Phase Equilibrium Studies in the RE₂O₃-REF₃-LiF System

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The solubility of rare earth oxides in molten salt directly affects the selection of operational parameters in the electrolysis process. When the added amount of RE_2O_3 is less than its solubility, it leads to a decreased electrolytic efficiency. Conversely, an excessive amount of oxide is prone to settle at the bottom of the electrolytic cell, impeding smooth production. The RE_2O_3 solubility in the fluoride salt can be represented by the phase equilibrium of the RE_2O_3 -REF₃-LiF system. The isothermal lines in the primary phase field of rare earth oxide represent the solubility of the oxide in the fluoride salt at the corresponding temperature.

Keywords: rare earth ; molten salt electrolysis ; phase equilibrium ; solubility

1. Introduction

Rare earth metals and alloys are increasingly used in the field of new materials, and there is a strong market demand. Rare earth elements have unique physical and chemical properties due to their special electronic structures, such as excellent optical and electrical properties, magnetic properties, and active chemical properties. With the development of modern science and technology, REEs have become indispensable key materials for high-tech and novel functional materials ^{[1][2]}.

In the process of producing rare earth metals through oxide–fluoride melt system electrolysis, REF₃ and LiF form an electrolyte with a low melting point, low density, and high electrical conductivity. Under the action of electrical current, the dissolved RE₂O₃ is converted to rare earth metals and oxygen at the cathode and anode, respectively. As the electrolysis process progresses, the dissolved RE₂O₃ in the molten salt is continuously consumed, requiring continuous addition of RE₂O₃ to maintain a high concentration in the electrolyte ^{[3][4][5]}. When the amount of RE₂O₃ added to the molten salt is lower than its solubility, the electrolysis efficiency and productivity are low. Conversely, if the amount of RE₂O₃ added to the molten salt the bottom of the electrolytic cell, increasing the cell resistance, affecting the metal purity, and even seriously impeding the smooth progress of production ^{[6][Z]}. Therefore, the solubility of RE₂O₃ in the REF₃-LiF-RE₂O₃ system provides the essential data for establishing a suitable feeding system in electrolytic production, playing an important role in improving electrolysis efficiency and maintaining the effective volume of the electrolytic cell. However, there have been significant differences in the solubility data of RE₂O₃ in the fluoride system, and the semi-empirical models developed based on these data have difficulty in accurately predicting the solubility of rare earth oxides ^{[8][9]}.

2. Nd₂O₃-NdF-LiF System

Due to the importance of neodymium-iron-boron magnetic materials, there has been an increasing amount of research on the phase equilibrium of the Nd₂O₃-NdF-LiF system, which is relevant to the production of neodymium through molten salt electrolysis ^{[10][11]}. Solubility data of Nd₂O₃ in the NdF₃-LiF system reported in the literature are summarized in **Table 1. Figure 1** summarizes the solubility data of Nd₂O₃ in the NdF₃-LiF system and annotates these data in the Nd₂O₃-NdF-LiF ternary phase diagram. It can be observed that large amounts of experimental data have been published in the range of 750–1200 °C and 60–90 wt.% NdF₃. In the liquid phase, the concentration of Nd₂O₃ mostly remains below 5 wt.% and increases with the temperature and percentage of NdF₃. However, the solubility data published by Wu et al. ^[12] significantly deviate from other data, with a decrease in Nd₂O₃ concentration as NdF₃ increases, indicating the unreliability of these data. The abundance of experimental data shown in **Figure 1** indicates the importance of phase equilibrium research in the Nd₂O₃-NdF-LiF system, both in terms of theoretical significance and practical applications, which has attracted numerous researchers to invest substantial efforts into studying this area. However, there are significant differences and even contradictions among these experimental data ^{[12][13][14][15][16][17][18][19][20][21][22][23]}, as detailed in the following two figures.



Figure 1. Liquidus points on the phase diagram of the NdF₃-LiF-Nd₂O₃ system in the NdF₃-rich corner (experimental data from $\frac{12[13][14][15][16][17][18][19][20][21][22][23]}{12}$).

wt.%			mol%			Normaliz	ation (wt.9	6)	Т.	
NdF ₃	LiF	Nd ₂ O ₃	NdF_3	LiF	Nd ₂ O ₃	NdF_3	LiF	Nd ₂ O ₃	(°C)	Ref.
58	42	0.54	15	85	0.08	57	42	0.54	800	[<u>13</u>]
58	42	0.75	15	85	0.12	57	42	0.74	850	[13]
58	42	0.82	15	85	0.13	57	42	0.81	860	[13]
58	42	0.96	15	85	0.15	57	42	0.95	900	[<u>13</u>]
63	37	1.68	18	82	0.29	62	36	1.65	1000	[<u>16</u>]
63	37	2.27	18	82	0.40	62	36	2.21	1050	[16]
63	37	2.57	18	82	0.45	61	36	2.51	1100	[<u>16</u>]
65	35	2.07	19	81	0.37	63	35	2.03	800	[<u>21</u>]
66	34	1.83	20	80	0.34	65	33	1.8	1000	[<u>14]</u>
66	34	1.92	20	80	0.35	65	33	1.88	1050	[14]
66	34	2.03	20	80	0.37	65	33	1.99	1100	[<u>14]</u>
66	34	2.12	20	80	0.39	65	33	2.08	1150	[<u>14]</u>
68	32	1.96	22	78	0.38	67	31	1.92	1000	[<u>13</u>]
68	32	2.59	22	78	0.50	66	31	2.52	1050	[13]
68	32	2.73	22	78	0.53	66	31	2.65	1100	[<u>13</u>]
70	30	9.24	23	77	1.96	64	28	8.46	850	[<u>12</u>]
70	30	1.4	23	77	0.28	69	30	1.38	850	[22]
70	30	4.4	23	77	0.90	67	29	4.21	1050	[22]
70	30	0.68	23	77	0.14	69	30	0.68	750	[<u>16</u>]
70	30	0.8	23	77	0.16	69	30	0.79	800	[<u>16</u>]
70	30	0.92	23	77	0.18	69	30	0.91	850	[<u>16</u>]
70	30	1.11	23	77	0.22	69	30	1.1	900	[<u>16</u>]
70	30	2.8	23	77	0.57	68	29	2.72	1100	[20]

Table 1. Solubility of Nd₂O₃ in NdF₃-LiF fluoride melts.

wt.%			mol%			Normaliza	ation (wt.%	ó)	Т.	
NdF ₃	LiF	Nd ₂ O ₃	NdF ₃	LiF	Nd ₂ O ₃	NdF ₃	LiF	Nd ₂ O ₃	(°C)	Ref.
70	30	3.1	23	77	0.63	68	29	3.01	1150	[20]
70	30	3.5	23	77	0.71	68	29	3.38	1200	[<u>20]</u>
72	28	2.07	25	75	0.44	71	27	2.03	1000	[<u>14]</u>
72	28	2.17	25	75	0.46	71	27	2.12	1050	[<u>14]</u>
72	28	2.29	25	75	0.48	70	27	2.24	1100	[<u>14]</u>
72	28	2.4	25	75	0.51	70	27	2.34	1150	[<u>14]</u>
73	27	2.18	26	74	0.47	71	26	2.14	1000	[<u>16]</u>
73	27	2.79	26	74	0.60	71	26	2.71	1050	[<u>16]</u>
73	27	3.08	26	74	0.67	71	26	2.99	1100	[<u>16]</u>
75	25	7.2	28	72	1.69	70	23	6.72	800	[<u>12]</u>
75	25	8.3	28	72	1.96	69	23	7.66	850	[<u>12]</u>
75	25	9.4	28	72	2.24	69	23	8.59	900	[<u>12]</u>
77	23	1.45	30	70	0.34	76	23	1.43	860	[<u>13]</u>
77	23	1.61	30	70	0.38	76	23	1.58	900	[<u>13]</u>
77	23	2.27	30	70	0.54	75	23	2.22	1000	[<u>14]</u>
77	23	2.39	30	70	0.57	75	23	2.33	1050	[<u>14]</u>
77	23	2.51	30	70	0.60	75	23	2.45	1100	[<u>14]</u>
77	23	2.62	30	70	0.63	75	23	2.55	1150	[<u>14]</u>
78	22	2.45	31	69	0.60	76	21	2.39	1000	[<u>16]</u>
78	22	2.3	31	69	0.56	76	22	2.25	1050	[<u>16]</u>
78	22	3.52	31	69	0.87	75	21	3.4	1100	[<u>16]</u>
80	20	7.29	34	66	1.95	75	19	6.79	850	[<u>12</u>]
81	19	2.49	35	65	0.66	79	19	2.43	1000	[<u>14]</u>
81	19	2.62	35	65	0.70	79	19	2.55	1050	[<u>14]</u>
81	19	2.73	35	65	0.73	79	19	2.66	1100	[<u>14]</u>
81	19	2.78	35	65	0.74	79	19	2.7	1150	[<u>14]</u>
83	17	1.1	39	61	0.31	82	17	1.09	957	[<u>18]</u>
83	17	1.75	39	61	0.49	81	17	1.72	979	[<u>18]</u>
83	17	3.4	39	61	0.97	80	17	3.29	1053	[<u>18]</u>
83	17	3.04	39	61	0.86	81	16	2.95	1000	[<u>16]</u>
83	17	3.36	39	61	0.96	80	16	3.25	1050	[<u>16]</u>
83	17	2.45	39	61	0.69	81	17	2.39	1100	[<u>15]</u>
83	17	4.09	39	61	1.17	80	16	3.93	1100	[<u>16]</u>
84	16	2.7	40	60	0.79	82	16	2.63	1000	[<u>14]</u>
84	16	2.81	40	60	0.82	82	16	2.73	1050	[<u>14]</u>
84	16	2.92	40	60	0.86	81	16	2.84	1100	[<u>14]</u>
84	16	3.05	40	60	0.90	81	16	2.96	1150	[<u>14]</u>
85	15	3.28	42	58	1.00	82	15	3.18	1050	[<u>17]</u>

wt.%		mol%				Normaliza	т.			
NdF ₃	LiF	Nd ₂ O ₃	NdF_3	LiF	Nd ₂ O ₃	NdF_3	LiF	Nd ₂ O ₃	(°C)	Ref.
85	15	3.88	42	58	1.18	82	15	3.74	1100	[<u>17]</u>
85	15	4.54	42	58	1.39	81	14	4.34	1150	[<u>17]</u>
88	12	3.82	49	51	1.29	85	12	3.68	1050	[<u>16</u>]
88	12	4.54	49	51	1.54	84	11	4.34	1100	[<u>16]</u>
88.5	11.5	3.74	50	50	1.29	85	11	3.61	1050	[17]
88.5	11.5	4.23	50	50	1.46	85	11	4.06	1100	[<u>17</u>]
88.5	11.5	4.71	50	50	1.63	85	11	4.5	1150	[<u>17</u>]
88.5	11.5	7.4	51	49	2.66	82	11	6.89	1200	[23]
90	10	4.2	54	46	1.54	86	10	4.03	1100	[20]
90	10	4.4	54	46	1.61	86	10	4.21	1150	[20]
90	10	4.7	54	46	1.73	86	10	4.49	1200	[20]
92	8	4.2	60	40	1.67	88	8	4.03	1050	[<u>17</u>]
92	8	4.62	60	40	1.84	88	8	4.42	1100	[<u>17]</u>
92	8	4.97	60	40	1.99	88	8	4.73	1150	[17]

Figure 2 represents the solubility data of Nd_2O_3 in the NdF_3 -LiF molten salt at 1100 and 1150 °C, plotted on the ternary phase diagram. According to all the available literature, at the same NdF_3 /LiF ratio, the solubility of Nd_2O_3 increases with increasing temperatures, and connecting the solubility data at the same temperature should obtain a smooth liquidus line (isotherm). However, it is difficult to determine a consistent liquidus line at 1100 and 1150 °C, based on the data shown in the figure. Some data points indicate a higher solubility of Nd_2O_3 at 1100 °C compared with 1150 °C. The estimated 1100 and 1150 °C isotherms are shown in the figure. These contradictory data not only pose challenges for production technicians but also cannot be used for developing thermodynamic databases.



Figure 2. Liquidus points and estimated 1100 and 1150 °C isotherms on the phase diagram of NdF₃-LiF-Nd₂O₃ system (experimental data from $\frac{14}{15}\frac{15}{16}\frac{17}{20}$).

Figure 3 shows the solubility data of Nd₂O₃ in the NdF₃-LiF system on a pseudo-binary phase diagram of Nd₂O₃-(NdF₃ + LiF), with NdF₃/LiF ratios of 2.3 and 3.3. It can be observed that the liquidus temperatures increase sharply with an increase in the concentration of Nd₂O₃. For every 1 wt.% increase in Nd₂O₃, the liquidus temperature rises by approximately 150 °C. In other words, the solubility of Nd₂O₃ is not sensitive to temperature, as increasing the temperature by 150 °C only results in a 1 wt.% increment in Nd₂O₃ solubility. The current consensus in the research is that, at the same temperature, a higher NdF₃/LiF ratio leads to a greater solubility of Nd₂O₃. From the figure, it can be

observed that at lower temperatures (800–900 °C), the solubility of Nd₂O₃ in NdF₃/LiF = 3.3 is higher than that in NdF₃/LiF = 2.3. However, at higher temperatures (1100–1150 °C), the solubility of Nd₂O₃ in NdF₃/LiF = 3.3 is lower than that in NdF₃/LiF = 2.3, indicating a significant discrepancy in the experimental data among different researchers. The dashed lines in the figure represent the estimated liquidus lines corresponding to NdF₃/LiF ratios of 2.3 and 3.3, based on the experimental data.



Figure 3. Pseudo-binary phase diagram of NdF₃-(LiF + Nd₂O₃) at fixed NdF₃/LiF of 2.3 and 3.3 [13][14][20].

3. La₂O₃-LaF-LiF System

Figure 4 presents the solubility data of La_2O_3 in the LaF_3 -LiF system annotated on a ternary phase diagram based on the summary of the literature data shown in **Table 2**. Within the range of 948–1250 °C and 60–90 wt.% LaF_3 , the solubility of La_2O_3 in the LaF_3 -LiF system ranges from 1.3 to 3.4 wt.%. With an increase in temperature and LaF_3 , there is a tendency for the solubility of La_2O_3 to increase, but the change is not significant $\frac{[14][24][25][26]}{2}$.



Figure 4. Liquidus points shown on the phase diagram of LaF₃-LiF-La₂O₃ system in LaF₃-rich corner (experimental data from $\frac{14![24][25][26]}{14!}$).

wt.% Т. mol% Normalization (wt.%) LaF₃ LiF La₂O₃ LaF₃ LiF La₂O₃ LaF₃ LiF La₂O₃ (°C) Ref. [<u>24]</u> 1.4 0.26 1.38 [24] 1.58 0.29 s [<u>24</u>] 1.78 0.33 1.75 [<u>24]</u> 1.94 0.36 1.9 [<u>24</u>] 2.1 0.39 2.06 [<u>14]</u> 1.79 0.33 1.76 [14] 1.87 0.35 1.84 <u>[14]</u> 1.94 0.36 1.9 [<u>14]</u> 2.01 0.37 1.97 [<u>24]</u> 1.54 0.32 1.52 [<u>24</u>] 0.36 1.73 1.76 [<u>24]</u> 1.94 0.40 1.9 [24] 2.2 0.45 2.15 [<u>24</u>] 2.35 0.49 2.3 [25] 1.95 1.99 0.43 [<u>25</u>] 2.08 0.45 2.04 [<u>26]</u> 1.64 0.35 1.61 [25] 2.17 0.47 2.12 [<u>14]</u> 2.01 0.43 1.97 [<u>14]</u> 2.13 0.46 2.09 [<u>14]</u> 2.26 0.49 2.21 [<u>14]</u> 2.37 0.51 2.32 [<u>24</u>] 1.65 0.38 1.62 [24] 1.95 0.45 1.91 [<u>24</u>] 2.23 0.52 2.18 [24] 2.5 0.58 2.44 [<u>24</u>] 2.65 0.62 2.58 [<u>14]</u> 0.53 2.23 2.18 [25] 2.12 0.50 2.08 [25] 2.3 0.55 2.25 [<u>26]</u> 1.81 0.43 1.78 [25] 2.36 0.56 2.31 <u>[14]</u> 2.35 0.56 2.3 [<u>14]</u> 2.48 0.59 2.42 [<u>14]</u> 2.58 0.62 2.52 [<u>24</u>] 2.31 2.26 0.61 [24] 2.53 0.67 2.47

Table 2. Solubility of La₂O₃ in LaF₃-LiF fluoride melts.

wt.%		mol%				Normaliza	т.			
LaF ₃	LiF	La ₂ O ₃	LaF ₃	LiF	La ₂ O ₃	LaF ₃	LiF	La ₂ O ₃	(°C)	Ref.
80	20	2.75	35	65	0.73	78	19	2.68	1150	[24]
80	20	2.93	35	65	0.78	78	19	2.85	1200	[24]
80	20	3.06	35	65	0.82	78	19	2.97	1250	[24]
80	20	2.56	35	65	0.68	78	19	2.5	1050	[14]
80	20	2.15	35	65	0.57	79	19	2.1	1062	[25]
80	20	2.45	35	65	0.65	78	19	2.39	1082	[25]
80	20	1.97	35	65	0.52	79	19	1.93	1090	[14]
80	20	2.69	35	65	0.71	78	19	2.62	1100	[14]
80	20	2.58	35	65	0.69	78	19	2.52	1102	[25]
80	20	2.78	35	65	0.74	78	19	2.7	1150	[<u>14]</u>
83	17	2.14	39	61	0.62	81	17	2.1	1100	[<u>15]</u>
83	17	2.73	39	61	0.79	81	16	2.66	1050	[14]
83	17	2.85	39	61	0.83	81	16	2.77	1100	[<u>14]</u>
83	17	3.01	39	61	0.88	81	16	2.92	1150	[14]
85	15	2.68	43	57	0.83	83	15	2.61	1100	[24]
85	15	2.85	43	57	0.88	83	15	2.77	1150	[24]
85	15	3.08	43	57	0.96	82	15	2.99	1200	[24]
85	15	3.25	43	57	1.01	82	15	3.15	1250	[24]
90	10	3.2	54	46	1.19	87	10	3.1	1200	[24]
90	10	3.5	54	46	1.30	87	10	3.38	1250	[24]

Figure 5 annotates the solubility data of La_2O_3 on a pseudo-binary phase diagram of La_2O_3 -($LaF_3 + LiF$), with the LaF_3/LiF weight ratios of 1.9 and 3.2. It can be observed that the liquidus temperature increases sharply with an increase in the concentration of La_2O_3 . For every 1 wt.% increase in La_2O_3 in the melt, the liquidus temperature rises by approximately 300 °C. In other words, the solubility of La_2O_3 is not sensitive to temperature, as increasing the temperature by 300 °C only results in a 1 wt.% increment in La_2O_3 solubility. At the same temperature, a higher LaF_3/LiF weight ratio leads to a greater solubility of La_2O_3 , but scattered data make it difficult to obtain precise liquidus lines. The dashed lines in the figure represent the estimated liquidus lines corresponding to LaF_3/LiF weight ratios of 1.9 and 3.2, based on the experimental data.



Figure 5. Pseudo-binary phase diagram of (LaF₃ + LiF)-La₂O₃ at fixed LaF₃/LiF of 1.9 and 3.2 [14][24][25]

4. Y₂O₃-YF₃-LiF System

Figure 6 presents the solubility data of Y_2O_3 in the YF₃-LiF system annotated on a ternary phase diagram, and the data from the literature are summarized in **Table 3** ^{[27][28]}. Within the range of 725–1009 °C and 60–90 wt.% YF₃, the solubility of Y_2O_3 in the YF₃-LiF system ranges from 0.45 to 5.09 wt.%. Data published by the same group of researchers indicate that the solubility of Y_2O_3 in YF₃-LiF increases with temperature and YF₃. However, as can be seen from the figure, there are significant differences in the data from different researchers. **Figure 7** annotates partial solubility data of Y_2O_3 on a pseudo-binary phase diagram of Y_2O_3 -(YF₃ + LiF), with YF₃/LiF weight ratios of 1.9 and 5.6. From the figure, it can be observed that the liquidus temperature increases with an increase in the concentration of Y_2O_3 , but the extent of increase is not as significant as in the La₂O₃-LaF₃-LiF and Nd₂O₃-NdF₃-LiF systems. Therefore, the solubility of Y_2O_3 in the YF₃/LiF ratio leads to a greater solubility of Y_2O_3 , but there are significant differences in the data from the researchers in the data from the two groups of researchers in the figure. The dashed lines in the figure represent the estimated liquidus lines corresponding to the YF₃/LiF weight ratios of 1.9 and 5.6, based on the experimental data.



Figure 6. Liquidus points shown on the phase diagram of YF_3 -LiF- Y_2O_3 system in YF_3 -rich corner.



Figure 7. Pseudo-binary phase diagram of $(YF_3 + LiF)-Y_2O_3$ at fixed YF_3/LiF of 1.9 and 5.6 $\frac{[28][29]}{2}$.

nart 04			mol04			Normalization (vt 0/)				
WL.%			m01%			Normaliza	1.	1.		
YF3	LiF	Y ₂ O ₃	YF3	LiF	Y ₂ O ₃	YF3	LiF	Y ₂ O ₃	(°C)	Ref.
58	42	1.17	20	80	0.26	58	41	1.16	725	[29]
58	42	1.25	20	80	0.28	58	41	1.23	750	[29]
58	42	1.48	20	80	0.33	58	41	1.46	800	[29]
58	42	1.87	20	80	0.42	57	41	1.84	875	[29]
58	42	2.09	20	80	0.47	57	41	2.05	920	[29]
58	42	2.35	20	80	0.53	57	41	2.3	950	[29]
58	42	2.87	20	80	0.65	57	40	2.79	1000	[29]
65	35	1.28	25	75	0.32	64	34	1.26	750	[29]

wt.%			mol%			Normaliza	ation (wt.%)	т.		
YF ₃	LiF	Y ₂ O ₃	YF ₃	LiF	Y ₂ O ₃	YF ₃	LiF	Y ₂ O ₃	(°C)	Ref.
65	35	0.45	25	75	0.11	65	35	0.45	810	[<u>28]</u>
65	35	1.63	25	75	0.41	64	34	1.6	825	[<u>29]</u>
65	35	0.5	25	75	0.12	65	35	0.5	831	[<u>28</u>]
65	35	1.79	25	75	0.45	64	34	1.76	850	[<u>29</u>]
65	35	0.59	25	75	0.15	65	35	0.59	850	[<u>28</u>]
65	35	0.8	25	75	0.20	65	35	0.79	882	[<u>28]</u>
65	35	0.8	25	75	0.20	65	35	0.79	900	[28]
65	35	2.11	25	75	0.53	64	34	2.07	900	[29]
65	35	0.88	25	75	0.22	65	34	0.87	900	[28]
65	35	1.65	25	75	0.41	64	34	1.62	1000	[<u>28]</u>
65	35	2.96	25	75	0.75	63	34	2.87	1000	[29]
65	35	1.65	25	75	0.41	64	34	1.62	1000	[28]
75	25	1.69	35	65	0.51	74	24	1.66	1000	[<u>28</u>]
79	21	1.72	40	60	0.57	78	21	1.69	750	[29]
79	21	2.14	40	60	0.71	77	21	2.1	800	[29]
79	21	2.26	40	60	0.75	77	21	2.21	825	[29]
79	21	2.93	40	60	0.98	77	20	2.85	900	[<u>29</u>]
79	21	3.52	40	60	1.18	76	20	3.4	950	[29]
79	21	4.9	40	60	1.66	75	20	4.67	1000	[29]
85	15	3.72	50	50	1.45	82	15	3.59	900	[<u>29]</u>
85	15	1.19	50	50	0.46	84	15	1.18	900	[<u>28]</u>
85	15	1.41	50	50	0.54	84	15	1.39	929	[<u>28]</u>
85	15	1.51	50	50	0.58	84	15	1.49	943	[<u>28]</u>
85	15	4.45	50	50	1.75	81	14	4.26	950	[<u>29]</u>
85	15	1.61	50	50	0.62	84	15	1.58	964	[<u>28]</u>
85	15	1.78	50	50	0.69	83	15	1.75	974	[<u>28]</u>
85	15	1.88	50	50	0.73	83	15	1.85	988	[<u>28]</u>
85	15	5.36	50	50	2.11	81	14	5.09	1000	[<u>29]</u>
85	15	1.98	50	50	0.77	83	15	1.94	1000	[<u>28]</u>
85	15	2	50	50	0.77	83	15	1.96	1000	[28]
85	15	2.09	50	50	0.81	83	15	2.05	1009	[28]
91	9	2.2	64	36	1.02	89	9	2.15	1000	[<u>28</u>]

5. Solubility Model of RE₂O₃-REF₃-LiF System

High-temperature phase equilibrium experiments not only consume a significant amount of time and funding, as mentioned above, they also yield substantial variations in the data among different researchers and experimental methods, which brings confusion to the applications of these data. Various thermodynamic models, such as FactSage ^[30] (31), MTDATA ^[32], and Thermo-Calc ^[33], have been developed to predict the thermodynamic properties of slags, molten salts, and alloys. The solubility of rare earth oxides in molten salts can theoretically be predicted using thermodynamic models. However, the construction of the core database for these thermodynamic models relies heavily on a large amount

of experimental data. The lack of accurate thermodynamic data for rare earth oxide–molten salt systems currently hinders the ability of existing thermodynamic models to predict their properties, including solubility. Researchers have attempted to establish semi-empirical models ^{[B][9]} to predict the solubility of rare earth oxides in molten salts based on available experimental data. **Figure 8** summarizes the solubility of various rare earth oxides in fluoride salts, where **Figure 8** shows the relationship between solubility and temperature, and **Figure 8** b demonstrates the relationship between the logarithm of solubility and the reciprocal of temperature ^[9]. It can be observed that the solubility of rare earth oxides in molten systems. For most systems, the logarithm of solubility exhibits a linear relationship with the reciprocal of temperature.



Figure 8. Solubility of rare earth oxides (sREO) in fluoride melts as a function of temperature: (**a**) solubility vs. temperature and (**b**) logarithm of solubility vs. reciprocal of the temperature [9].

Figure 9 illustrates the relationship between the solubility of Nd_2O_3 and Y_2O_3 and the concentration of rare earth fluoride (REF₃). Within the studied concentration and temperature ranges, the solubility of the oxides increases with an increase in the concentration of REF₃ in the molten salt. At higher temperatures, the solubility of rare earth oxides is more sensitive to the concentration of REF₃ in the molten salt. As shown in **Figure 9**, the solubility data for different rare earth oxides in fluoride salts exhibit considerable variability, making it difficult to be expressed by a unified model. Guo et al. ^[9] proposed semi-empirical prediction models for each rare earth oxide with available solubility experimental data. For example, they developed a solubility prediction model for Nd_2O_3 in the NdF_3 -LiF-(MgF₂/CaF₂) system using the data from three articles ^[12][13]^[12]. The comparison between the predicted and experimental results is shown in **Figure 10**, with an average error of 8%. However, the error can reach 30% for low solubility cases.



Figure 9. Solubility of rare earth oxides in fluoride melts as a function of REF₃ content (data from Refs. [13][17][28][29]).



Figure 10. Relative error between the experimental data and the data calculated with the current model for Nd_2O_3 solubility ^[9].

As shown in **Figure 1**, the solubility data of Nd₂O₃ in the NdF₃-LiF system reported in the literature are much more extensive than those used by Guo et al. ^[9]. **Figure 11** compares the solubility calculated by Guo et al.'s model ^[9] with all the experimental solubility data of Nd₂O₃ in the NdF₃-LiF system. It can be seen that the solubilities calculated by Guo et al.'s model show a big difference compared with the experimental data in low NdF₃ fluoride salt.



Figure 11. Nd_2O_3 solubility in melts with different NdF_3 concentration and at different temperatures (data from references [12][13][14][16][17][20][22]).

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