Hydraulic Actuators

Subjects: Materials Science, Composites

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Hydraulic actuators are elements converting the energy of the working fluid into mechanical energy related to the reciprocating motion. The most frequently applied materials used in power hydraulics are described, and various surface modifications of the discussed elements, which are aimed at improving the operating parameters of actuators, are presented. The most frequently used materials for actuators elements are iron alloys. However, due to rising ecological requirements, there is a tendency to looking for modern replacements to obtain the same or even better mechanical or tribological parameters. Sealing systems are manufactured mainly from thermoplastic or elastomeric polymers, which are characterized by low friction and ensure the best possible interaction of seals with the cooperating element. In the field of surface modification, among others, the issue of chromium plating of piston rods has been discussed, which, due, to the toxicity of hexavalent chromium, should be replaced by other methods of improving surface properties.

Keywords: structural materials; power hydraulics; hydraulic actuators; sealing system; coatings; surface modifications

1. Introduction

Hydraulic actuators are elements converting the energy of the working fluid into mechanical energy related to the reciprocating motion. The pressure of the working fluid acts on the piston and creates a force causing the piston assembly to move. As a result, the piston rod can perform useful work $^{[\![1]\!][\![2]\!]}$. Hydraulic actuators are an executive element in power hydraulic systems. These structures have several advantages, which include the possibility of obtaining large working forces and low operating speeds $^{[\![3]\!]}$.

The most general division of the actuators includes single-acting, double-acting, and rotary actuators $^{[4]}$. A characteristic feature of single-acting actuators is the presence of one working chamber and the possibility of executive (active) movement only in one direction. The return movement can be carried out by an external force or a spring force. Double-acting actuators, in turn, are characterized by a working stroke in both directions.

Single-acting actuators are divided into (Figure 1):

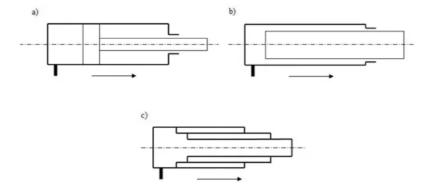


Figure 1. Types of single-acting actuators: (a) piston, (b) plunger, (c) telescopic.

- · piston actuator;
- · plunger actuator;
- · telescopic actuator.

Double acting actuators are divided into (Figure 2):

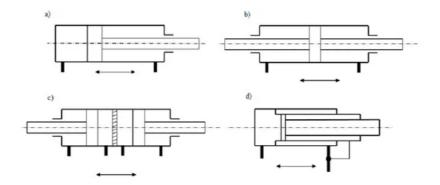


Figure 2. Types of double-acting actuators: (a) with one-sided piston rod, (b) two-sided piston rod, (c) multi-piston (double piston), (d) telescopic.

- piston actuator with one piston rod (with one-sided piston rod);
- piston actuator with two-piston rods (with double-sided piston rod);
- · multi-piston actuator;
- · telescopic actuator.

Piston actuators are the most common type of actuators. They are characterized by the fact that at the end of the piston rod on which the piston is mounted.

In a plunger actuator, there is the so-called plunger instead of the piston assembly. A telescopic actuator consists of a set of several pipes, extending one from the other—such an actuator allows obtaining large strokes.

The construction of a hydraulic actuator is described on the example of the simplest piston actuator (Figure 3).

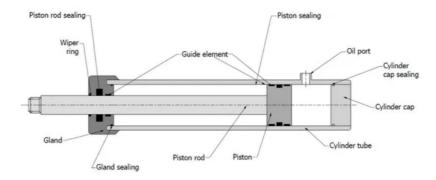


Figure 3. Design of hydraulic piston actuator.

The casing of the actuator units is a cylinder tube. Inside the tube, there is a piston rod with a piston fixed at the end. On one side, the cylinder is closed by the end cap, and on the other side, there is a so-called actuator gland [5][6].

The cylinder cap can be assembled with a pipe using a welded connection—this is the most common way. Another method is to use a threaded cap. In the case of the latter solution, it is necessary to use a static seal to ensure adequate tightness here $^{[\underline{A}][\underline{5}]}$.

The piston rod is the component that transfers the load to the receiving element. The gland is usually attached to the cylinder pipe using a threaded connection, which is why sealing between the two components is also necessary here. The gland contains the entire sealing system for the piston rod. Most often there are one or two seals to prevent the working fluid from flowing outside and a wiper ring to prevent contamination from being transferred from outside to inside the cylinder. Such a sealing system contributes to increase the life of the cylinder [5][7][8][9].

There are also guide elements of the piston rod in the gland. They must be sufficiently lubricated with the working fluid of the hydraulic system. These elements absorb radial loads and hold the piston rod axially $^{[10]}$.

The piston is usually connected to the piston rod using a thread connection. In this case, the sealing element must also be located here. Guide elements mounted on the piston transmit side forces and ensure that the piston is centred in the cylinder [5][10]. In addition to the guides, there are also sealing rings that prevent the working fluid from moving between the chambers. The piston seal acts as a pressure barrier which, for example, keeps the piston rod in a specific position

[11]. Piston seals can be single- or double-acting. The thickness of the acceptable lubricant film depends on the design of the actuator. Single-acting actuators require a small oil film; in double-acting actuators, the oil film can be slightly thicker [10]

Hydraulic actuators are used in many branches of industry, often requiring large working forces. They are used in construction and transportation equipment (excavators, forklifts, telescopic handlers, basket elevators, booms) [2][12][13]. Industries, where hydraulic cylinders are used, include mining, robotics, and aviation [6][14]. Therefore, manufacturers of actuators are outdoing each other in new material solutions and methods of improving the operational parameters of actuators.

To systematize the materials and surface modification methods used for hydraulic actuators elements, an extensive review of the existing literature has been made, which allowed for the preparation of a work presenting the current state of art in the field of hydraulic actuators manufacturing. This study focuses on several of the most important elements of hydraulic actuators: pistons, piston rods, cylinders, glands, bottoms, and seals. The most common causes of failure of these parts are described, with particular emphasis on operational factors such as abrasive wear and material fatigue. Errors during the component manufacturing stage were also noted.

In the next part, the analysis of materials used for selected parts of hydraulic cylinders was performed. Material groups such as iron alloys, light metal alloys, composites, and polymers are discussed. For each of the discussed materials, the most important mechanical properties are presented, such as tensile strength, yield strength, hardness, impact energy, or elongation at break.

2. Materials and Surface Modifications Used for Hydraulic Actuator Elements

2.1. Cylinders

2.1.1. Materials Used for Cylinders

A variety of different materials are used for the cylinders, from metal materials to composites and polymers. Most often, the cylinders are made of steel or aluminum. At pressures lower than 10 MPa, cast iron cylinders are used. At pressures higher than 20 MPa, they are made of seamless steel pipe. For pressures above 20 MPa, the pipes are made of steel or forged steel [6].

The properties of the discussed metals and polymer materials are described in <u>Table 1</u> and <u>Table 2</u>. The basic data is also presented graphically in <u>Figure 4</u>. The chart clearly shows the difference in the density of steel and polymer materials.

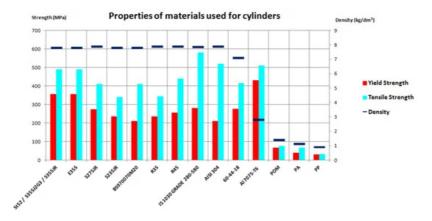


Figure 4. Chart of basic properties of the materials used for the cylinders.

Table 1. Basic properties of the materials used for cylinders.

Material	Density (kg/dm³)	Minimum Yield Strength (MPa)	Minimum Tensile Strength (MPa)	Maximum Carbon Content (%)	Description
St52/S355J2G3/S355JR	7.8	355	490	0.2	low-carbon structural steel
E355				0.22	low-carbon quality steel

Material	Density (kg/dm³)	Minimum Yield Strength (MPa)	Minimum Tensile Strength (MPa)	Maximum Carbon Content (%)	Description
S275JR	7.9	275	410	0.21	low-carbon structural steel
S235JR	7.8	235	340	0.2	low-carbon structural steel
BS970070M20	7.8	210	410	0.24	low-carbon structural steel
R35	7.9	235	345	0.16	low-carbon structural steel for pipes
R45	7.9	255	440	0.22	low-carbon structural steel for pipes
IS 1030 GRADE 280- 580	7.85	280	580	0.25	non-alloy steel, genera purpose
AISI 304	7.9	210	520	0.08	austenitic stainless stee
60-40-18	7.1	276	414	3.4–3.8	spheroidal cast iron
AI 7075-T6	2.8	430 *	510	-	Al-Zn alloy
РОМ	1.41	67–69	67–85	-	polyoxymethylene
PA	1.13	40	67	-	polyamide
PP	0.92	30	32	-	polypropylene

^{*} For aluminium alloy, instead of the yield strength R_{e} , the conventional yield strength $R_{\text{p0.2}}$ is given.

Table 2. Additional properties of the materials used for cylinders.

Material	Average Hardness	Impact Energy (J)	Elongation at Break (%)
St52/S355J2G3/S355JR	180 HB	27 (-20 °C)	22
E355	100 HB	27 (-20 C)	22
S275JR	160 HB	27 (20 °C)	22
S235JR	140 HB	27 (20 °C)	26
BS970070M20	140 HB	24 (10 °C)	21
R35	112 HB	27 (0 °C)	24
R45	142 HB	22 (20 °C)	22
IS 1030 GRADE 280-580	220 HB	22 (20 °C)	18
AISI 304	215 HB	60 (-196 °C)	45
60-40-18	160 HB	12 (-20 °C)	18
AI 7075-T6	150 HB	17 (23 °C)	10
РОМ	81 (Shore D)	-	30
PA	76-82 (Shore D)	-	20–200
PP	70-83 (Shore D)	-	150-600

One of the most popular cylinder steels is steel St 52 [15][16][17]. It is steel belonging to the grade of low-carbon structural steel. It is characterized by good weldability, machinability, and does not require special treatment for both processes. This material in the context of this application is also described in the article [18]; however, there is a designation according to European standards: S355J2G3. Similar material is also described in [19], where it appears as S355JR. The latter two types of steel differ only permanently in the temperature of the impact test, as indicated by the mark at the letter "J." Another equivalent of this steel, also used for cylinder tubes, is E355 [2]. It is quality steel, often used for tubular elements.

Cylinders are also made of S275 JR [20][21] and S235 JR [22]. Both have slightly lower yield strength than S355 (Table 1).

Cylinders made of another low-carbon steel are mentioned in [23]: BS970070M20. This material is also available under a different designation: C22E. This steel was selected for testing in this article because of its appropriate yield strength and tensile strength. Moreover, its advantage is low price. Other materials used for cylinders are unalloyed steels with a special purpose: R35 or R45 [24]. Cylinders can also be made of IS 1030 GRADE 280-580 [25] or AISI 304 stainless steel [22]. The latter, however, is used for special applications or those working in difficult conditions.

In the article ^[26], an analysis of a selection of suitable material for the cylinder pipe was carried out. After establishing requirements such as corrosion resistance, high strength, low density, good machinability, and low cost, the most optimal material was selected: spheroidal cast iron 60-40-18. It is a good choice in hydraulic systems with relatively low working pressures. Moreover, the use of cast iron allows avoiding noise caused by excessive vibrations, as this material, like any cast iron, has the ability to dampen them ^[27].

Apart from ferrous materials, the tendency to reduce mass determines the use of light metal alloys, e.g., aluminum, for cylinders. In [28], AlZnMgCu cylinders are mentioned—this is a group of aluminium alloys, in which zinc is the dominant additive. To this group belongs the material Al 7075-T6, which was described in many articles.

In [22], the steel materials were compared with Al 7075-T6 and a composite material consisting of 40% epoxy resin and 60% carbon fibers. Comparing the cylinder made of structural steel and this composite material, the mass was reduced by as much as 96% while maintaining appropriate mechanical properties. Unfortunately, the price of the composite cylinder is even several times higher than for the other materials tested. A good solution seems to be the use of aluminum, which reduces the weight of the cylinder by 91% compared to steel, and in economic terms, it more than doubles the price of the cylinder.

In $\frac{[19]}{}$, it was noted that the change of material from structural steel to Al 7075-T6 resulted in a significant reduction of the cylinder weight, which had a positive impact on the degree of the ecology of the hydraulic system as well as on its power demand. In $\frac{[21]}{}$, similar tests were carried out, but here the Al 7075-T6 aluminium pipe was wrapped in a composite consisting of epoxy resin and carbon fibers with the same proportions as in $\frac{[22]}{}$. Such a solution was chosen to avoid damage caused by seals slipping on the inner surface of the pipe. A similar construction was also discussed in works $\frac{[29]}{}$

In [30], the pipe is made from a thin S355 steel insert on the inside and is wrapped with CFRP (Carbon Fiber Reinforced Polymer) on the outside. The use of the insert was to provide the sealing system with appropriate tribological working conditions. This approach reduced the weight of the cylinder by several dozen percent. CFRP material has high strength, is resistant to corrosion and fatigue. Additionally, it has a low density. As the name suggests, it consists of carbon fibers embedded in a polymer resin, in which the carbon fibers act as a strengthening material and the polymer resin acts as a matrix holding the fibers [31]. The article [32][33] also discusses the application of CFRP to hydraulic cylinders. The paper [32] points out that the application of the composite for the cylinder pipe will allow for significantly reducing the weight; however, it will bring additional tribological problems in the piston-cylinder contact, hence the need to find a suitable method of manufacturing such cylinders. In the article [33], it was noted that in some situations steel inserts in a polymer tube may be damaged due to critical stress caused by the difference in mechanical properties of the metal and CFRP. The article notes the necessity of stiffening the structure. The application of nanostructured epoxy resin gelcoat made of Al2O3 nanoparticles inside a multilayer CFRP cylinder was proposed as a method. The inner surface of such a cylinder proved to be very durable.

The article [34][35] present prototypes of cylinders made of POM (polyoxymethylene) plastic. Such an approach was explained by many advantages of this type of materials: reduction of weight, an increase of vibration damping, and thus reduction of noise and nuisance to the environment. POM plastic shows adequate mechanical strength and heat resistance. Plastics can provide better tribological properties and resistance to aggressive environments.

In $\frac{[36]}{}$, the use of polyamide (PA) and polypropylene (PP), of which prototype hydraulic cylinders are made, is described. PA is a polymer with good mechanical properties and abrasion resistance, but can, unfortunately, absorb water. In turn, PP is a material characterized by chemical inertia and very good fatigue strength $\frac{[37]}{}$.

2.1.2. Surface Modifications of Cylinder

The inner surfaces of the cylinders are ground and honed to achieve a smooth surface. However, sometimes machining proves to be insufficient. The performance of most steels used for hydraulic cylinders is improved by additional surface modification.

In $\frac{[24]}{}$, the technology of production of hydraulic cylinders is described, which is a combination of machining and forming (burnishing). Burnishing can be carried out with simultaneous rolling of the sleeve or after the manufacturing process. It enables to skip the honing stage. Burnishing allows obtaining high smoothness of the surface layer and additionally strengthens it. The surface becomes more resistant to abrasive wear and fatigue. The pressing process is also economical as it can be carried out simultaneously with other processes.

The properties of the steel used for cylinders, such as hardness, can also be improved by carburizing $^{[23]}$. After the carburizing process, hardening is carried out, which directly leads to increased resistance. The surface layer of the steel becomes wear-resistant and retains its mechanical properties at the same time $^{[38]}$.

For special applications, the inner surface of the cylinder can be chrome plated—this is the case with telescopic cylinders, for example. Such a coating makes it possible to give it abrasion resistance.

In $^{[39]}$, the application of n-Al₂O₃/Ni–Co nanocomposite coatings on hydraulic cylinders by brush plating was mentioned to increase their resistance to wear.

Hydraulic cylinders can also be coated with zinc or tin coatings on the outside. The main role of such coatings is to give protection against corrosion. This is especially important for cylinders working outside and exposed to adverse weather conditions.

In [40], the application of DLC (Diamond-Like Carbon) coatings on hydraulic actuator tubes is also mentioned. These coatings are resistant to harmful substances, characterized by low friction coefficient and high hardness as well as resistance to wear and corrosion.

2.2. Pistons

The pistons are usually made of steel or cast iron [4]. It must be a high-quality material to allow for the longest possible trouble-free operation.

In [41], spheroidal cast iron 65-45-12 for piston application is mentioned. It is a good alternative to carbon steel. The graphite content facilitates processing. Furthermore, ductile iron is lighter than steel.

The pistons of hydraulic cylinders can be made of C35 or C45 steel [6]. These are unalloyed steels that are very easy to heat treat, but difficult to weld. Other steels are S275 JR [21], S 355 JR [19], and BS970070M20 [23]. These are structural steels already mentioned in the hydraulic cylinders. Stainless steels are used for pistons (e.g., in special purpose cylinders) [42].

Apart from ferrous materials, light metals such as Al 7075-T6 [21][30] are also used in the context of this application.

Currently, research is being conducted on the application of composite and polymer materials in pistons. The article $\frac{[34]}{}$ proposes a piston from POM.

Pistons are rarely subject to surface modifications. Sometimes it is possible to improve their surface parameters by applying DLC coatings [40].

The basic data is also presented graphically in Figure 5.

Properties of materials used for pistons

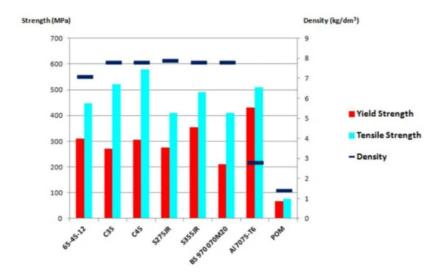


Figure 5. Chart of properties of the materials used for the pistons.

2.3. Piston Rods

2.3.1. Materials Used for Piston Rods

The piston rod, as a quite demanding element, must be made of good quality material with appropriate parameters. Both unalloyed and alloyed and even stainless steel are used for the piston rod.

In $\frac{[22]}{}$, S235 JR steel is used for the piston rod. In $\frac{[21]}{}$, steel with a slightly higher yield point was selected: S275 JR. In $\frac{[43]}{}$, the use of other structural steel was described: S355J0. Its other designation is 18G2A.

Many papers discussed piston rods made of steel C45 $\frac{[44][45][46][47]}{[48]}$. In $\frac{[6]}{[48]}$, apart from the mentioned steel, C35 is also used, and if the influence of vibrations is high, even C55 or 40Cr. In $\frac{[48]}{[48]}$, piston rods made of the equivalent steel 40Cr, 40X are used. In $\frac{[1][49]}{[48]}$, C45E is used.

The steel commonly used for the piston rod can also be 40HM (42CrMo4) $\frac{[50][30][43]}{[50][30][43]}$. Other materials are 20MnV6 $\frac{[51]}{[52]}$ 19MnVS6, 38MnVS6 $\frac{[1]}{[52]}$, or 30CrNiMo8 $\frac{[31]}{[52]}$. BS970070M20 $\frac{[23]}{[52]}$ and similar BS970070M55 (other designation: C55E) $\frac{[52]}{[52]}$ are also applied.

For more demanding applications, stainless steel is used. These are 17-4PH $^{[53]}$, AISI 304 $^{[22]}$, and AISI 410 $^{[54]}$. The latter belongs to the group of martensitic steels, which are mechanically durable and at the same time resistant to corrosion. Their resistance depends strictly on chromium and carbon content and processing conditions. Unfortunately, these materials belong to the group of soft steels $^{[55]}$.

Apart from steel, piston rods can be made of aluminium alloys $^{[28]}$. In $^{[20][22][21]}$, the piston rod is made of Al 7075-T6. In $^{[34]}$, the piston rod is made of POM. Another material, still in the testing phase, is a composite of epoxy resin and carbon fibers $^{[22]}$.

The basic data is also presented graphically in Figure 6.

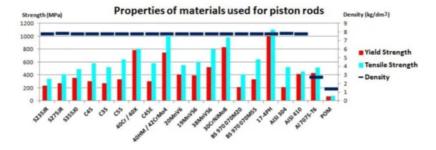


Figure 6. Chart of properties of the materials used for the piston rods.

2.3.2. Surface Modifications of Piston Rods

The surface of the piston rod is modified very often by heat- and heat-chemical treatment or by coating.

In $\frac{[52][56]}{}$, quenching and tempering was proposed as a treatment for the piston rod. Improvement is a process of combining hardening and high tempering. Its aim is to achieve high impact strength and ductility with appropriate hardness and strength values $\frac{[57]}{}$.

In [58], there is talk about induction hardening of the hydraulic cylinder piston rod. This method allows increasing surface resistance to damage. In [53], the precipitation hardening was proposed to improve the surface parameters of the piston rods and obtain high strength of the layer.

Among the coatings, a definitely basic modification is hard chromium plating $\frac{[4][9][49][59][48][60]}{[4][59][48][60]}$. Such a coating is applied electrolytically in a bath $\frac{[61]}{[61]}$. The action of direct current causes the deposition of metal ions of the coating on the steel surface.

Chromium plating allows obtaining a coating resistant to wear and corrosion, even in aggressive environments. The hard chrome layers are characterized by high hardness and low friction. However, the accuracy of application is important, as there is a risk of micro-cracks weakening the properties of coatings $\frac{[62]}{}$. The solution may be to apply a layer of nickel under the chromium layer, which additionally improves the corrosion resistance $\frac{[49]}{}$.

Unfortunately, chromium coatings have their disadvantages. Already during the coating process, there is a risk of chrome poisoning by the process personnel. This metal is toxic and may cause respiratory damage, asthma, or cancer [63]. The process absorbs large amounts of energy and generates dangerous waste, which is difficult to utilize [64]. In many countries, it is recommended to abandon hexavalent chromium coatings by standards introducing limits for this element or completely banning its use in some applications [65][66][67]. Hence, there is a need to find alternatives to this method of surface modification.

The issue of alternative surface modifications is described in detail in the article [65]. The main method is the use of one of the varieties of thermal spraying—HVOF (High Velocity Oxygen Fuel) process, which can give corrosion and wear resistance even better than galvanic chromium plating. This method is based on the fact that the particles of the applied material are raised in a gas stream with a speed several times higher than the speed of sound. Such high speed allows limiting unfavourable changes in the chemical composition of these particles. Accelerated particles affect the surface of the substrate and result in a coating [38][68]. This method can be used to obtain homogeneous coatings with low porosity, good adhesion to the substrate, and high strength. The process is more efficient than galvanic chromium plating and does not produce so much waste. However, the cost may be even twice as high as for electrolytic chromium plating [64][65][67]

Examples of coatings used on piston rods produced by HVOF and giving similar features as electrolytic chrome plating are: WC-10Co-4Cr, Cr_3C_2 -NiCr, and WC/Co/Cr $^{[65]}$.

Another alternative is APS (Atmospheric Plasma Spraying). The process allows obtaining coatings of similar structure and porosity to HVOF. It consists of melting the material for the coating in electric arc plasma [38]. In the case of plasma spraying, it is possible to combine materials in one layer and control the parameters of the coating relatively precisely. Plasma spraying has the advantage over HVOF that it can also be used for internal surfaces, such as cylinders. Coatings that can be applied to the piston rod using the APS method are, e.g., Cr_2O_3 — SiO_2 — TiO_2 [65].

HVOF coating as an alternative to chromium plating is also given in [47]. The possibility of applying Fe/TiC coatings produced with HVOF to the piston rods was investigated, and its properties were compared with hard chromium coatings applied electrolytically and with WC/CoCr coatings applied with HVAF (High Velocity Air Fuel) process. Studies have shown that Fe/TiC coatings showed similar anti-wear and anti-corrosion properties as the reference coatings, but their application was much more economical. The method of thermal spraying for modification of the piston rod surface was also mentioned in [56].

In [70], it was noted that the application of protective layers melted from cored wires (CW) under the flux layer is more ecological and economical than galvanic chromium plating. The article examines different layers embedded in the mentioned technology, differing in phase structure. It was shown that with an increase in the percentage of ferrite in the structure, the corrosion resistance of the austenitic matrix increases. Among the investigated coatings, the most resistant to corrosion turned out to be the core wire coating with an only ferritic matrix structure.

In [59], the application of CVD (Chemical Vapour Deposition) and PVD (Physical Vapour Deposition) coatings, laser coating, and thermal spraying were indicated as an alternative to chromium plating. Surface treatment technologies are also proposed as a combination of gas nitrocarbonation, plasma nitrocarbonation, and oxidation. This provides a layer that protects against corrosion and wear and has tribological parameters. Nitrided piston rods were also mentioned in [43].

In [71], it was proposed to apply a nanostructured tungsten carbide coating deposited with CVD on metal elements in contact with seals in order to minimize possible leaks, among others in actuators. Such a coating allows obtaining high resistance to abrasion and corrosion and general protection of surface roughness parameters of the substrate. All this has a positive effect on the durability of seals. It has been noted that this coating can also be a very good alternative to hard chrome coatings.

In $^{[39]}$, as an alternative to chromium coatings on the piston rod, a n-Al₂O₃/Ni–Co nanocomposite coating produced in the process of brush plating was proposed. This method belongs to galvanic methods. It can be used to repair damages in chromium plated piston rods. Such a coating gives much higher wear resistance and is tribologically similar to hard chromium coatings.

In [45], the method of repairing piston rods that have been corroded by powder welding (Plasma-Powder Surfacing) with a Fe–C–Cr–V coating is described. Conventional arc welding (AS, Arc Surfacing) could not be applied due to the risk of deformation of a relatively small diameter bar. Corrosion-resistant material, chrome-vanadium cast iron 315Kh19F3 grade was used as a padding weld.

In [72], the application of DLC coatings for hydraulic actuator components, which are covered by the concept of sliding motion, was examined. An example of such an element is the piston rod. In [40], the application of DLC coatings for the piston rod of a hydraulic cylinder used in construction machines was mentioned. It was related to very good parameters of these coatings in terms of resistance to wear and aggressive environment [73].

In $\frac{[74]}{}$, the DLC coating was compared with TiN coating. Both are characterized by high mechanical strength. TiN has better wear resistance, but DLC has better tribology and corrosion resistance.

2.4. End Caps and Glands

Glands and end caps of hydraulic actuators are described and tested relatively rarely. Both of these elements are indirectly responsible for the tightness of the actuator, so great care must also be taken to manufacture them.

The caps are often made of the same material as the cylinder. This can be low carbon steel S355 [30], S355 JR [2], or S275 JR [21]. In [20][21], Al 7075-T6 alloy is additionally proposed for this element.

In the work $^{[25]}$, IS 1030 GRADE 280-580 was used for the cylinder cap. In $^{[23]}$, BS970070M20 was proposed. The article $^{[4]}$ also mentions the cast iron caps. Quite a modern and still being tested material is POM $^{[34][35]}$ —such elements are used for cylinders made of plastic.

As far as the gland is concerned, it can be made of steel or aluminum. The gland made of S275 JR steel is described in [21]. In industry, these parts are also made of C45, 42CRMo4, AISI 304, or G25 cast iron.

Aluminum Al 7075-T6 for glands was used in [20][21][30]. In [34], the application of POM type plastic is mentioned.

When it comes to surface treatment, glands can sometimes be modified with chromium-containing coatings, which protect the elements against corrosion [65]. The basic data is also presented graphically in <u>Figure 7</u>.

Properties of materials used for end caps and glands

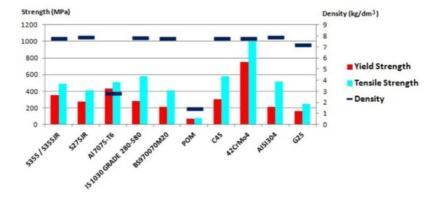


Figure 7. Chart of properties of the materials used for the end caps and glands.

References

- 1. Bohman, E. Understanding Buckling Strength of Hydraulic Cylinders. The Hydraulics & Pneumatics Article 2017. Available online: (accessed on 8 January 2021).
- 2. Nicoletto, G.; Marin, T. Failure of a heavy-duty hydraulic cylinder and its fatigue re-design. Eng. Fail. Anal. 2011, 18, 1030–1036.
- 3. Uzny, S.; Kutrowski, Ł. Strength analysis of a telescopic hydraulic cylinder elastically mounted on both ends. J. Appl. Math. Comput. Mech. 2019, 18, 89–96.
- 4. Osiecki, A. Hydrostatyczny Napęd Maszyn, 1st ed.; Wydawnictwa Naukowo-Techniczne: Warsaw, Poland, 1998; pp. 199–216.
- 5. Bauer, W. Hydropneumatic Suspension Systems, 1st ed.; Springer-Verlag Berlin Heidelberg: Berlin, Germany, 2011; pp. 95–140.
- 6. Luo, P.; Hu, J.; Tan, S. Design and Realization of Hydraulic Cylinder. Reg. Water Conserv. 2018, 1, 27–34.
- 7. Huang, Y.; Salant, R.F. Numerical analysis of a hydraulic rod seal: Flooded vs. starved conditions. Tribol. Int. 2015, 92, 577–584.
- 8. Sealing system for piston rods. Seal. Technol. 1995, 18, 4.
- 9. Peppiatt, N.; Seals, H. The influence of the rod wiper on the leakage from a hydraulic cylinder gland. Seal. Technol. 2003, 12, 5–8.
- 10. McBride, T. Seals for Hydraulic Cylinders. The Hydraulics & Pneumatics Article 2019. Available online: (accessed on 8 January 2021).
- 11. Barth, S. Sealing the Deal in Hydraulic Cylinders. P.I. Process Instrumentation Article 2018. Available online: (accessed on 8 January 2021).
- 12. Uzny, S.; Kutrowski, Ł. Obciążalność rozsuniętego teleskopowego siłownika hydraulicznego przy uwzględnieniu wyboczenia oraz wytężenia materiału. Modelowanie Inżynierskie 2018, 37, 125–131.
- 13. Kowalski, K.; Złoto, T. Exploitation and Repair of Hydraulic Cylinders Used in Mobile Machinery. Teka Comm. Mot. Energetics Agric. 2014, 14, 53–58.
- 14. Chalamoński, M. Równomierność ruchu tłoka siłownika hydraulicznego. Diagnostyka 2004, 30, 97–100.
- 15. Jakubczak, H.; Rojek, J. Zmęczeniowe pękanie siłowników hydraulicznych. Diagnostyka 2005, 36, 61-66.
- 16. Bednarek, T.; Sosnowski, W. Practical fatigue analysis of hydraulic cylinders—Part II, damage mechanics approach. Int. J. Fatigue 2010, 32, 1591–1599.
- 17. Marczewska, I.; Bednarek, T.; Marczewski, A.; Sosnowski, W.; Jakubczak, H.; Rojek, J. Practical fatigue analysis of hydraulic cylinders and some design recommendations. Int. J. Fatigue 2006, 28, 1739–1751.
- 18. Dašić, P.; Manđuka, A.; Pantić, R. Research of optimal parameters of machining big hydraulic cylinders from the aspect of quality. In Annals of the Oradea University—Fascicle of Management and Technological Engineering VII (XVII); Editura Universității din Oradea: Oradea, Romania, 2008; pp. 1563–1571.
- 19. Formicola, R.; Solazzi, L.; Buffoli, A. The Multi-Parametric Weight Optimization of a Hydraulic Actuator. Actuators 2020, 9. 60.
- 20. Solazzi, L. Design and experimental tests on hydraulic actuator made of composite material. Compos. Struct. 2020, 232, 111544.
- 21. Solazzi, L. Feasibility study of hydraulic cylinder subject to high pressure made of aluminum alloy and composite material. Compos. Struct. 2019, 209, 739–746.
- 22. Solazzi, L.; Buffoli, A. Telescopic Hydraulic Cylinder Made of Composite Material. Appl. Compos. Mater. 2019, 26, 1189–1206.
- 23. Boye, T.; Adeyemi, O.; Emagbetere, E. Design and Finite Element Analysis of Double—Acting, Double—Ends Hydraulic Cylinder for Industrial Automation Application. Am. J. Eng. Res. 2017, 6, 131–138.
- 24. Przybylski, W. Zastosowanie obróbki nagniataniem w technologii siłowników hydraulicznych. Postępy Nauk. I Tech. 2011, 6, 196–201.
- 25. Balavignesh, V.N.; Balasubramaniam, B.; Kotkunde, N. Numerical investigations of fracture parameters for a cracked hydraulic cylinder barrel and its redesign. Mater. Today Proc. Part A 2017, 4, 927–936.
- 26. Otsima, M. Material Selection Process for Hydraulic Cylinder. Eat309 Mechanical Design. Part 5, Materials Review and Selection. 2015. Available online: (accessed on 13 March 2021).

- 27. Pawłowski, W.; Kępczak, N. Teoretyczne badania właściwości dynamicznych łóż obrabiarki wykonanych z żeliwa i hybrydowego połączenia żeliwa z odlewem mineralnym. Mechanik 2015, 8, 199–203.
- 28. Tubielewicz, K.; Turczyński, K.; Szyguła, M.; Chlebek, D.; Michalczuk, H. Indywidualny siłownik hydrauliczny wykonany ze stopów lekkich. Mechanik 2015, 7, 907–912.
- 29. Solazzi, L. Stress variability in multilayer composite hydraulic cylinder. Compos. Struct. 2021, 259, 113249.
- 30. Mantovani, S. Feasibility Analysis of a Double-Acting Composite Cylinder in High-Pressure Loading Conditions for Fluid Power Applications. Appl. Sci. 2020, 10, 826.
- 31. Liu, Y.; Zwingmann, B.; Schlaich, M. Carbon Fiber Reinforced Polymer for Cable Structures—A Review. Polymers 2015, 7, 2078–2099.
- 32. Lubecki, M. Selected design issues in hydraulic cylinder made of composite materials. In Badania i Rozwój Młodych Naukowców w Polsce: Nauki Techniczne i Inżynieryjne: Materiały, Polimery, Kompozyty; Leśny, J., Chojnicki, B.H., Panfil, M., Nyćkowiak, J., Eds.; Młodzi Naukowcy: Poznań, Poland, 2019.
- 33. Scholz, S.; Kroll, L. Nanocomposite glide surfaces for FRP hydraulic cylinders—Evaluation and test. Compos. Part B Eng. 2014, 61, 207–213.
- 34. Stryczek, P.; Przystupa, F.; Banaś, M. Research on series of hydraulic cylinders made of plastics. In Proceedings of the 2018 Global Fluid Power Society PhD Symposium, Samara, Russia, 18–20 July 2018; p. 47.
- 35. Stryczek, J.; Banaś, M.; Krawczyk, J.; Marciniak, L.; Stryczek, P. The Fluid Power Elements and Systems Made of Plastics. Procedia Eng. 2017, 176, 600–609.
- 36. Harnisch, M. Kunststoffe n fluidtechnischen Antrieben. Oelhydraulik Und Pneum. 2013, 11–12, 14–16.
- 37. Dobrzański, L.A. Podstawy Nauki o Materiałach i Metaloznawstwo, 2nd ed.; Wydawnictwa Naukowo-Techniczne: Warsaw, Poland, 2006; pp. 523–684, 947–1053.
- 38. Kula, P. Inżynieria Warstwy Wierzchniej, 1st ed.; Monografie: Łodź, Poland, 2000; pp. 79–243.
- 39. Wang, H.; Ma, G.; Xu, B.; Yong, Q.; He, P. Design and application of friction pair surface modification coating for remanufacturing. Friction 2017, 5, 351–360.
- 40. Walczak, P. Analiza modelu matematycznego układu sterowania kierownicą turbiny wodnej małej mocy. Logistyka 2014, 6, 10823–10831.
- 41. O'Rourke, B. Pressure Ratings and Design Guidelines for Ductile Iron Manifolds. In 2014 IFPE Technical Conference: Where All the Solutions Come Together and Connections Are Made; NFPA: Las Vegas, NV, USA, 2014.
- 42. Krawczyk, J.; Stryczek, J. Układ hydrauliczny z elementami wykonanymi z tworzyw sztucznych. Górnictwo Odkryw. 2013, 54, 52–57.
- 43. Wach, P.; Michalski, J.; Tacikowski, J.; Kowalski, S.; Betiuk, M. Gazowe azotowanie i jego odmiany w przemysłowych zastosowaniach. Inżynieria Mater. 2008, 29, 808–811.
- 44. Knez, M.; Glodež, S.; Kramberger, J. Fatigue assessment of piston rod threaded end. Eng. Fail. Anal. 2009, 16, 1977–1982.
- 45. Nefed'ev, S.P.; Dema, R.R.; Kharchenko, M.V.; Pelymskaya, I.S.; Romanenko, D.N.; Zhuravlev, G.M. Experience in Restoring Hydraulic Cylinder Rods by Plasma Powder Surfacing. Chem. Pet. Eng. 2017, 52, 785–789.
- 46. Dai, L.-Y.; Lin, S.-F.; Yang, S.-Z.; Pan, G.-F.; Guo, N.; Dai, L.-L. Cracking cause analysis of 45 steel piston rod. Heat Treat. Met. 2011, 36, 119–121.
- 47. Bobzin, K.; Öte, M.; Linke, T.F.; Malik, K.M. Wear and Corrosion Resistance of Fe-Based Coatings Reinforced by TiC Particles for Application in Hydraulic Systems. J. Therm. Spray Technol. 2015, 25, 365–374.
- 48. Sevagin, S.; Mnatsakanyan, V.U. Ensuring the required manufacturing quality of hydraulic-cylinder rods in mining machines. In IOP Conference Series: Materials Science and Engineering 2019; Institute of Physics Publishing: Sevastopol, Russia, 2020; p. 4.
- 49. Israelson, P. Better Steels Make Better Cylinders. The Hydraulics & Pneumatics Article 2016. Available online: (accessed on 8 January 2021).
- 50. Tavares, S.M.O.; Viriato, N.; Vaz, M.; de Castro, P.M.S.T. Failure analysis of the rod of a hydraulic cylinder. Procedia Struct. Integr. 2016, 1, 173–180.
- 51. Kawiak, M. Spawanie tłoczyska siłowników hydraulicznych. Przegląd Spaw. 2013, 85, 6-10.
- 52. Rütti, T.F.; Wentzel, E.J. Investigation of failed actuator piston rods. In Failure Analysis Case Studies II; Jones, D.R.H., Ed.; Pergamon: Oxford, UK, 2001; pp. 139–146.

- 53. Tian, J.; Wang, W.; Yan, W.; Jiang, Z.; Shan, Y.; Yang, K. Microstructure characteristics of segregation zone in 17-4PH stainless steel piston rod. J. Iron Steel Res. Int. 2017, 24, 718–723.
- 54. Moreira, D.C.; Furtado, H.C.; Buarque, J.S.; Cardoso, B.R.; Merlin, B.; Moreira, D.D.C. Failure analysis of AISI 410 stainless-steel piston rod in spillway floodgate. Eng. Fail. Anal. 2019, 97, 506–517.
- 55. Xi, Y.; Liu, D.; Han, D. Improvement of corrosion and wear resistances of AISI 420 martensitic stainless steel using plasma nitriding at low temperature. Surf. Coat. Technol. 2008, 202, 2577–2583.
- 56. Tuominen, J.; Näkki, J.; Pajukoski, H.; Miettinen, J.; Peltola, T.; Vuoristo, P. Wear and corrosion resistant laser coatings for hydraulic piston rods. J. Laser Appl. 2015, 27, 022009.
- 57. Deng, X.; Ju, D. Modeling and Simulation of Quenching and Tempering Process in steels. Phys. Procedia 2013, 50, 368–374.
- 58. Awad, M.; Hultgren, J.; Roberts, W. Increased Resistance to Buckling of Piston Rods Through Induction Hardening, OVAKO Article 2018. Available online: (accessed on 8 January 2021).
- 59. Papatheodorou, T.; Hannifin, P. Influence of hard chrome plated rod surface treatments on sealing behavior of hydraulic rod seals. Seal. Technol. 2005, 4, 5–10.
- 60. Gayathri, N.; Karthick, N.; Shanmuganathan, V.K.; Adhithyan, T.R.; Madhan Kumar, T.; Gopalakrishnan, J. Productivity Improvement and Cost Reduction in Hydraulic Cylinders. Int. J. Eng. Technol. 2018, 7, 382–384.
- 61. Veeman, D.; Jagadeesha, T. Tribological characterization of electrolytic hard chrome & WC-C0 coatings. Mater. Today Proc. 2020.
- 62. Podgornik, B.; Massler, O.; Kafexhiu, F.; Sedlaček, M. Crack density and tribological performance of hard-chrome coatings. Tribol. Int. 2018, 121, 333–340.
- 63. Schneider, B.C.; Constant, S.L.; Patierno, S.R.; Jurjus, R.A.; Ceryak, S.M. Exposure to particulate hexavalent chromium exacerbates allergic asthma pathology. Toxicol. Appl. Pharm. 2012, 259, 38–44.
- 64. Vardelle, A.M. LCA F18 Hard chrome and HVOF coating. In Proceedings of the International Thermal Spray Conference and Exposition 2008—ASM Thermal Spray Society, Maastricht, The Netherlands, 2–4 June 2008.
- 65. Flitney, B. Alternatives to chrome for hydraulic actuators. Seal. Technol. 2007, 10, 8-12.
- 66. Bolelli, G.; Giovanardi, R.; Lusvarghi, L.; Manfredini, T. Corrosion resistance of HVOF-sprayed coatings for hard chrome replacement. Corros. Sci. 2006, 48, 3375–3397.
- 67. Picas, J.A.; Forn, A.; Matthäus, G. HVOF coatings as an alternative to hard chrome for pistons and valves. Wear 2006, 261, 477–484.
- 68. Hackett, C.; Settles, G. The High-Velocity Oxy-Fuel (HVOF) thermal spray—Materials processing from a gas dynamics perspective. In Proceedings of the Fluid Dynamic Conference, San Diego, CA, USA, 19–22 June 1995.
- 69. Hutsaylyuk, V.; Student, M.M.; Zadorozhna, K.; Student, O.; Veselivska, H.; Gvosdetskii, V.; Maruschak, P.; Pokhmurska, H. Improvement of wear resistance of aluminum alloy by HVOF method. J. Mater. Res. Technol. 2020, 9, 16367–16377.
- 70. Holyakevych, A.A.; Orlov, L.M.; Pokhmurs'ka, H.V.; Student, M.M.; Chervins'ka, N.R.; Khyl'ko, O.V. Influence of the Phase Composition of the Layers Deposited on the Rods of Hydraulic Cylinders on Their Local Corrosion. Mater. Sci. 2015, 50, 740–747.
- 71. Zhuk, Y. Nanostructured CVD Tungsten Carbide Coating on Aircraft Actuators and Gearbox Shafts Reduces Oil Leakage and Improves Durability. J. Mater. Eng. Perform. 2019, 28, 1914–1923.
- 72. Tonelli, L.; Martini, C.; Ceschini, L. Improvement of wear resistance of components for hydraulic actuators: Dry sliding tests for coating selection and bench tests for final assessment. Tribol. Int. 2017, 115, 154–164.
- 73. Madej, M.; Ozimina, D.; Pająk, M. Właściwości powłok węglowych uzyskiwanych w procesach fizycznego osadzania z fazy gazowej. Mechanik 2015, 88, 151–156.
- 74. Dalibón, E.L.; Pecina, J.N.; Moscatelli, M.N.; Ramírez Ramos, M.A.; Trava-Airoldi, V.J.; Brühl, S.P. Mechanical and Corrosion Behaviour of DLC and TiN Coatings Deposited on Martensitic Stainless Steel. J. Bio-Tribo-Corros. 2019, 5, 34.