depending on the requirements and the design of the device.



Figure 11. Example of wafer level-integration of NdFeB micromagnets into a MEMS device. **(a)** NdFeB micropowder solidified by Al2O3 into the silicon device wafer (8 inch / 200 mm). **(b)** MEMS energy harvesting device with piezoelectric AlN layer (bright grey) and NdFeB micromagnets (black). **(c)** 200 mm silicon wafer with harvester design variations. All devices contain PowderMEMS NdFeB micromagnets.

3.2 Further Applications

The wide choice of materials and customizable properties opens a multitude of applications for the PowderMEMS technology. Apart from the shape and volume of the 3D structure itself, additional application-specific physical and chemical characteristics can be controlled by choice of the particles and the ALD layer (see Figure 12). Table 1 presents a list of the applications discussed. The list is not conclusive, and provides application examples in which PowderMEMS enables the improvement and the realization of existing and novel MEMS devices, respectively.



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Application	Powder	Powder Property of Interest	ALD Layer	ALD Layer Property of Interest	the MikroSystemT solid phase suitab	echnik le for			
Magnetic	Integrated permanent magnets	NdFeB, Fe, ferrites	Hard/soft ferromagnetism	Al ₂ O ₃	Mechanical	nt			
	Energy harvesting / wake- up					uators. s and			
	Integrated inductors					uel			
Optical	Light conversion	Phosphor	Fluorescence	Al ₂ O ₃	Mechanical/optical transparency	'lin,			
Thermal	Cooling of MEMS	Si	High thermal conductivity	Al ₂ O ₃	Mechanical	CoNiP			
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	Thermal insulation	Pyrogenic SiO ₂	Low thermal conductivity	Al ₂ O ₃ /SiO ₂	Mechanical
Fluidic	Filter Mixer	Si/SiO ₂ /Si ₃ N ₄	Mechanical	Al ₂ O ₃ /SiO ₂	Mechanical
	Solid support				Adsorption of (bio)molecules
Sensors	Flow sensors	Pyrogenic SiO ₂	Low thermal conductivity	Al ₂ O ₃ /SiO ₂	Mechanical
	Gas sensors	Si/Metal	Electrical conductivity	TiO ₂	Catalysis
	Electrochemistry/biosensors	Si/metal/glassy carbon	Electrical conductivity	Metal	Electrical conductivity/adsorption of (bio)molecules