

Polymer 3D Printing

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Contributor: Paul F Egan

Polymer 3D printing is an emerging technology with recent research translating towards increased use in diverse industries. The polymer 3D printing process works by depositing a polymer in a directed fashion to form a completed part, generally through layer by layer deposition. Polymer printing is advantageous because it enables printing low-cost functional parts with diverse properties and capabilities. An important aspect polymer 3D printing is the consideration of materials, processes, and design strategies that all influence a parts performance. Research in materials has led to the development of polymers with advantageous characteristics for mechanics and biocompatibility, with tuning of mechanical properties achieved by altering printing process parameters. Suitable polymer printing processes include extrusion, resin, and powder 3D printing, which enable directed material deposition for the design of advantageous and customized architectures. Through careful consideration of material, process, and design it is possible to create a 3D printed polymer part of complex geometry that is tuned for a specific application on a per-print basis.

[3D printing](#)[additive manufacturing](#)[materials](#)[polymers](#)[design](#)[lattices](#)[mechanics](#)[simulation](#)[engineering](#)[medical](#)

1. Introduction

Polymer 3D (three-dimensional) printing has advanced rapidly in recent years with many areas of research now translating to engineered products, especially in medical fields [\[1\]\[2\]\[3\]\[4\]](#). Polymer printing is advantageous for a broad range of medical areas that benefit from the diversity of polymer material characteristics and processing approaches [\[5\]\[6\]\[7\]\[8\]](#). 3D printing is a highly desirable fabrication approach because it enables the construction of designs with complex geometries and architectures that are not possible with conventional manufacturing processes. For instance, tissue scaffold structures fabricated with polyjet and stereolithography printing can achieve hierarchical forms that mimic bone, thereby providing a mechanical and biological niche to support tissue regeneration [\[9\]\[10\]](#). Additionally, the selection of polymers has advantages over metal printing approaches, that result in metal implants that do not degrade in the body and lead to mechanical issues such as stress shielding [\[11\]](#). In areas of safety equipment, polymer-printed lattices achieve efficient energy absorption with a rapid fabrication process that bypasses the supply chain limitations of bulk manufacturing [\[12\]\[13\]](#). Polymer printing is possible using extrusion, resin, and powder 3D printing processes that provide versatility for material selection and supporting designs with diverse architectures, responses, and layouts [\[14\]\[15\]](#). Because of the large design space offered by 3D polymer printing, and its opportunities for improving medical applications, we carried out a critical review by

considering recent advances in materials, processes, and design strategies that all influence an application's outcome [16], as illustrated in [Figure 1](#) for a tissue scaffold example.

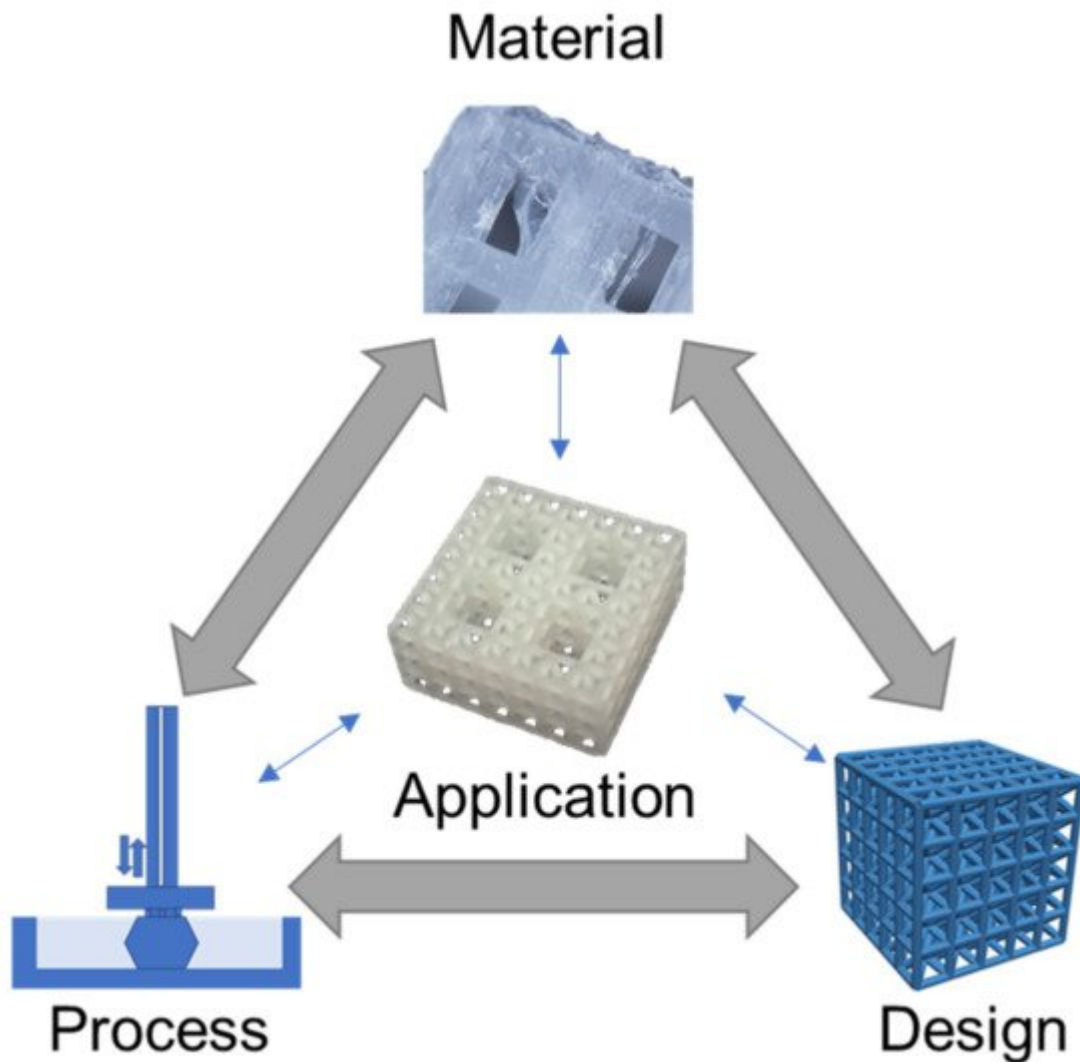


Figure 1. Material, process, and design considerations for medical applications, illustrated for a tissue scaffold example [17]. Images adapted with permission.

The [Figure 1](#) schematic highlights a hierarchical tissue scaffold constructed from beam-based unit cells with interconnected considerations in materials, process, and design for ensuring appropriate mechanical and biological functioning [17]. In this example, a design strategy for mimicking the hierarchical structure of bone largely drove the need for a suitable printing process and material selection to support the application. The material choice was dictated by a need for appropriate stiffness to ensure structural integrity while retaining biocompatibility to promote tissue growth, which was fulfilled with a methacrylic acid-based polymer. The printing process requires the formation of layers for building the complicated hierarchical truss structure, which was achieved by stereolithography printing. However, once these factors are selected, there is a need to iterate and refine the structure's design based on performance variability attributed to uncertainty and part variation in the 3D printing process [9][18].

Comparative studies for tissue scaffolds can achieve widely different design strategies based on different material/printing process decisions. For instance, tissue scaffolds constructed from polycaprolactone (PCL) using fused deposition modeling have more compliant structures with biodegradability, while titanium scaffolds printed with selective laser sintering have a higher stiffness, but no biodegradability [19][20]. These choices then influence the scaffold's topological design, since it is generally not feasible to print polycaprolactone as a truss-based structure, whereas selective laser sintering processes are able to produce titanium in forms to achieve mechanically efficient truss-based structures that promote high porosity for large void volumes for tissue growth.

Generally, decisions across material, process, and design strategies occur in a nonlinear and integrated fashion that requires careful consideration and knowledge of their relation to an application. Here, materials, process, and design strategies for polymer printing are reviewed in the context of medical applications, with a critical assessment for how each of these decision factors influence applications and one another. Initially, materials are reviewed to highlight their capabilities and properties, with data presented to compare diverse materials available for mechanical applications. Reviews on printing processes include extrusion, resin, and powder printing, which are among the most common approaches for polymer printing, with considerations for how processing influences part fidelity and functionality. The investigation of design strategies provides an overview for organizing processed materials that is advantageous for tuning application performance. Considered applications include prosthetics, safety equipment, and drug delivery, which provide context for how fundamental research in these areas translates to medical scenarios.

2. Material Capabilities

Material capabilities of polymers for 3D printing are informed by their molecular structures, and also depend on a material's processing during printing. The selection of materials for design applications is often conducted by considering measurable properties, such as mechanical properties, with ranges based on processing and testing methods that provide further complications in predicting part performance during the system design.

2.1. Material Structure

There is a broad range of polymer materials for 3D printing, with capabilities informed from their molecular structure, with polymers processed in different manners for each printing process. In extrusion processes, thermoplastics are commonly used for 3D printing where they are melted for extrusion followed by hardening after deposition [21]. For example, acrylonitrile butadiene styrene (ABS) is a common thermoplastic that exhibits favorable impact strength and improved chemical resistance compared to pure polystyrene [22]. The properties of ABS are tunable based on the ratio of its three monomers, for instance, its density may range from 1.05 mg/m³ to 1.07 mg/m³ with resulting tensile moduli from 2.5 GPa to 2.7 GPa. Acrylonitrile styrene acrylate (ASA) is an alternative to ABS with improved heat resistance and exceptional ultraviolet stability [23], while polylactic acid (PLA) is another popular thermoplastic with biocompatibility but a lower glass transition temperature.

PLA is also suitable for further types of printing processes, such as resin curing with stereolithography [24], which enables the construction of more complex part architectures than is generally possible with extrusion processes. Although PLA is biocompatible, there is some concern for toxicity in stereolithography printed PLA because of the addition of photopolymers to the resin solution, which is necessary for cross-linking monomers to form polymers in the presence of ultraviolet light. However, when properly printed and post-processed, resin curing processes have been demonstrated as safe for medical applications, depending on the particular combination of chemical components [25]. These considerations for linking the chemical structure of a polymer to its functioning and printing are essential in pairing printing processes with materials to achieve a desired set of properties for a specified application.

2.2. Material Properties

There are diverse material properties necessitated by medical applications that are achievable through 3D printing. Often, medical applications drive the need for specific material capabilities, such as the need for energy absorbing materials in impact resistance, multicolored parts with suitable textures for modeling surgical anatomies, or specified material properties to mimic biological tissues. [Figure 2](#) highlights recent research in medical polymer materials with a focus on mechanical capabilities for toughness [26][27] and flexibility [28][29], biological capabilities for biocompatibility [24][30], and further capabilities such as electrical conductivity [31][32].

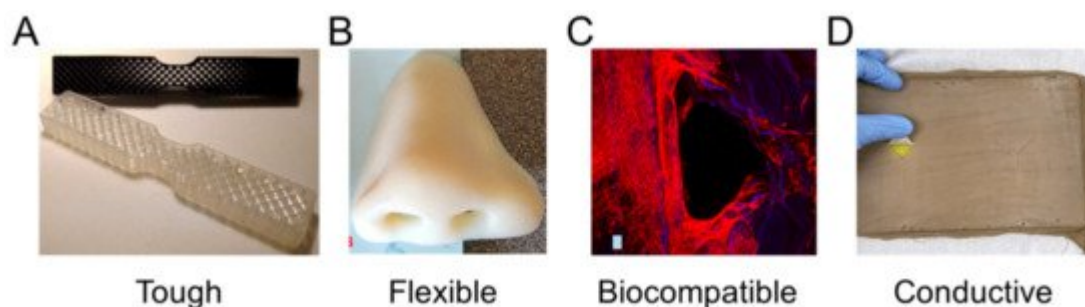


Figure 2. Materials with highlighted properties for (A) toughness [26], (B) flexibility [28], (C) biocompatibility [30], and (D) conductivity [31]. Images adapted with permission.

Toughness in a material refers to its capability to absorb energy and plastically deform without fracturing, which is calculated from a combination of the material's strength and ductility. Recently, a 3D-printed tensile bar with crosshatch structures was printed from a tough polyurethane material with comparisons including physically cross-linked Carbothane AC-4095A in pellet form and chemically cross-linked polyurethane with 68A hardness in liquid resin form ([Figure 2A](#)) [26]. Results demonstrated elastomeric polyurethanes are relatively tolerant of architectures and notches, which also promotes their use in a variety of design strategies. A further example of toughness for biomedical materials was demonstrated with a methacrylic polymer printed using the resin curing process with a tensile strength of 41 MPa and a general elongation up to 50% before breaking [27]. The material was used for printing a shaft coupling for an assembly without any post-treatment necessary due to the high accuracy of the printing process.

Flexible materials have been constructed recently that are useful as prosthetics, and enable the optimization of a specified form for a person's unique physiology through scanning and fitting technologies ([Figure 2B](#)) ^[28]. The patient of interest for the study was 27 years old and had a topographic scan of their face that used 3D mapping software to print the nose shape using a Stratasys polyjet printer with TangoPlus flexible material. The TangoPlus material had a 26 to 28 Shore A Hardness, 0.8 to 1.5 MPa tensile strength, and 2 to 4 kg/cm tear resistance, while having a feel similar to rubber. Recoloring was necessary to match the patient's skin tone. Flexible materials have also been used to print complex structures, such as an Eiffel tower model printed with temperature-stimulated flexible polymer printed using stereolithography ^[29]. The model distorts at lower temperature and as the temperature increases to 70 °C, the print regains its original form. This temperature-dependent functionality provides possibilities for medical applications with heat-initiated actuation, which could be initiated by body heat or devices.

Biocompatibility is a necessary material property for printed devices that interact with the body, such as hearing aids and retainers, or are implanted in vivo, such as artificial joints or tissue scaffolds. Depending on the application, biocompatibility can have differing criteria, but generally refers to the need for the material to do no harm to the body while facilitating its intended function. For tissue scaffolds, biocompatibility typically refers to a need for non-cytotoxicity, biodegradability, and promotion of tissue growth. Polyjet printing uses Stratasys MED610 material, which is an acrylic-based polymer that has recently had success for printing tissue scaffolds of complex topologies ([Figure 2C](#)) ^[30]. Biological testing was conducted by measuring cell viability using Saos-2 cells that survived, with no difference between the 3D-printed materials and controls after 48 h. Further testing demonstrated growth on tissue scaffold surfaces; however, the growth was limited compared to other tissue engineering materials. An alternative approach is the use of stereolithography for 3D-printed lattices using polylactic acid that can reliably form lattice structures with microscale features ^[24]. Further testing is required to determine the benefits of 3D-printed polymers to conventional tissue engineering approaches; however, polymers provide immediate advantages over metals due to their ability to degrade safely in vivo.

Electrical conductance is another material property that is useful for medical applications and has been used for fabricated, sensorized tissue analogues through the 3D printing of an organogel. The technology was used to create a suture training pad fabricated with embedded piezoresistive strain sensors and conductive threads as electrodes to quantify the performance of the trainee ([Figure 2D](#)) ^[31]. Fabrication steps included fixing nylon fabric to the bottom of a PLA mold, then pouring and curing skin-colored liquid PDMS, inserting conductive threads into the 3D-printed organogel, encapsulating sensors, adding a fat layer, and cutting the sample to form a suture pad. Further polymer electrical conductivity has been demonstrated with thermoplastics mixed with conductive carbon black fillers for 3D printing a chess rook that enables turning on an LED light ^[32]. These printing capabilities enable new types of design applications that could provide feedback in different medical scenarios through embedding sensors in fabricated designs, possibly activating when certain mechanical triggers are reached.

2.3. Material Capabilities

Properties of 3D-printed parts are dependent on both their material structure and printing process, and therefore require extensive testing of combinations of materials/process parameters to determine material capabilities for a given application [33]. For instance, a part's mechanical response when fabricated with fused deposition modeling is alterable based on the printed layer thickness, processing temperature, and orientation [34][35]. In [Table 1](#) a summary is provided that highlights the measured mechanical properties of some common polymer 3D-printed materials tested as solid samples; additional notes in the table provide context for how testing was carried out to provide ranges of process-dependent properties. Material properties include strength- and stiffness-related metrics that are key properties for selecting suitable materials in mechanical applications.

Table 1. Measured 3D-printed part properties organized by material and printing process. Further details included to provide relevant context.

Material	Printing Process	Measured Properties	References
Acrylonitrile butadiene styrene (ABS)	Fused deposition modeling	Tensile Strength: 35 MPa; Elastic Modulus: 1300 MPa.	[36]
Acrylonitrile butadiene styrene (ABS)	Fused deposition modeling	Tensile Strength: 27–31 MPa; Layer height: 0.05–0.14 mm; Processed at 210–240 °C.	[34]
Acrylonitrile butadiene styrene (ABS)	Fused deposition modeling	Tensile Strength: 15–38 MPa; Elastic Modulus: 1220–1430 MPa; Orientations of 0° to 90°.	[35]
Polycarbonate (PC)	Fused deposition modeling	Tensile Strength: 37 MPa; Elastic Modulus: 1000 MPa.	[36]
Polycarbonate (PC); Biomaterial blend	Fused deposition modeling	Tensile Strength: 35–65 MPa; Elastic Modulus: 2100 MPa; Nozzle Temperature: 240–270 °C; Orientations of 0° to 90°.	[35]
Polycarbonate (PC); Fossil-fuel blend	Fused deposition modeling	Tensile Strength: 28–62 MPa; Elastic Modulus: 1300–1500 MPa; Orientations of 0° to 90°.	[35]
Polyether ether ketone (PEEK)	Fused deposition modeling	Tensile Strength: 58–85 MPa Elastic Modulus: 3000–4100 MPa; Temperature dependent.	[37]

and face with a surface of ultra-fine texture [9][17]. Polymer 3D printing studies concluded that a decrease in pore diameter and increase in pore size led to a decrease in porosity [44][45] (Figure 3D). The strength of 65 MPa is significantly higher than the elastic modulus of 2100 MPa than a solidified material. The tensile strength of the printed part is 62 MPa and 1500 MPa elastic modulus [35]. Polyether ether ketone (PEEK) and polylactic acid (PLA) are commonly used biocompatible

3.1. Extrusion

Materials with relatively high mechanical strength and stiffness among polymers, and are also manufacturable with fused deposition modeling [37][38]. PEEK is generally the more expensive of the two materials with an elastic modulus up to 4100 MPa, while PLA has an elastic modulus of 4400 MPa; both are the highest values among the In fused deposition modeling material is fed into the printer as a continuous filament. The extruder body is heated surveyed Table 1 materials.

to melt the filament that is extruded by the pressure generated by the filament feed. After filament extrusion, the filament cools down and solidifies to form a solid geometry. Some of the most common printing materials for fused deposition modeling are polylactic acid (PLA), acrylonitrile butadiene styrene (ABS), polyethylene terephthalate with several methacrylic/acrylic-based materials included as examples in Table 1 [9][16][17]. These materials were (PET), and thermoplastic polyurethane (TPU). Support materials are also available that are removed during post-processed with varied resin curing processes and all demonstrated similar elastic moduli around 1500 MPa to 2000 MPa, with some dependency on build orientation. In comparison to the fused deposition modeling parts, these wax. The performance of the printed parts depends on material selection and process parameters such as layer thickness, build orientation, raster angle, infill density, nozzle temperature, and printing speed [46]. In fused deposition modeling, the nozzle temperature is generally maintained at a few degrees higher than the melting point of the polymer, since further increasing the nozzle temperatures may affect the performance for materials like processes enable material selection with similar property ranges. Further considerations for selecting a PEEK and polyetherimide (PEI). It has been reported that the elongation percentage before failure, and impact strength of a PEI part starts reducing when the temperature increases beyond an optimal nozzle temperature [47]. decisions when selecting a 3D printing approach for a given application.

On the other hand, lower temperatures may result in extrusion difficulty and poor print quality due to the formation of porous volumes between the layers [47]. Additionally, layer size presents trade-offs in print resolution, part performance, and printing speed while resulting in variable amounts of anisotropy in final part properties introduced by patterning of layers in specified directions.

Direct ink writing, also known as robocasting, is another extrusion 3D printing process that avoids the heating requirements of fused deposition modeling, and rather deposits a shear, thinning viscoelastic material via a nozzle by applying external shear stress [48][49][50]. Since the process enables printing in ambient conditions, it is ideal for printing soft materials. As the shear stress increases, the viscosity of the ink reduces and enables extrusion through the nozzle. As the ink is extruded, it regains its viscosity to form a 3D structure. The filaments are stacked to additively form the final part. The printed part is cured in a different environment as per the material requirement. Direct ink writing is used to print different materials including bio-inks [41], fiber-suspended inks [48][51], electro/magnetic inks [52], and multi-material inks [53]. The capability of printing different materials in direct ink writing has made it possible to produce designs for diverse applications [48][50]. Some of the most widely used polymers for direct ink writing are polydimethylsiloxane (PDMS), thermoplastics, and epoxy. The major factors in determining the printability are the viscosity and shear thinning property of the material.

3.2. Resin Curing

Resin 3D printing processes expose photosensitive monomers to controlled ultraviolet light or other high energy light sources [54]. Resin curing processes typically benefit from high resolutions and quality part finishing in comparison to other printing methods in comparable price ranges. Ultraviolet curing strategies include

stereolithography with direct laser writing (SLA; [Figure 3B](#)), digital light processing (DLP) [\[55\]\[56\]](#), continuous liquid interface production (CLIP) [\[56\]](#), and continuous digital light manufacturing (CDLM) [\[57\]](#), which all have varied strategies of exposing a vat of resin to light to form a part. Stereolithography printing with direct laser writing includes a resin tank, a high energy light source, and a reflecting mirror to control the resin exposure to a laser. The resin in the tank is exposed to a computer-controlled laser that solidifies the resin to form a solid layer. After exposure to one layer, the printing platform moves vertically for printing the next layer [\[54\]](#). After all the layers are printed, the part is washed and cured under ultraviolet light to strengthen the structure, which provides fine tuning for specific applications [\[58\]](#). The duration of curing alters the printed part mechanics, for instance, when comparing parts that were post-cured for 30 h to those that had no post-curing, the post-curing with ultraviolet light was more time-efficient and improved mechanical properties, such as elastic modulus, and promoted material homogeneity through higher crosslinking [\[59\]](#). Though stereolithography printing has a high resolution and printing speed, in general, it lacks multi-material printability.

Polyjet (also known as inkjet) printing is an alternate resin curing process that uses a nozzle to deposit droplets of material that are immediately cured by an ultraviolet beam upon deposition to form a layer [\[60\]](#). Polyjet printing is advantageous for printing multimaterial models rapidly with multi-nozzle jetting, which also enables printing with support materials [\[61\]\[62\]](#). However, materials should generally still have shear thinning properties, which limits availability [\[56\]](#). Inkjet printing has applications in fields ranging from prototyping to electronics to bio-printing [\[60\]\[62\]](#), and has been demonstrated recently for use in biomedical devices using mechanically efficient lattice structures [\[9\]](#). Lattices were printed using a network of beams with diameters of approximately 400 μm , with fabrication defects depending on topology design and build direction. Further studies are required to determine whether polyjet printing is suitable for tissue engineering applications, with a need to further demonstrate its capabilities by producing structures with cell seeding and proliferation capabilities [\[30\]](#). However, the technology provides a potential for the rapid fabrication of large sets of structures that are customizable for specific patients in applications such as safety equipment.

3.3. Powder Fusion

Powder fusion processes rely on depositing powder layers that are either melted or bonded to additively fabricate parts. Two common powder fusion techniques for polymer printing are selective laser sintering and binder jetting [\[63\]](#). [Figure 3C](#) demonstrates the working principles of selective laser sintering, which relies on a powder stock leveled to enable fusion of one layer through exposure to a laser that follows a specified path. Once a layer is printed, the platform is lowered, and the process is repeated. One of the major advantages of selective laser sintering is the leftover powder in the platform acts as a support during part construction. Therefore the process does not require printing a separate support material and enables complex part and assembly fabrication [\[45\]](#).

In binder jetting printing, a jetted material binds powder as an alternative to laser melting [\[63\]](#). The powder is spread on the printing platform within a predetermined thickness and then the binding material is injected to form a bonded layer. The binder jetting technique uses multiple nozzles to inject the binding material, which is potentially faster than laser melting. Binder jetting is generally an efficient process capable of printing multicolor, multi-material, and

functionally graded materials [64]. Since the binding material acts as an adhesive to hold the powder together and form a printed geometry, the achieved properties of the printed parts depend on the binding material in addition to the shape and size of the powder [65][66].

4. Design Considerations

Based on the material and process capabilities of polymer 3D printing, it is possible to use computer aided softwares to design complex geometries that have specified properties based on process and material selection. Computational algorithms are often used to automate the design of 3D printed parts, such that every print can be a unique and optimized structure that is suitable particularly for wide-ranging applications in customized medical designs for patients.

References

1. Egan, P.F. Integrated Design Approaches for 3D Printed Tissue Scaffolds: Review and Outlook. *Materials* 2019, 12, 2355.
2. Ngo, T.D.; Kashani, A.; Imbalzano, G.; Nguyen, K.T.; Hui, D. Additive manufacturing (3D printing): A review of materials, methods, applications and challenges. *Compos. Part B Eng.* 2018, 143, 172–196.
3. Ventola, C.L. Medical applications for 3D printing: Current and projected uses. *Pharm. Ther.* 2014, 39, 704.
4. Ligon, S.C.; Liska, R.; Stampfl, J.; Gurr, M.; Mülhaupt, R. Polymers for 3D printing and customized additive manufacturing. *Chem. Rev.* 2017, 117, 10212–10290.
5. Egan, P.F.; Shea, K.A.; Ferguson, S.J. Simulated tissue growth for 3D printed scaffolds. *Biomech. Model. Mechanobiol.* 2018, 17, 1481–1495.
6. Liaw, C.-Y.; Guvendiren, M. Current and emerging applications of 3D printing in medicine. *Biofabrication* 2017, 9, 024102.
7. Jonathan, G.; Karim, A. 3D printing in pharmaceuticals: A new tool for designing customized drug delivery systems. *Int. J. Pharm.* 2016, 499, 376–394.
8. Rubio-Perez, I.; Diaz Lantada, A. Surgical Planning of Sacral Nerve Stimulation Procedure in Presence of Sacral Anomalies by Using Personalized Polymeric Prototypes Obtained with Additive Manufacturing Techniques. *Polymers* 2020, 12, 581.
9. Egan, P.F.; Bauer, I.; Shea, K.; Ferguson, S.J. Mechanics of Three-Dimensional Printed Lattices for Biomedical Devices. *J. Mech. Des.* 2019, 141, 031703.

10. Kang, H.; Hollister, S.J.; La Marca, F.; Park, P.; Lin, C.-Y. Porous biodegradable lumbar interbody fusion cage design and fabrication using integrated global-local topology optimization with laser sintering. *J. Biomech. Eng.* 2013, 135, 101013.
11. Seaman, S.; Kerezoudis, P.; Bydon, M.; Torner, J.C.; Hitchon, P.W. Titanium vs. polyetheretherketone (PEEK) interbody fusion: Meta-analysis and review of the literature. *J. Clin. Neurosci.* 2017, 44, 23–29.
12. Erickson, M.M.; Richardson, E.S.; Hernandez, N.M.; Bobbert, D.W., II; Gall, K.; Fearis, P. Helmet Modification to PPE With 3D Printing During the COVID-19 Pandemic at Duke University Medical Center: A Novel Technique. *J. Arthroplast.* 2020, 35, S23–S27.
13. Provenzano, D.; Rao, Y.J.; Mitic, K.; Obaid, S.N.; Pierce, D.; Huckenpahler, J.; Berger, J.; Goyal, S.; Loew, M.H. Rapid Prototyping of Reusable 3D-Printed N95 Equivalent Respirators at the George Washington University. *Preprints 2020*, 2020030444.
14. Egan, P.F.; Ferguson, S.J.; Shea, K. Design of hierarchical three-dimensional printed scaffolds considering mechanical and biological factors for bone tissue engineering. *J. Mech. Des.* 2017, 139, 061401.
15. Mao, Y.; Yu, K.; Isakov, M.S.; Wu, J.; Dunn, M.L.; Qi, H.J. Sequential self-folding structures by 3D printed digital shape memory polymers. *Sci. Rep.* 2015, 5, 1–12.
16. Briguiet, G.; Egan, P.F. Structure, process, and material influences for 3D printed lattices designed with mixed unit cells. In *Proceedings of the ASME 2020 International Design Engineering Technical Conferences and Computers and Information in Engineering*, 17–19 August 2020; Available online: (accessed on 3 November 2020).
17. Moniruzzaman, M.; O’Neal, C.; Bhuiyan, A.; Egan, P.F. Design and Mechanical Testing of 3D Printed Hierarchical Lattices Using Biocompatible Stereolithography. *Designs* 2020, 4, 22.
18. Singh, S.; Singh, M.; Prakash, C.; Gupta, M.K.; Mia, M.; Singh, R. Optimization and reliability analysis to improve surface quality and mechanical characteristics of heat-treated fused filament fabricated parts. *Int. J. Adv. Manuf. Technol.* 2019, 102, 1521–1536.
19. Yao, Q.; Wei, B.; Guo, Y.; Jin, C.; Du, X.; Yan, C.; Yan, J.; Hu, W.; Xu, Y.; Zhou, Z. Design, construction and mechanical testing of digital 3D anatomical data-based PCL–HA bone tissue engineering scaffold. *J. Mater. Sci. Mater. Med.* 2015, 26, 51.
20. Arabnejad, S.; Johnston, R.B.; Pura, J.A.; Singh, B.; Tanzer, M.; Pasini, D. High-strength porous biomaterials for bone replacement: A strategy to assess the interplay between cell morphology, mechanical properties, bone ingrowth and manufacturing constraints. *Acta Biomater.* 2016, 30, 345–356.
21. Dizon, J.R.C.; Espera, A.H., Jr.; Chen, Q.; Advincula, R.C. Mechanical characterization of 3D-printed polymers. *Addit. Manuf.* 2018, 20, 44–67.

22. Peters, E.N. *Plastics: Thermoplastics, Thermosets, and Elastomers*; Wiley-Interscience: New York, NY, USA, 2002.
23. Butt, J.; Bhaskar, R. Investigating the Effects of Annealing on the Mechanical Properties of FFF-Printed Thermoplastics. *J. Manuf. Mater. Process.* 2020, 4, 38.
24. Melchels, F.P.; Bertoldi, K.; Gabbriellini, R.; Velders, A.H.; Feijen, J.; Grijpma, D.W. Mathematically defined tissue engineering scaffold architectures prepared by stereolithography. *Biomaterials* 2010, 31, 6909–6916.
25. Alifui-Segbaya, F.; Varma, S.; Lieschke, G.J.; George, R. Biocompatibility of Photopolymers in 3D Printing. *3d Print. Addit. Manuf.* 2017, 4, 185–191.
26. Miller, A.T.; Safranski, D.L.; Wood, C.; Guldborg, R.E.; Gall, K. Deformation and fatigue of tough 3D printed elastomer scaffolds processed by fused deposition modeling and continuous liquid interface production. *J. Mech. Behav. Biomed. Mater.* 2017, 75, 1–13.
27. Steyrer, B.; Neubauer, P.; Liska, R.; Stampfl, J. Visible light photoinitiator for 3D-printing of tough methacrylate resins. *Materials* 2017, 10, 1445.
28. Nuseir, A.; Hatamleh, M.M.d.; Alnazzawi, A.; Al-Rabab'ah, M.; Kamel, B.; Jaradat, E. Direct 3D printing of flexible nasal prosthesis: Optimized digital workflow from scan to fit. *J. Prosthodont.* 2019, 28, 10–14.
29. Zarek, M.; Layani, M.; Cooperstein, I.; Sachyani, E.; Cohn, D.; Magdassi, S. 3D printing of shape memory polymers for flexible electronic devices. *Adv. Mater.* 2016, 28, 4449–4454.
30. Egan, P.; Wang, X.; Greutert, H.; Shea, K.; Wuertz-Kozak, K.; Ferguson, S. Mechanical and biological characterization of 3D printed lattices. *3d Print. Addit. Manuf.* 2019, 6, 73–81.
31. Crump, M.R.; Bidinger, S.L.; Pavinatto, F.J.; Gong, A.T.; Sweet, R.M.; MacKenzie, J.D. Sensorized tissue analogues enabled by a 3D-printed conductive organogel. *Npj Flex. Electron.* 2021, 5, 1–8.
32. Leigh, S.J.; Bradley, R.J.; Purssell, C.P.; Billson, D.R.; Hutchins, D.A. A simple, low-cost conductive composite material for 3D printing of electronic sensors. *PLoS ONE* 2012, 7, e49365.
33. Dong, G.; Tang, Y.; Zhao, Y.F. A Survey of Modeling of Lattice Structures Fabricated by Additive Manufacturing. *J. Mech. Des.* 2017, 139, 100906.
34. Yadav, D.; Chhabra, D.; Gupta, R.K.; Phogat, A.; Ahlawat, A. Modeling and analysis of significant process parameters of FDM 3D printer using ANFIS. *Mater. Today Proc.* 2020, 21, 1592–1604.
35. Park, S.J.; Lee, J.E.; Lee, H.B.; Park, J.; Lee, N.-K.; Son, Y.; Park, S.-H. 3D printing of bio-based polycarbonate and its potential applications in ecofriendly indoor manufacturing. *Addit. Manuf.* 2020, 31, 100974.

36. Kannan, S.; Ramamoorthy, M. Mechanical characterization and experimental modal analysis of 3D Printed ABS, PC and PC-ABS materials. *Mater. Res. Express* 2020, 7, 015341.
37. Yang, C.; Tian, X.; Li, D.; Cao, Y.; Zhao, F.; Shi, C. Influence of thermal processing conditions in 3D printing on the crystallinity and mechanical properties of PEEK material. *J. Mater. Process. Technol.* 2017, 248, 1–7.
38. Song, X.; He, W.; Qin, H.; Yang, S.; Wen, S. Fused Deposition Modeling of Poly (lactic acid)/Macadamia Composites—Thermal, Mechanical Properties and Scaffolds. *Materials* 2020, 13, 258.
39. Dong, G.; Wijaya, G.; Tang, Y.; Zhao, Y.F. Optimizing process parameters of fused deposition modeling by Taguchi method for the fabrication of lattice structures. *Addit. Manuf.* 2018, 19, 62–72.
40. Carneiro, O.S.; Silva, A.; Gomes, R. Fused deposition modeling with polypropylene. *Mater. Des.* 2015, 83, 768–776.
41. Skylar-Scott, M.A.; Uzel, S.G.; Nam, L.L.; Ahrens, J.H.; Truby, R.L.; Damaraju, S.; Lewis, J.A. Biomanufacturing of organ-specific tissues with high cellular density and embedded vascular channels. *Sci. Adv.* 2019, 5, eaaw2459.
42. Melchels, F.P.; Feijen, J.; Grijpma, D.W. A review on stereolithography and its applications in biomedical engineering. *Biomaterials* 2010, 31, 6121–6130.
43. Pham, D.T.; Gault, R.S. A comparison of rapid prototyping technologies. *Int. J. Mach. Tools Manuf.* 1998, 38, 1257–1287.
44. Brighenti, R.; Cosma, M.P.; Marsavina, L.; Spagnoli, A.; Terzano, M. Laser-based additively manufactured polymers: A review on processes and mechanical models. *J. Mater. Sci.* 2020, 56, 961–998.
45. Goodridge, R.D.; Tuck, C.J.; Hague, R.J.M. Laser sintering of polyamides and other polymers. *Prog. Mater. Sci.* 2012, 57, 229–267.
46. Mohamed, O.A.; Masood, S.H.; Bhowmik, J.L. Optimization of fused deposition modeling process parameters: A review of current research and future prospects. *Adv. Manuf.* 2015, 3, 42–53.
47. Ding, S.; Zou, B.; Wang, P.; Ding, H. Effects of nozzle temperature and building orientation on mechanical properties and microstructure of PEEK and PEI printed by 3D-FDM. *Polym. Test.* 2019, 78.
48. Compton, B.G.; Lewis, J.A. 3D-printing of lightweight cellular composites. *Adv Mater* 2014, 26, 5930–5935.
49. Cesarano, J. A Review of Robocasting Technology. *MRS Proc.* 2011, 542.

50. Lewis, J.A.; Gratson, G.M. Direct writing in three dimensions. *Mater. Today* 2004, 7, 32–39.
51. Raney, J.R.; Compton, B.G.; Mueller, J.; Ober, T.J.; Shea, K.; Lewis, J.A. Rotational 3D printing of damage-tolerant composites with programmable mechanics. *Proc. Natl. Acad. Sci. USA* 2018, 115, 1198–1203.
52. Kokkinis, D.; Schaffner, M.; Studart, A.R. Multimaterial magnetically assisted 3D printing of composite materials. *Nat Commun.* 2015, 6, 8643.
53. Ober, T.J.; Foresti, D.; Lewis, J.A. Active mixing of complex fluids at the microscale. *Proc. Natl. Acad. Sci. USA* 2015, 112, 12293–12298.
54. Wendel, B.; Rietzel, D.; Kühnlein, F.; Feulner, R.; Hülder, G.; Schmachtenberg, E. Additive Processing of Polymers. *Macromol. Mater. Eng.* 2008, 293, 799–809.
55. Sodupe-Ortega, E.; Sanz-Garcia, A.; Pernia-Espinoza, A.; Escobedo-Lucea, C. Accurate Calibration in Multi-Material 3D Bioprinting for Tissue Engineering. *Materials* 2018, 11, 1402.
56. Stansbury, J.W.; Idacavage, M.J. 3D printing with polymers: Challenges among expanding options and opportunities. *Dent. Mater.* 2016, 32, 54–64.
57. Wallace, J.; Wang, M.O.; Thompson, P.; Busso, M.; Belle, V.; Mammoser, N.; Kim, K.; Fisher, J.P.; Siblani, A.; Xu, Y.; et al. Validating continuous digital light processing (cDLP) additive manufacturing accuracy and tissue engineering utility of a dye-initiator package. *Biofabrication* 2014, 6, 015003.
58. Cooke, M.N.; Fisher, J.P.; Dean, D.; Rimnac, C.; Mikos, A.G. Use of stereolithography to manufacture critical-sized 3D biodegradable scaffolds for bone ingrowth. *J. Biomed. Mater. Res. B Appl. Biomater.* 2003, 64, 65–69.
59. Mendes-Felipe, C.; Patrocinio, D.; Laza, J.M.; Ruiz-Rubio, L.; Vilas-Vilela, J.L. Evaluation of postcuring process on the thermal and mechanical properties of the Clear02™ resin used in stereolithography. *Polym. Test.* 2018, 72, 115–121.
60. Cummins, G.; Desmulliez, M.P.Y. Inkjet printing of conductive materials: A review. *Circuit World* 2012, 38, 193–213.
61. Taylor, A.P.; Velasquez-Garcia, L.F. Miniaturized Diaphragm Vacuum Pump by Multi-Material Additive Manufacturing. *J. Microelectromech. Syst.* 2017, 26, 1316–1326.
62. Li, F.; Macdonald, N.P.; Guijt, R.M.; Breadmore, M.C. Increasing the functionalities of 3D printed microchemical devices by single material, multimaterial, and print-pause-print 3D printing. *Lab. Chip.* 2018, 19, 35–49.
63. Wang, Y.; Xu, Z.; Wu, D.; Bai, J. Current Status and Prospects of Polymer Powder 3D Printing Technologies. *Materials* 2020, 13, 2406.

64. Ziaee, M.; Crane, N.B. Binder jetting: A review of process, materials, and methods. *Addit. Manuf.* 2019, 28, 781–801.
65. Utela, B.; Storti, D.; Anderson, R.; Ganter, M. A review of process development steps for new material systems in three dimensional printing (3DP). *J. Manuf. Process.* 2008, 10, 96–104.
66. Parab, N.D.; Barnes, J.E.; Zhao, C.; Cunningham, R.W.; Fezzaa, K.; Rollett, A.D.; Sun, T. Real time observation of binder jetting printing process using high-speed X-ray imaging. *Sci. Rep.* 2019, 9, 2499.

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