


Delamination-and Electromigration-Related Failures

Subjects: Energy & Fuels

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Definition

The reliability of photovoltaic (PV) modules operating under various weather conditions attracts the manufacturer's concern since several studies reveal a degradation rate higher than 0.8% per year for the silicon-based technology and reached up to 2.76% per year in a harsh climate. The lifetime of the PV modules is decreased because of numerous degradation modes. Electromigration and delamination are two failure modes that play a significant role in PV modules' output power losses. The correlations of these two phenomena are not sufficiently explained and understood like other failures such as corrosion and potential-induced degradation.

1. Introduction

The energy transformation from fossil fuels to zero-carbon energy is just around the corner as the solar energy sector expands rapidly across the globe. By 2050, the World Energy Council aims to shift from fossil fuel to solar energy as an alternative energy source ^[1]. However, the efficiency, reliability, and performance of photovoltaic modules become more crucial, although the average lifetime of the photovoltaic (PV) modules is about 25 years. The performance of PV modules depends not only on their features but also on other conditions, including climate and installation configurations ^{[2][3]}. There are several reports in the literature regarding the severe environmental conditions that can severely affect the PV modules' performance. Among all the environmental conditions, humidity, heat, extreme weather, dust, and cloud shading affect the PV modules' performance drastically and may degrade their lifetime ^{[4][5][6][7]}. It is also reported that snail trails due to water vapor ^[5] can be the cause of discolorations on solar cells and indicators of cell cracks. However, more research and investigation are still needed to confirm the major effects of snail trails on PV modules; however, today, it is assumed that the snail trails can significantly reduce the output power of the PV modules and thus reduce their lifetime ^{[5][6][7][8][9]}. Robust, reliable, and best-performing PV modules are now the foremost apprehension of commercial solar cell manufacturers to keep the PV modules working with the best output efficiency throughout their life span. Hence, the mechanisms related to the failure of PV modules must be understood. In the early stage of PV solar cell development, identifying the failure mechanisms was difficult. However, technological advancement has boosted up the development of highly efficient solar cells recently. Several failure mechanisms, such as cell crack, delamination, discoloration, and potential-induced degradation (PID), have been reported in the literature.

Indeed, understanding the most significant long-term degradation mechanisms has contributed to measure the long-term performance and lifetime of PV modules, which makes today's qualification tests of PV modules more valuable ^{[10][11]}. Thus, the most popular certification check used currently is based on the International Electrotechnical Commission (IEC) Certification (i.e., IEC 61215 standard for crystalline silicon (c-Si) modules and IEC 61646 for thin-film modules (TF)) ^[12]. These standards indicate early product life failures of the PV module because of poor design, assembly, or materials choice ^[10]. Based on a pass or fail criteria, a set of experiments, such as damp heat (DH), thermal cycling, ultraviolet (UV) light, and other tests, were conducted to estimate the infant failures that affected long-term performance ^[13]. Moreover, the defined percentage of power loss to pass the qualification standards should not exceed more than 5% for c-Si modules and 10% for TF modules, whereas more than 5% in power loss is considered to fail ^[14]. Conversely, accelerated lifetime tests (ALTs) are vital tools for the industry of PV modules and researchers. ALTs encourage the manufacturers to test the modules' real lifetime behavior using different structures or submaterials. For every new unit they make, they ensure to develop more

robust, reliable, and high-efficiency PV modules. For example, according to the IEC 61215, the back sheet and the encapsulation of a PV module were investigated via a damp heat test with 85% RH, 85 °C, and 1000 h [15].

Packaging material degradation such as glass breakage, cell cracking, and back-sheet cracking could occur during shipment or deployment that are the first important phases in a PV panel's lifetime. Although these failures do not affect the PV module's efficiency at the beginning of field operation, they can induce and trigger other environment-related failures such as failed electrical insulation, delamination, discoloration, corrosion, and PID [11][16][17]. Conversely, electromigration (EM) has a tremendous impact on the photovoltaic modules' metallization and interconnections [18]. A high flow of current through the PV module can cause voltage stress and potentially lead to the cause of EM. The failures due to this phenomenon, which influence the growth of etch pits at the metal/semiconductor interface, can vary, and the formation of hillocks and protuberances that cause shorts (shunts) and the formation of voids in the conductor eventually result in an open circuit [19]. Both the front and back junctions intersect the cell wall within the small shunt defect area, diminishing the solar cell's quality. Silver and its past components were identified on ethylene-vinyl acetate (EVA) sample taken (over the finger area) from a 20-year-old outdoor exposure c-Si PV module [18]. The author stated that the transfer of Ag was because of the adhesion loss at the Ag-Si interface. However, this study did not show the root cause of this transport, which we believe has a strong relationship with the EM mechanism. There have been suggestions for further investigations on the material migration of the solar cell's metallization (fingers and busbar) especially for new metallization techniques such as the Ni-Cu plating metallization [20]. Ni-Cu metallization is believed to be an alternative method to the current dominant screen-printed metallization in conventional silicon solar cells [20]. Additionally, since the width of Ag fingers is minimized to approximately 35 μm in 2019 from 100 μm in 2010 [21], these fingers will be more susceptible to EM failure.

Additionally, because of the compromised front junction and the blocking activity of the back contact, the open-circuit voltage (V_{OC}) and fill factor (FF) of the PV modules get affected [22]. The small shunted area causes profound changes in the I-V behavior of the entire cell because of a very permeable diode disorder. Conversely, the formation of the void increases the series resistance and leads to the fall of the FF and the short-circuit current density (J_{SC}) of the solar cells. The systematic approach began in studying EM in the early 1950s while electronic industries are booming; however, interest in studying EM existed already in the 20th century. At the end of the 1960s, the first signs of damages caused by EM in integrated circuits (ICs) were observed on metal film interconnects in chips [23]. The concept of "electron wind" as a flow of charge carriers that mechanically affect the conductor's lattice atoms started to take shape. Some of the research studies use the aluminum ribbon as an interconnection model for the high-efficiency c-Si, but they did not mention the reliability issues such as EM failure [24]. Additionally, EM phenomena have been reported in c-Si solar cells [25][26], rare passivated Si solar cells [27], passivated emitter and rear cells [28], CdTe solar cells [22], and perovskite solar cells [29].

Conversely, the most widely observed deterioration of encapsulants is discoloration and delamination [30]. Delamination occurs because of the loss in the interfacial bonds, resulting in gaps between glass-EVA, EVA-cell, cell-EVA, and EVA-back sheet of a PV module. Additionally, the delamination of the PV module is considered to be one of the major failure modes. According to SolarWorld (a German-based company), delamination failure has been seen in over 90% of the restored modules [31]. However, there is no reason to believe that it is related to the manufacturers. This phenomenon is mostly observed and recorded under extreme weather (very hot and humid) conditions [18][32]. Reduced the module's performance by inducing the moisture ingress, leading to power output degradation, and increased series resistance are the effects of delamination [33]. Delamination has been addressed in various studies. For example, Li et al. [34] investigated two major failures: delamination and corrosion on Si PV modules exposed to high temperatures and humidity. Corrosion and delamination are mainly the results of electrochemical reactions on the metallization of the cell. They are leakage current dependent because of the high potential between the frame and the metallization, which induces a leakage current via an electric field

on the cell's antireflective coating, glass, and encapsulant. Then, the hydrogen gas starts accumulating on the metal surface and induces delamination failure. Additionally, the authors concluded that the hydroxide ions start changing the local environments close to the metallization, causing serious damages to the bonds between the encapsulant and the solar cell. However, they only reported the effects of high temperatures and humidity but did not provide a solution or remedy to avoid these effects.

2. Delamination Failures

2.1. ALTs for Delamination Failures

ALTs are stresses subjected to the PV module until the failure occurs, whereas specific durations of stresses are assigned in qualification certificate testing [35]. Some of the delamination failures can be easily observed on the PV modules operating in the field via visual inspection. Additionally, certain test procedures in the laboratory experience the same failures seen in the field. To improve the reliability of photovoltaic modules, multiple ATLs were developed on the industry side to predict the lifetime of the PV modules. ALTs are also used to mimic delamination failures. For instance, DH, whose parameters are 85 °C, and 85% RH for 1000 h, is required for IEC [36], humidity freeze, and UV exposure. However, some of the PV modules in the field that passed the IEC of DH test show a severe degradation rate [33]. Hence, some of the researchers change these parameters by increasing or decreasing to explore more about the failures. Table 1 is showing different ATLs with different parameters utilized to predict the delamination failure and the characterization tools.

Table 1. Summary of accelerated lifetime tests with different parameters used for delamination failure investigations—see the abbreviation.

Paper Reference	Test Type	PV Technology	Parameters	Affected Region	Failure Result	Diagnostic Tool
[36]	Damp heat	c-Si	Phase 1: 85 °C, 85% RH, 1300 h Phase 2: 85 °C, 85% RH, 1000 h	Delamination and corrosion	I_{SC} reduced by more than 85% from the initial value.	Visual inspection
[37]	Damp heat	c-Si	85 °C, 85% RH, 1000 h	EVA–silver interface (after 300 h only)	More than 90% loss in adhesion energy	Visual inspection
[38]	Damp heat	TF	85 °C, 85% RH, 683 h	Delamination of TCO layer	Efficiency reduced from 14% to 5.3% and increased R_s	Visual inspection
[39]	Damp heat	TF	85 °C, 85% RH, 1000 h	Delamination of AZO layer	NA	Visual inspection
[18]	Damp heat	c-Si	85 °C, 85% RH, 3000 h	Adhesion loss of Si-Ag interface	Decrease in FF by (12–14%) because of migration of tin metal (from the solder joints)	EL image and SEM, EDX image
[34]	Combined stress	c-Si	(85 °C, 85% RH, damp heat 1000 h) (72 °C, 95% RH, bias –1000 V, 292 h)	Front EVA and cell interface delamination	Corrosion of Si and SiO_xN_y	SEM and EDX

Paper Reference	Test Type	PV Technology	Parameters	Affected Region	Failure Result	Diagnostic Tool
[40]	Combined stress	c-Si	85 °C, 85% RH, damp heat 1000 h). Additionally, 72 °C, 95% RH, bias +1000 V dwell time was extended to 3 months	EVA discoloration and enable delamination caused by migration of Ag ions oxide and/or Ag sulfide	30–32% power losses are mainly attributed to I_{sc} loss. I_{sc} (16–25%), FF (<12%), and a slight reduction in V_{oc} (<6%)	X-ray photoelectron spectroscopy (XPS)

Issa Faye et al. [36] investigated the consumer-type of minimodules where they were used in severe climate conditions in Senegal. Two modules were evaluated by the DH test for 1000 and 1300 h, respectively, using 85 °C, and 85% RH. The other two modules (named C and D) were exposed to 55 and 66 cycles of thermal cycle (TC) test using a thermal chamber with diagnostic tools such as infrared (IR) thermal image, I-V curve analysis, and electroluminescence (EL). The visual inspection confirmed that the modules were affected by corrosion, bubbles, and delamination. However, by observing the EL image of the modules C and D that had been through 66 and 55 cycles of TC, respectively, as shown in Figure 1, they summarized their findings:

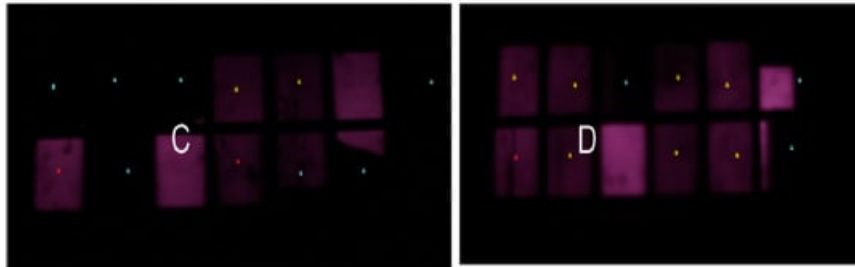


Figure 1. EL image of the C and D minimodules. Adapted with permission from ref. [36]. Copyright 2019, Elsevier.

- Cells with a disrupted finger contact lead to darker areas in the solar cell's active areas.
- Dark spots in the cell region resulted from the solar cell cracks and/or metallization interruption: the 55-cycle minimodule displays five dark areas. The 66-cycle minimodule shows two dark region cells. The dark regions within the active region of a solar cell, as shown in Figure 1, suggest full disconnection, which may be triggered by the front or backside metallization interruptions.
- Cells with discoloration provoked by corrosion undergo a rapid transition from dark to lighter regions.

Their overall result indicated that almost all defects found on the module were due to the impacts of exposure conditions. Consequently, the study's findings suggest that the consumer-type c-Si minimodules may not be suitable for hot and humid African climates [36].

2.2. Encapsulation Delamination

The encapsulant used in Si modules is a polymeric substance, and it functions to grant an adhesion to the solar cell and the glass, the back sheet and solar cell, and any location within the back sheet and the glass. Moreover, it gives mechanical assistance to the module structure and cell configuration while providing enough optical binding, PV cell protection against electrical agents, and other external actions [41]. For approximately three decades, the materials utilized as encapsulants are the EVA copolymers and EVA materials encapsulated nearly 80% of PV modules. However, EVA is the most generally used investor in encapsulated Si-based PV modules [42][43].

Various studies have reported that encapsulant delamination was among the most significant common

field failures for PV modules [44][45]. Figure 2 illustrates the structure of the c-Si PV module. Encapsulant is one of the essential materials of the PV module. Hence, it should be more reliable to optimize the module efficiency.

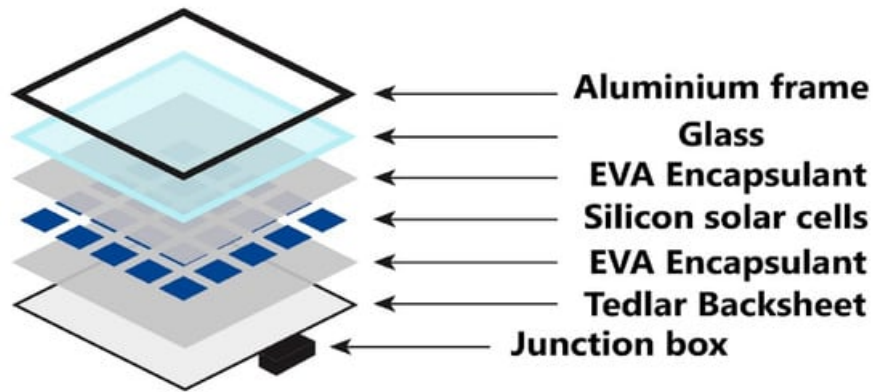



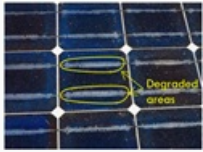
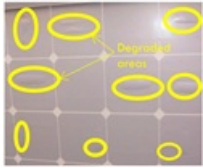
Figure 2. c-Si PV module composition [46].

Meena et al. [47] examined the delaminated and discolored encapsulant degradation of 20-year-old c-Si solar panels. Findings show that the gray delaminated EVA deterioration is associated with the reflection effects at high wavelengths. By contrast, the absorption at low wavelengths is referred to as the brown discolor that appeared on the EVA. Their results indicated that the influence of these effects on panel output was observed as a loss in short-circuit current, with a further power loss due to cell failure. Furthermore, simulation for the degraded region’s effect showed a loss in the solar panel’s output power of more than 40%. All in all, they demonstrated the qualitative impacts of predominant EVA deterioration that are possibly beneficial for developing the EVA design and production for PV modules factories.

In Wohlgemuth et al. [48], during the visit for PV arrays, the National Renewable Energy Laboratory (NREL) community observed any changes in PV modules. Three different observations of delamination have been reported in this paper: encapsulant-glass delamination, encapsulant-cell delamination, and back-sheet delamination [48]. Remarkably, the encapsulant delamination is considered to be one of the main degradations that affect the PV modules’ overall performance. As discussed previously, various forms of encapsulant delamination were identified in the field, including front glass-encapsulant delamination, cells, interconnecting ribbons, and back sheet [49][50]. Conversely, they mostly share some of the effects, causes, and mechanisms, and they differ in impacting PV modules. For instance, the EVA-cell and EVA-glass delaminations are more damaging than the EVA-back-sheet delamination [37][51]. Table 2 illustrates the differences of these three types.

Table 2. Different delamination failures associated with EVA and their main causes and effects.

Type of Encapsulation Degradation	Figure	Causes	Effects
Encapsulant-glass delamination	<p>EVA-glass delamination has a propensity to occur either directly over the junction box or at the corner areas [48]</p> 	<p>UV exposure at higher temperature and humidity Contamination of the glass and EVA materials</p>	<p>Increase the light reflection of the glass Water penetration into the module structure</p>

Type of Encapsulation Degradation	Figure	Causes	Effects
Encapsulant-cell delamination	<p>Mostly, occurring around the interconnect ribbons and metallization [52]</p> 	<p>High current leakage (by enhancing the flow of ions like sodium) Fluxing cycle issues by leaving residues Insufficient EVA flowing under the tabbing ribbon leaves voids below the ribbon where water can intensify at the cool condition and evaporate, creating a bubble in a hot condition</p>	<p>Major transmission loss Major loss in power output of the module greater than EVA glass Enhance the occurring of corrosion due to the condensation of sodium ions</p>
Encapsulant-back sheet delamination	<p>Occur between the encapsulant and the back sheet or between layers of the back sheet itself [49]</p> 	<p>Residual and external stresses, which weaken the adhesion between the encapsulant and the back sheet</p>	<p>In terms of PV performance, back sheets do not play a role as important as EVA-glass and EVA-cell encapsulant</p>

A similar observation has been demonstrated by N. C. Park et al. [51] during the failure analysis of a PV module. They confirmed that delamination happened at the EVA sheet and glass interfaces, following the EVA sheet and solar cell. Moreover, delamination exists at the back sheet, as shown in Figure 3 [51]. The electrical properties of the 25-year-old module located in Yeosu, South Korea, show a decreasing P_{max} by 17.9%, I_{SC} by 17.7%, and V_{OC} by 1.9% from the initial measurement. The leading cause of this reduction was suggested to be the minimizing of transmittance light, which occurred because of the discoloration and delamination that directly affect the I_{SC} .

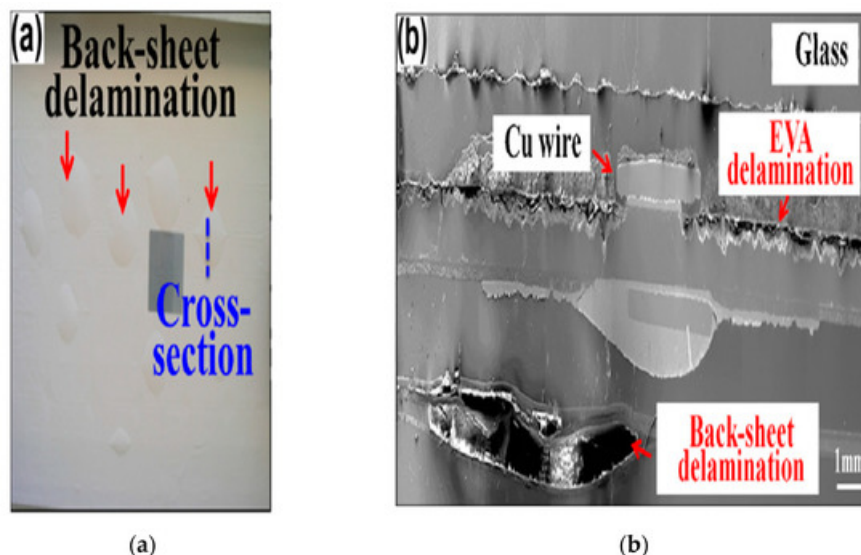


Figure 3. (a) Back-sheet region delamination (red arrows) and (b) cross-sectional picture for PV module, delamination appeared at the interfaces between EVA-glass and EVA-cell. Adapted with permission from ref. [51]. Copyright 2013, Elsevier.

Other mechanisms that help the occurrence of encapsulant delamination are chemical reactions that break the bond interface because of the humidity or material contamination and photothermal reaction that break the bond interface due to UV light and high temperature [35][48]. Lastly, the effects of the mentioned mechanisms could resemble a power drop beyond the warranty limit, promoting corrosion and

moisture ingress to the structure of the PV module.

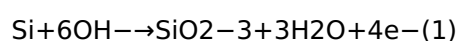
2.3. Delamination Associated with Corrosion

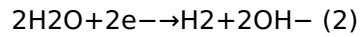
Li et al. [34] claimed that corrosion and delamination are cooperative and encourage mutual development between them. They observed the electrochemical reduction reaction of water with the metallization via dump heat test (1000 h, 85% RH, and 85 °C) followed by the biasing test (–1000 V, 292 h, 95% RH, and 72 °C) for a mini-PV module as shown in Figure 4 [34]. They confirmed that the degree of corrosion depends on the encapsulant resistance against the alkaline solution. It has also been reported that electrochemical reaction mechanisms in the PV modules drive the leakage current that primarily contributes to the occurrence of corrosion and delamination [34][53][54]. In this case, hydroxide ions and hydrogen gas are caused by the electrochemical reduction reactions of an ionic factor of the leakage current subjected to negative biasing. The hydrogen gas acts as a promoting agent for delamination when it accumulates on the metal surface, whereas hydroxide ions are altering the local environment near the metallization. Therefore, the corrosion of Si or SiO₂ materials in solar cells within the alkaline environment destroys the bonds that exist between the encapsulant and the cell's surface.



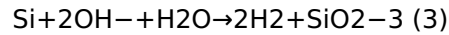
Figure 4. Four cells initially stressed at 85 °C/85% RH, 1000 h for DH test, and then biased at (–1000 V) for 292 (the area covered by the rectangle used for SEM and EDS analyses). Adapted with permission from ref. [34]. Copyright 2018, Elsevier.

Figure 5a illustrates Ag fingers' morphology analyzed using scanning electron microscopy (SEM) and associated energy-dispersive X-ray spectroscopy (EDS) mapping of the element at the selected area in Figure 4. Granular particles, such as Na, O, and Si, were found in the SEM images on the edge of Ag's fingers that were not detected in the unexposed cell. The EDS analysis shows that the materials' composition was 40.9 wt % Si, 44.1-wt % O, and 7.3-wt % Na and indicated that they were Si corrosion products [34]. These materials reacted with the hydroxide ions, leading to silicate creation, as shown in Figure 5b. It should be mentioned that the hydroxide ions are heavily concentrated close to metal fingers and enter through the pinhole in the nitride layer [55][56]. The OH[–] ions, which create an alkaline environment, damages the bonds that exist between the encapsulant and solar cell and lead to the occurrence of delamination [34]. The electrochemical reactions could be written as:





resulting in,



and SiO_2 dissolves by the acid-base reaction

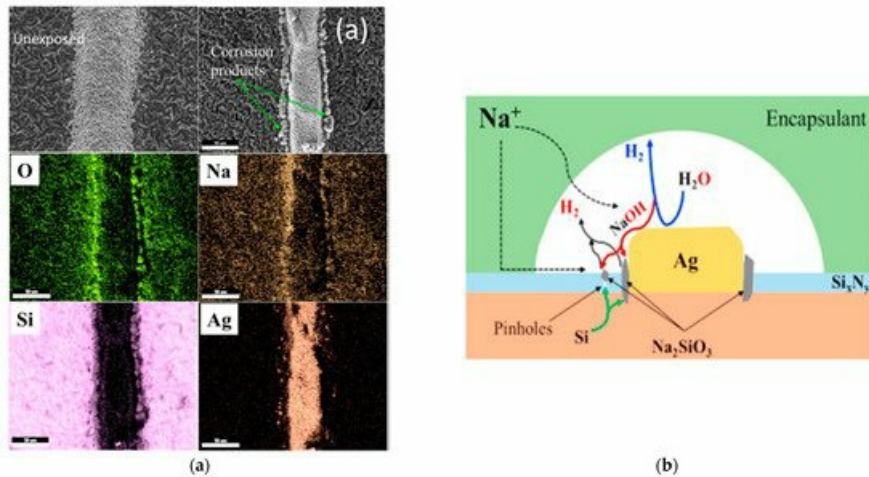
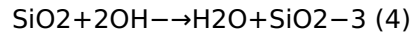


Figure 5. (a) SEM and EDS image of silver fingers at the delamination area; (b) silicon corrosion close to the silver fingers and at defects or pinholes in the SiO_xN_y during the negative biasing test. Adapted with permission from ref. [34]. Copyright 2018, Elsevier.

Asadpour et al. [57] conducted a one-dimensional simulation focusing on the delamination and corrosion of fingers on a c-Si solar cell/module's front side. Since the layer's thickness is only a few millimeters, which is negligible relative to the module area, a reasonable approximation of a three-dimensional structure would be a one-dimensional simulation, as shown in Figure 6. Reportedly, the reduction of Ag finger thickness via corrosion enhances the series resistance of the cell-module and reduces the efficiency [57].

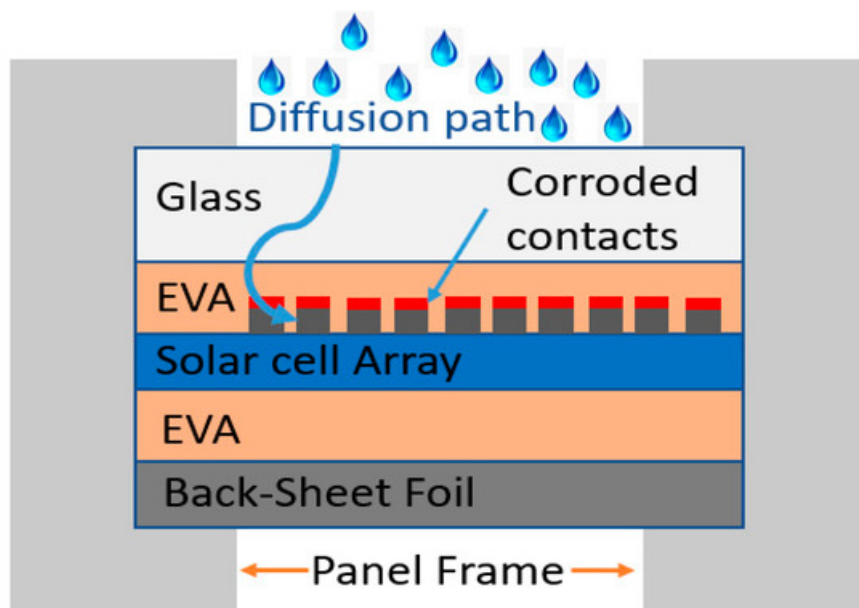


Figure 6. Schematic of moisture diffusion path inside the PV module structure. Adapted and redrawn from ref. [57].

The previous report has also shown that corrosion would not be a concern for Tampa, Florida, with a temperature mean of nearly 23 °C and 79% RH for well-built systems. However, a high percentage of module output deterioration if the environmental condition is 85 °C/85% RH tends to be a severe failure relative to the field conditions. Additionally, delamination often will not be a problem if the only trigger is the moisture penetration from the glass and the encapsulant.

2.4. Delamination Associated with PID

PID has become the subject of recent research [58]. According to the authors of the article, such delamination is accompanying PID, which occurred for different commercial c-Si PV modules that share common construction, particularly at the grid fingers region. Conversely, thin films, such as CdTe and Si photovoltaic modules, are affected by the PID, which occurred because of the delamination around the TCO layer [59]. Delamination is the leading cause of PID in TF Si PV modules [60]. A PV station's output power loss can be up to 30% when severe PID affects it [61]. The PID mode of c-Si PV modules in the field was first introduced in 2010 [62] and especially for P-type PV modules that gained much attention [63]. Through the encapsulation and front glass, PID leads to high paths of leakage between the cells and the ground [64]. Early research investigations suggested that the onset of PID included the combined impacts of EVA encapsulation, soda lime front glass sheets, and the solar cell's antireflective coating, which is a highly traditional mixture of the attributes of commercial PV modules. Exploring PV modules' real world showed that the PID relies more on external parameters such as high voltage, temperature, and humidity [65][66]. Na ions from soda lime glass have been demonstrated to play a significant role in the degradation cycle [67][68].

By contrast, the use of borosilicate glass that consists of alkali metal of high K and low Na could improve the initial PV performance [69]. Additionally, microscopic analyses have shown the existence of sodium precipitates on solar cell surfaces. Observing the effect of PID could be accomplished by focusing on the mobile sodium ions and other metal ions through the microscopic image [70][71] and impedance spectroscopy [72]. However, PID was also confirmed in sodium-free glass specimens and suggested that the PID resulted from some ionic strain movement and is not directly linked to Na migration [64]. Table 3 shows a similar indoor test and field PID associated with the delamination failure of different Si PV modules.

Table 3. Similar indoor test and field PID associated with the delamination failure of different Si PV modules.

Paper Reference	[73]	[60]
Type of solar cell	Multi c-Si	Tandem TF
PVstructure	Glass/EVA/mc-Si cell/EVA/(PVF/PET/PVF back sheet)	Substrate glass (SLG)/ a-Si:H/ μ c-Si:H cell/EVA/(PVF/PET/PVF backsheet)
PID test structure	Aluminum foil used to cover the front glass (72 °C and 95% RH) while applying the system voltage of -1000 V for 292 h	Al plate/conductive rubber sheet/substrate SLG/Tandem TF cell/EVA/back sheet), positive and negative shorted electrodes then -1000 V applied from the grounded aluminum plate to the shorted electrodes (85 °C and relative humidity of <2%)
Electrical result of the PID test	High leakage current and power losses of the sample that are showing delamination failure	I _{sc} and FF decreased by 17% and 22%, respectively, within the first 150 h. Then, this decreased become saturated after the 150 h until 300 h. Unlike V _{OC} and P _{max} , they did not show any saturation for the decreasing until 300 h (38% and 59%), respectively.

Paper Reference	
Remark for PID test	Field and stressed samples exhibit delamination around the bus bars: severe in field one but comparable delamination for both Linear-shape delamination is also observed after over 150 h of the PID test. The starting point of the linear-shape delamination is located at a scribe line or near interconnector ribbons
Location	Florida Japan

For instance, Peter Hacke et al. [73] at the NREL conducted a test on four c-Si PV modules of 250 W. PID-delamination test conducted to the four modules on the basis of the sequence of 85 °C, 85%(RH), 1000 h DH test followed by a PID test of 72 °C, 95% RH, and –1000 V. This study shows that the delamination occurred after 156 h and again after 292 h of the PID test in module #3, at the same time the power loss was observed in the three modules together with the one experienced the delamination. However, module #4 showing neither power drop nor delamination had the lowest characteristic current transfer along the experiment course, whereas module #3 showing delamination had the highest current transfer. They conclude that the factors that lead to delamination are Na accumulation at the cell's surface develop degrading adhesion, DH, and gaseous byproducts electrochemical motivated by the negative voltage supplied to the active cell circuit.

Naumann et al. [74] provided a precise observation of the PID mechanism. Their paper showed sodium's prevalence in decorating preferentially the deep channels correlated with silicon stacking defects that were native to the process of multicrystalline solar cell crystallization [74]. Most of these stacking faults were deep enough to channel carriers directly through the emitter area and bypass the PN junction. The mechanistic reason for the reversible shunt resistance shift is the out diffusion of sodium from the stacking faults under the inverse bias process, as shown in Figure 7. The Na ion migrates via the glass, and EVA encapsulants accumulate on the cell surface and decorate Si bulk stacking faults [75].

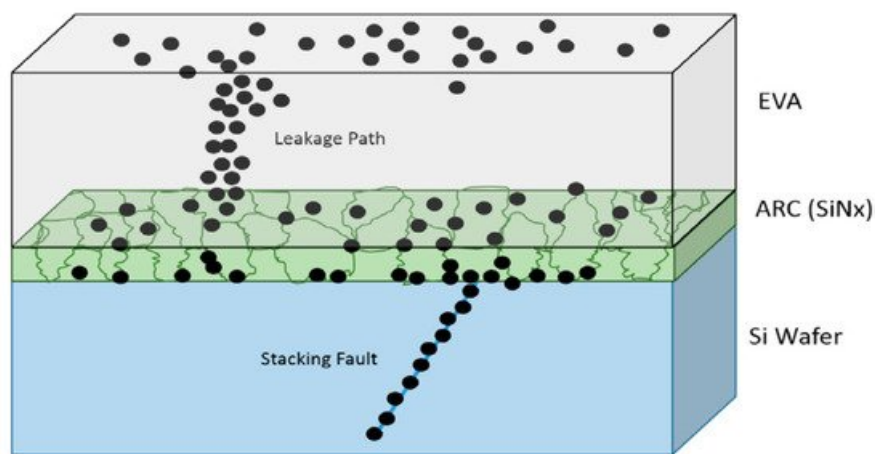


Figure 7. Image of the hypothetical PID process. Adapted with permission from ref. [75]. Copyright 2019, Elsevier.

3. EM Failure

EM failure is considered one of the degradation mechanism modes besides the corrosion failure in contact metallization and interconnects of PV systems. Degrading the contact layer increases the value of the series resistance, whereas EM failure can influence the series and shunt resistance [76]. Mainly EM failure has been widely investigated in the ICs, especially on the interconnect's technology of ICs since the aluminum metal is used in interconnection films. EM is a diffusion mechanism that occurs when the interconnecting tracks' current density is high enough to allow the metal atoms to migrate (diffusion) in the electron flow direction [19]. According to Michael G. Pecht's book [19], two factors are responsible for the occurrence of EM: the environmental and material factors.

However, material factors such as the chemical composition may trigger the metallization system's contact, e.g., Al, prone to EM. Next, a physical composition, the crystal grain size, e.g., the number of grain boundaries and void density in the metallization. Moreover, electron current is another environmental factor that causes Al ions to migrate [19]. EM in the metal electrode in solar cells could potentially occur with the same mechanism explained in [19].

J. Li et al. [77] used a buffer layer to establish an ohmic contact in the CdTe solar cells, where this buffer layer is used to reduce the barrier height. The author experimented with the Au, Ti, and Cr as a metallization layer along with ZnTe: Cu as a buffer layer. Experimental results show that the optimum thickness of the additive Cu to the metallization is, Au:15 nm, Ti:10 nm, and Cr:5 nm, where their efficiencies are 14.5%, 14.1%, and 14%, respectively. Hence, this is a good indication for a successful back contact creation. Later on, these samples undergo an ALT in dark and light stressing under a temperature of 85 °C. Dark stressing shows a sharp decrease in efficiency at the initial hours. Then, it stabilized after 100 h at 80–85%. Conversely, under illumination stress, it experiences a huge decline at the first 5 h and stabilization when the $t > 125$ for all the metals where Ti had the highest efficiency of 86% compared with others where they stabilized at 64% for Cr and 49% for Au. Thus, they reveal that the severe degradation under the illumination was because of the EM of (Cu+) since the cells are biased at almost the V_{OC} of the cell. However, this study did not consider environmental factors such as humidity, which we believe has a huge contribution to the EM [78]. Moreover, the combination of humidity, temperature, and voltage (HTV) can be found in aging tests, such as PID. The degradation of metallization within the c-Si PV modules and the corrosion of the TCO layer of TF PV modules are other types of PID effects [74], where ion migration is accelerated by these three combinations HTV [78]. Particularly, Ag fingers' corrosion and the migration of ions from interconnect ribbon to the grounded frame of PV module, which mostly happens in areas that are experiencing high moisture ingress.

3.1. EM in Metal Film Interconnects

In general, because of the high temperature and sometimes the high current density that passes through the interconnects, they are prone to EM since they are made of metals such as aluminum, copper, and silver [79][80][81][82]. Interconnection technology plays a significant role in the reliability of PV modules since it is responsible for transporting the current from one cell to another. Therefore, any damage or extra stress among the interconnects could lead to a massive drop in the efficiency in both levels of cells and modules, especially for c-Si PV. The integrity of the solder interconnection impacts the power conversion efficiency and output power as well [83]. In solar cells, especially for organic cells, Khaligh and Goldthorpe [84] showed that in an unsatisfactory short time, the silver nanowire electrodes fail specifically and wires with high-level sheet resistance and electrodes that are subject to high-level current densities fail faster. They also examined the characteristics of EM and attempted to correlate it with the failure of wires. Therefore, the reason behind the electrode's failure is that the silver nanowires are suffering from instability at higher temperatures provoked via Joule heating.

Certain challenges arise when using Cu metal as contacts in Si solar cells, especially as a front contact. Alison Lennon [85] identified three key challenges affecting the application of copper-plated Si PVs metallization, namely, (1) increase in carrier recombination due to the use of a copper metal for contact formation, (2) reliability issues due to failures of contact integrity or adhesion, and (3) shortage of cost-effective metal plating processes and equipment. Thus, for Si PV cell contacts, the technological benefits of utilizing Cu are not as convincing as using it for IC since PV cells could withstand relatively large feature sizes, thereby reducing the criticality of the contact's conductivity and EM properties metal. Conversely, PV cells face another challenge, like the need to function in the field for more than 25 years in different climatic conditions [85].

Another challenge is the interconnections of silicon PVs is the soldering process. Zarmai et al. [86] conducted a review work for the current reliability challenges of interconnection technologies and identification of the suitable technique for the solar cell interconnection assembly. Their results indicate

that the trending soldering technology of interconnection ribbon in silicon solar cells is the laser soldering since it produces a more reliable interconnection joint from the front to the back of the cell's surface. However, it induces mechanical and thermal stresses in the cell and joints, which results in series resistance and shadowing losses in crystalline silicon solar cells. Therefore, they suggested conducting more R&D to reduce the losses of series resistance [86]. In light of that, the rear and top metal contacts and the ribbons are made of copper (Cu), silver (Ag), or aluminum (Al), which are prone to EM.

EM phenomena have been reported in c-Si solar cells [25][26]. Numerous solar cell degradations could be correlated with the edge of the cell, usually erratic such as CdTe thin films. Exposure of the diode's front and back junctions at the corners and edges makes it more susceptible to environmental pressure and EM ending in a "very shunted, very leaky" microdiode, significantly affecting the efficiency of the other 99.95% of the cell [22]. Additionally, the most susceptible metal to migration is silver because the migration process required low activation energy [87]. Ag electroplating is used to reduce the contact finger's electrical resistance. However, because of the toxic CN^- ions of Ag plating, there is a safety issue that arises, and another environmental issue shows up because of the detoxication of the plating. Therefore, Kang et al. [25] studied the idea of using Cu metallization instead of Ag metallization for Si solar cells since Cu has better EM resistance.

Colwell et al. [88] studied the reliability of copper-plated front side metallization of Si solar cells by exposing them to long-range thermal tests. The sun's V_{OC} measurements experience a noticeable voltage bend-back shown in Figure 8 during higher intensities of more than one sun illumination followed by 200 °C for a 500 h thermal stress of laser-ablated cells with a Ni/Cu/Ag plated front metal panel. Therefore, throughout the thermal annealing, the authors revealed that huge voids could develop within the Ag capping layer and the primary Cu stack, where the effects of the presence of voids in the grid line (Ag's fingers) are increasing the series resistance and line resistance, which also reduce the FF [88][89].

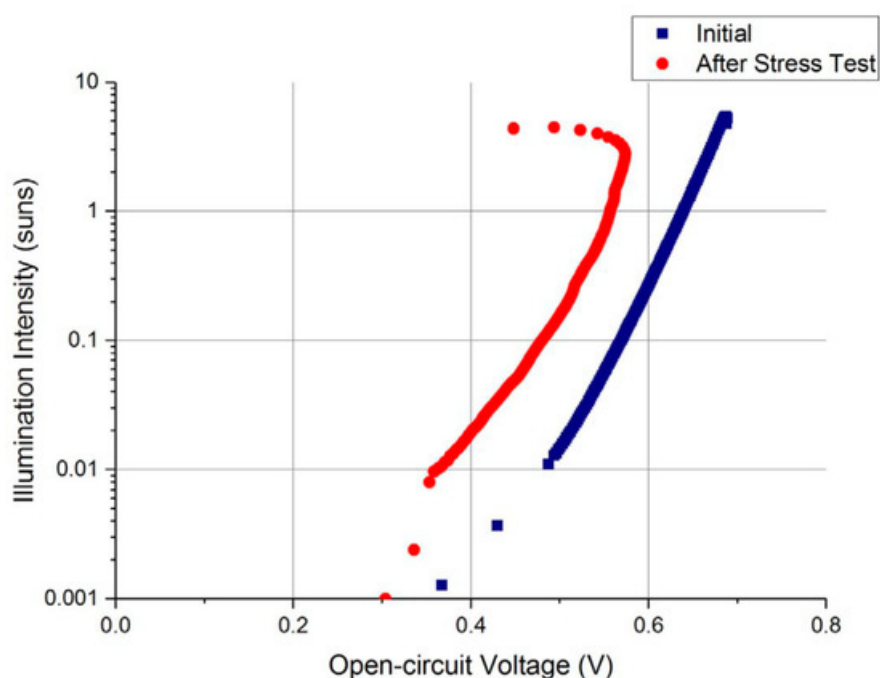


Figure 8. Cu-plated solar cell with a LIP Ag capping layer Suns- V_{OC} curve measurement (sintered) before and after thermal stress at 200 °C for 500 h. Adapted with permission from ref. [88]. Copyright 2018, Elsevier.

Nonetheless, another observation was that new metal layer consisting largely of diffused Cu straight over the Ag capping, as shown in Figure 9b,d for both immersion Ag cell and light-induced plating (LIP) cell; also, in Figure 10, the EDS map is the clearer image with the presence of the new layer. It was hypothesized that the voids grow through the capping metal was because of the grain boundary diffusion. This theory is backed by earlier low-temperature Cu diffusion studies along dislocations and grain

boundaries of polycrystalline metals such as Au [88]. The Schottky behavior's origin was theoretically due to higher contact resistance from the voids that are assumed to form as a consequence of Cu's grain boundary diffusion through the Ag capping layer. However, it has been shown that the voids could collapse by "scratching" the busbar with the measuring probe, after which Schottky behavior was no longer observed in Suns- V_{OC} curve measurements [88].

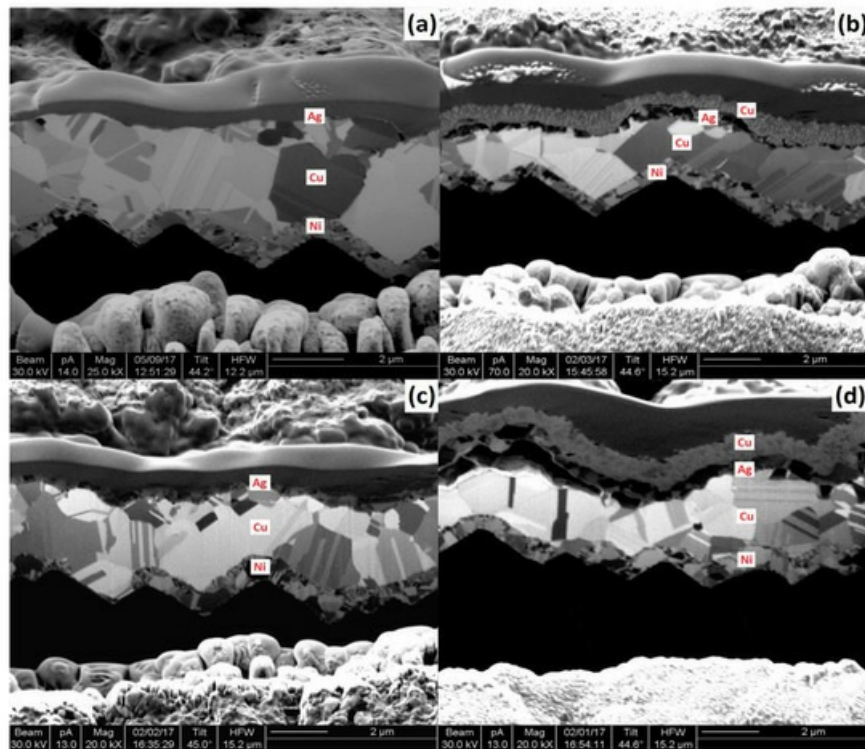


Figure 9. Ni/Cu/Ag plated and sintered contacts cross-sectional FIB pictures of before and after the thermal test—(a) immersion Ag (before), (b) immersion Ag (after), (c) LIP Ag (before), and (d) LIP Ag (after). Adapted with permission from ref. [88]. Copyright 2018, Elsevier.

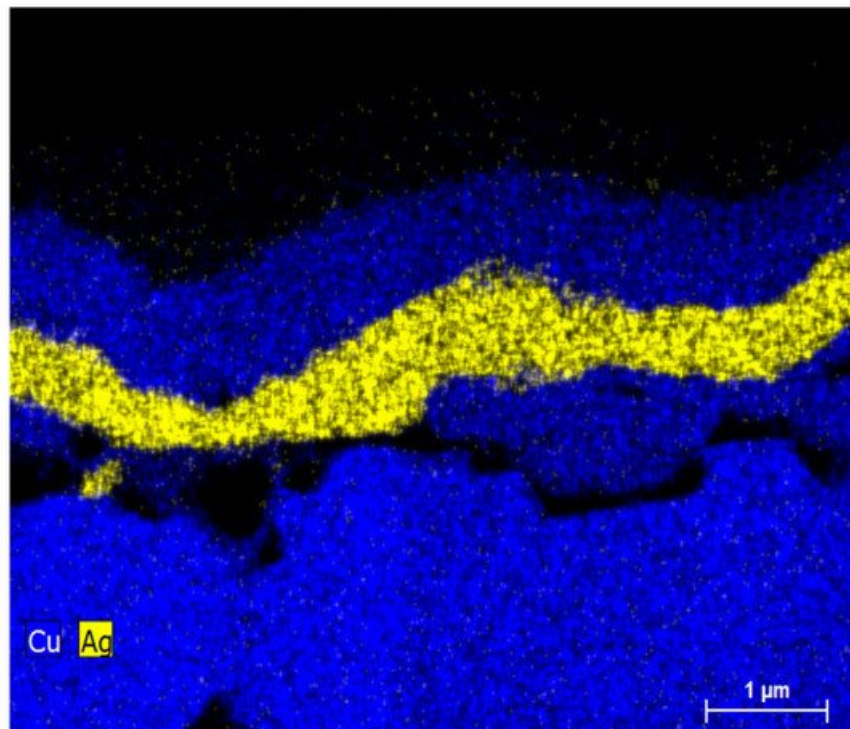


Figure 10. Ag/Cu interface EDS mapping of a sintered and plated contact (LIP capping). Adapted with permission from ref. [88]. Copyright 2018, Elsevier.

For Cu EM, the formation of voids attributed to Cu diffusion has been observed [90]. Although Cu diffusion through the capping metal could pose questions regarding the plated module's durability, it has been demonstrated that if the thermal test was implemented at a reduced temperature of 80 °C, then void formation can be prevented. Additionally, the grain boundary diffusion is motivated by the existence of the sinks. The encapsulant around the metal might remove the sink reactions presented in this cell experiment [88]. However, this study suggests investigating the possibility of Cu diffusion via the Ag capping layers in modules with encapsulation technology and the impact if it happened [88].

Dang et al. [91] conducted another reliability testing on the plated Ni/Cu/Ag metallization for c-Si solar cells. It was indicated that this structure could be a promising replacement for Ag metal contact because of its good resistivity for EM. According to their results during the cell processing, some of the nickel particles diffused in. Another observation was for the migration of copper to the silicon surface after aging at 235 °C; however, at the Ni/Si interface, there is less Cu separation when using soft-laser ablation compared with the hard-laser ablation method. Thereby, the diffusion of copper through the silver layer has led to the formation of Cu_2O_x on the Ag layer, creating massive voids at the interface of Cu/Ag as shown in Figure 11, because the specimens were brought out periodically for electrical measurement. Hence, the impacts of the Cu migration on the cell performance require further studies, particularly for the real-life operation [91].

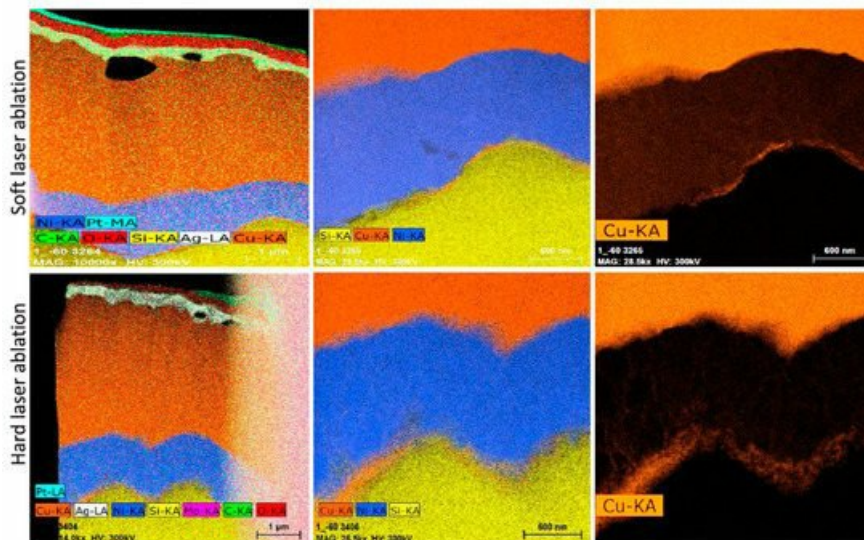


Figure 11. Cu/Ni/Si stack TEM images taken after accelerated aging at 235 °C. Adapted with permission from ref. [91]. Copyright 2018, Elsevier.

Kuan-Jen Chen et al. [26] studied a module's structure (Ag/solder/Cu-Zn/Al) with a hot dipping and an electroplated Sn PV ribbon that reflowed onto the Ag electrode on a silicon solar cell was tested to estimate its feasibility over the traditional (Ag/solder/Cu/Al) module. A bias-aging test evaluates the growth of intermetallic compounds (IMCs) promoted by the bias-induced thermal diffusion and EM. However, the Ag_3Sn joined with the photovoltaic Al ribbon and the silicon solar substrate, whereas the Cu_6Sn_5 IMC grows at the Cu/Sn interface. Additionally, the hot-dipped PV module has a thicker Ag_3Sn IMC at the Sn/Ag interface compared with the electroplated (EP) PV module, which would be correlated with a higher temperature return flow [26].

Additionally, compared with the previous results, EP and HD PV modules with Ag-direction biased had a higher growth mechanism of IMCs' Cu_6Sn_5 and Ag_3Sn because of EM's driving force direction. Especially, Ag_3Sn IMC overgrows following the biasing of the Ag direction, increasing the module's series resistance. Improving the Al-ribbon conductivity and decreasing IMC's overgrowth attitude in the EP PV module has led to reducing the module architecture's series resistance, having the potential for solar cell applications [26].

3.2. Characteristics of EM

Mainly, voids and hillocks are the characteristics of EM phenomena [92]. In metallic wires, the wind force causes preliminary damage (voids) on the cathode side and hillocks on the anode side, whereas the direct force produces void on the anode side and hillocks on the cathode side [93]. Quan Sun and his team [94] studied the effect of stress migration and thermal fatigue of silver thin films on the flexible substrate. Their results indicated that the combination of thermal fatigue and stress migration increases the number of atomic diffusions then causes the thin films to experience cracks, voids, and hillocks, which could cause the electrical conductivity to deteriorate [94]. According to Liu et al. [95], copper diffuses into the silver layer's vacancies after the annealing process, and then the vacancies transfer to the copper layer. Thereby, suppose the copper layer does not have sinks to absorb these vacancies. In this case, this will lead to the nucleation of voids at the copper/silver interface since the vacancies will be in supersaturated condition.

EM failure in rigidly passive metal interconnecting lines is analyzed with specific respect to vacancy supersaturations and hydrostatic stresses, which could be formed under EM circumstances while blocking grain boundaries [96]. It can be seen that the elevated stresses required for homogeneous void nucleation are likely too high for EM to create, and that breakdown is more likely to involve the growth of already presented voids. A study of the EM of the already existing small voids indicates that large voids migrate quicker than smaller voids above the critical size. This may lead to a disastrous mechanism where larger voids could catch up with smaller ones and coalesce with them, expand in size and move faster as they do so. Hence, Nix and Arzt assumed that the pre-existing voids migration and coalescence is possible for the mechanism of EM failure [96].

Several methods were introduced to study EM material diffusion because of the stress of the electrical current. In situ SEM EM inspections allow mass transport to be observed by examining the time-dependent development of voids and hillocks in metallic interconnections [97]. In Cu nanowires, Qiaojian Huang et al. [97] have extensively studied EM with a thickness of 50 nm and widths of 90 and 141 nm. The experiments in situ were carried out using the measurement of in situ resistance with SEM analysis. The mean time to fail approach was measured and used to calculate the activation energy. The activation energies for a nanowire width of 90 nm were 1.06 eV, whereas for a width of 141 nm, the activation energy was 0.94 eV. The findings support the author's statement that surface diffusion can be a significant failure mechanism of nanoscale wires from EM.

Archana Sinha et al. [40] illustrated the deterioration mechanism and impact of the subsequent mass transport of Ag from the cell gridline into EVA in high positive voltage bias stressed minimodules. The results from their study show that the corrosion of silver gridlines causes discoloration and enables adhesion failure (delamination) at the EVA/cell interface. This was attributed to the +1000 V bias, which drives the degradation and not just the DH ALT 85 °C/85% RH or 75 °C/85% RH on the samples. According to the chemical analysis, they assumed that Ag reacts with any sulfur available at the interface and then reacts with oxygen, leading to both the sulfide and the oxide species being mixed, where the source of the sulfur was from the back sheet. This finding is opposite to the -1000 bias where sodium ions migrating from the cover glass to the solar cell are liable for the deterioration. The module deterioration under +1000 bias is driven by the silver ions migrating from the cell gridlines toward the glass. As a result of the positive bias degradation in this study, the power loss was in the range of 30–32%, which is predominantly due to loss of I_{SC} .

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Keywords

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