

In Situ Polymerization for Composites

Subjects: Materials Science, Composites

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Due to the extremely low viscosity of the cyclic lactams and the superior mechanical properties of the polymers obtained from them, these materials have great potential for application in different liquid composite molding (LCM) techniques. Unsurprisingly, extensive academic research has been conducted over the past years to investigate possible industrial applications of anionically polymerized thermoplastic composites (TPCs) reinforced with glass, carbon, aramid, or natural fibers. It is important to remember that enormous progress has been made in the development of machinery and materials. There are different types of reactive processes for obtaining Nylon-6 composites; some of the main technologies are presented.

Keywords: thermoplastic resin ; casting ; chemical properties ; anionic polyamide 6 ; vacuum infusion ; composite LCA

1. Reactive Injection Pultrusion

The thermoplastic reaction injection pultrusion provides an alternative for the preparation of thermoplastic composites with high fiber content. Pultrusion is one of the most cost-effective and energy-efficient methods of manufacturing continuous fiber-reinforced composite profiles. Over the past 70 years, thermosetting resins have dominated the pultrusion industry, owing to their rapid curing and effective impregnation, along with low viscosity. However, thermosetting resins have several disadvantages. They are brittle, sensitive to impact, and cannot be recycled. In addition, volatile compounds would be released during the pultrusion process of many thermosetting resins, and this is contrary to environmental protection policies. Thermoplastic polymers completely avoid the above shortcomings and offer improved impact strength, damage tolerance, toughness, and reparability ^[1]. Nevertheless, a relative high viscosity (100–10,000 Pa·s) of molten thermoplastics ^[2] limits the impregnation ability, resulting in the poor quality of the pultruded products. Several impregnation techniques for thermoplastic pultrusion have been developed by researchers. One way was to put the polymer and fibers in intimate contact prior to the final molding step. Pre-impregnated materials, such as prepreg tapes, commingled fibers, and powder coated towpregs, had been well-developed for pultrusion processes ^{[3][4][5][6]}. However, there was still a large gap in achieving good impregnation with high fiber content between thermoplastic polymers and thermosetting resins ^[1].

In order to solve this problem, reactive processing of thermoplastic composites with anionic ring-opening polymerization of polyamide-6 (PA-6) has been developed by researchers ^{[7][8]}. The impregnation of high content fibers can be easily achieved through caprolactam (monomer of PA-6) with extremely low viscosity (5 m Pa·s) ^[8]. Luisier et al. developed a pilot reactive injection pultrusion line in the base of anionic polymerization of polyamide-12 (PA-12) ^[9]. Eppe et al. successfully prepared thermoplastic composites with anionic PA-6, using a pultrusion process, but the optimization of process condition, properties, and microstructure of pultruded composites were not reported in detail ^[10].

2. Infusion Techniques

The infusion techniques described in this section are already optimized for thermosets, while, for thermoplastics, researchers are still trying to implement them, as there are some difficulties.

Three reactive processes are introduced: structural reaction injection molding, resin film infusion, and vacuum infusion (see **Figure 1**). Reactive processes for the manufacturing of short-fiber-reinforced composite parts, such as reinforced reaction injection molding (RRIM) ^{[11][12][13][14]}, are discussed in the literature.

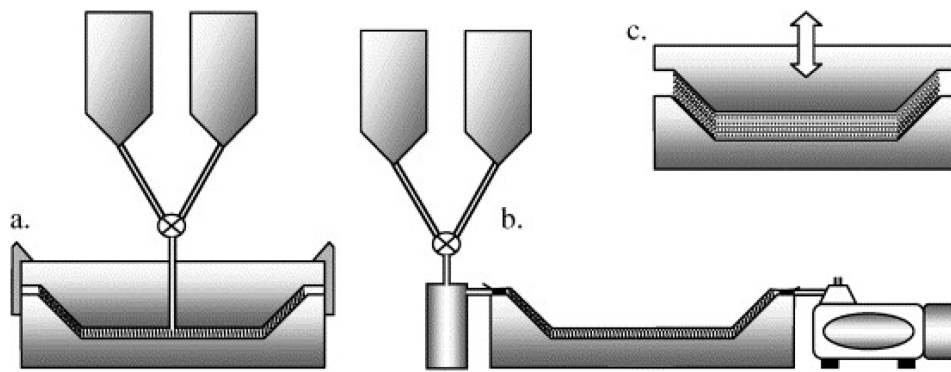


Figure 1. Schematic representation of three reactive processes for manufacturing of thermoplastic composites: (a) structural reaction injection molding (SRIM), (b) vacuum infusion (VI) and (c) resin film infusion (RFI). Reprinted from Reference [15], under open-access license.

2.1. Structural Reaction Injection Molding (SRIM)

The mixture is infused onto the dry fiber bed, which is placed between two solid mold halves, at high pressure (8–10 bar) (see **Figure 1a**) [16][17][18][19][20][21][22][23][24][25][26][27][28][29]. The process is closely related to Resin Transfer Molding (RTM) of thermoset composites [1]. To obtain a proper fiber impregnation, 1 Pa s is generally regarded as the maximum viscosity limit of the reactive mixture [30]. At the end of the polymerization, the composite part can be demolded. As the size of the product increases, the clamping force required to keep the mold closed during resin injection also increases. As a result, the dimensions of parts produced via SRIM are limited. The reactive material systems are separated into two material feeds to prevent premature polymerization. Just before entering the mold, material feeds from two tanks are mixed and polymerization begins. The great advantage of SRIM is the fast cycle time, and the high tooling costs are the main disadvantage.

Injection Molded Thermoplastic Composites

Injection molding, which allows for the fast, low-cost production of composite parts, is, however, a commonly used technique to produce short-fiber-reinforced thermoplastics. Their applications are growing rapidly, because of the good feature of the net-shaped components with good dimensional accuracy and relatively short cycle time [31]. Short-fiber reinforcement of thermoplastics materials is extensively used because it results in composites with high impact resistance, good dimensional stability, a high strength-to-weight ratio, and good thermal insulation properties of the molded parts comparable to unreinforced plastics and some conventional metal alloys. However, the mechanical properties of short-fiber composites are not as good as composite with continuous reinforcing fibers [32]. According to Fu et al. [33], the specific work of fracture or the fracture toughness of short-fiber composites is caused by all of the following failure mechanisms: (1) fiber–matrix interfacial debonding, (2) post-debonding friction, (3) matrix plastic deformation, (4) fiber plastic deformation, (5) fiber fracture, (6) matrix fracture, and (7) fiber pull-out, and it is closely related to the fiber volume fraction and the fiber length. In general, the failure mechanisms depend not only on the properties of the constituents but also on the bonding efficiency across the interface, as well as the fiber volume fraction, the fiber length, and the fiber orientation.

This technology currently allows for the production of PA-6 matrix thermoplastic composites reinforced with short glass fibers such as polyamide PA-6 Nylon composite pellets. It is reiterated that, to produce this type of material, the process does not start from the monomer, but directly from the polymerized thermoplastic, which, in turn, is mixed with the short fibers and is molded by injection molding.

To manufacture long-fiber composites and ensure a good impregnation, starting from the monomer is the only way. This also brings into play the possibility to impregnate non-woven fabrics and move toward an increasingly green direction, since, in contrast to the fabric, there is the chance to create composites with recycled fibers (TNT) and a recyclable matrix.

2.2. Resin Film Infusion (RFI)

Fabrics already pre-impregnated by the mixture are used with inhibition of reactivity during the handling and storage phases. This is a film of resin superimposed on the fabric, generally referred to as thermosetting matrices, such as epoxy resin. The polymerization will take place through the application of heat and pressure (see **Figure 1c**) [34].

2.3. Vacuum Infusion

In a common vacuum infusion process for polymer composite [35] dry fiber fabrics are placed on a solid mold half, which defines the part geometry (see **Figure 1b**) [7][35][36][37][38][39][40]. Among the processes just described, vacuum infusion turns out to be one of the most effective techniques that allows treating high volumes with simpler and even cheaper equipment.

3. Thermoplastic Resin Transfer Molding (T-RTM)

In resin transfer molding (RTM), the reinforcing material is preplaced in the mold and impregnated with the matrix material by pressure or vacuum. This technology has made it possible to reduce manual work, but, despite this, the cycle time and, for most of the resins, the curing time are still long. Furthermore, the recycling of crosslinked matrix composites on an industrial scale is still in its infancy [41]. T-RTM was developed to overcome these problems. The technology is based on RTM, which was previously used for crosslinked composites, but, in this case, is used for reactive thermoplastic polymers. In reactive processing, polymerization takes place starting from monomers with the addition of an initiator and activator. Monomers have a low molecular mass, which leads them to have a viscosity similar to water, so they can easily impregnate the dry reinforcement material. During reactive processing, a chemical change occurs, but the result is a thermoplastic polymer without crosslinking [42].

High reinforcing fiber content can be achieved by this process, and no post-processing of the finished product is required [43].

References

1. Chen, K.; Jia, M.; Sun, H.; Xue, P. Thermoplastic reaction injection pultrusion for continuous glass fiber-reinforced poly amide-6 composites. *Materials* 2019, 12, 463.
2. Van Rijswijk, K.; Teuwen, J.J.E.; Bersee, H.E.N.; Beukers, A. Textile fiber-reinforced anionic polyamide-6 composites. Part I: The vacuum infusion process. *Compos. Part A Appl. Sci. Manuf.* 2009, 40, 1–10.
3. Novo, P.J.; Silva, J.F.; Nunes, J.P.; Marques, A.T. Pultrusion of fibre reinforced thermoplastic pre-impregnated materials. *Compos. Part B Eng.* 2016, 89, 328–339.
4. Silva, R.F.; Silva, J.F.; Nunes, J.P.; Bernardo, C.A.; Marques, A.T. New Powder Coating Equipment to Produce Continuous Fibre Thermoplastic Matrix Towpregs. *Mater. Sci. Fórum* 2008, 587, 246–250.
5. Angelov, I.; Wiedmer, S.; Evstatiev, M.; Friedrich, K.; Mennig, G. Pultrusion of a flax/polypropylene yarn. *Compos. Part A Appl. Sci. Manuf.* 2007, 38, 1431–1438.
6. Linganiso, L.Z.; Bezerra, R.; Bhat, S.; John, M.; Braeuning, R.; Anandjiwala, R.D. Pultrusion of flax/poly(lactic acid) commingled yarns and nonwoven fabrics. *J. Thermoplast. Compos. Mater.* 2014, 27, 1553–1572.
7. Van Rijswijk, K.; Bersee, H.E.N.; Jager, W.F.; Picken, S.J. Optimisation of Anionic Polyamide-6 for Vacuum Infusion of Thermoplastic Composites: Choice of Activator and Initiator. *Composites Part A: Applied Science and Manufacturing*; Elsevier Ltd.: Amsterdam, The Netherlands, 2006; Volume 37, pp. 949–956.
8. Van Rijswijk, K.; Bersee, H.E.N.; Beukers, A.; Picken, S.J.; van Geenen, A.A. Optimisation of anionic polyamide-6 for vacuum infusion of thermoplastic composites: Influence of polymerisation temperature on matrix properties. *Polym. Test.* 2006, 25, 392–404.
9. Luisier, A.; Bourban, P.E.; Manson, J.A.E. Reaction injection pultrusion of PA12 composites: Process and modelling. *Compos. Part A Appl. Sci. Manuf.* 2003, 34, 583–595.
10. Epple, S.; Bonten, C. Production of continuous fiber thermoplastic composites by in-situ pultrusion. *AIP Conf. Proc.* 2014, 454, 454–457.
11. Mateva, R.; Ishtinakova, O.; Nikolov, R.N.; Djambova, C.H. Kinetics of Polymerization of ϵ -Caprolactam in the Presence of Inorganic Dispersed Additives. *Eur. Polym. J.* 2018, 34, 1061–1067.
12. Te Nijenhuis, K.; Addink, R.; van der Vegt, A.K. A Study on Composites of Nylon-6 with Hollow Glass Microspheres. *Polym. Bull.* 1989, 21, 467–474.
13. Gabbert, J.D.; Hedrick, R.M.; Tierney, P.A. Reinforced Polymer Compositions; Monsanto Company: St. Louis, MO, USA, 1971.
14. Williams, G.T. Reinforced and foamed nyrim—An overview. *Eng. Plast.* 1992, 1, 48–52.

15. Van Rijswijk, K.; Bersee, H.E.N. Reactive processing of textile fiber-reinforced thermoplastic composites—An overview. *Compos. Part A Appl. Sci. Manuf.* 2007, 38, 666–681.
16. Parton, H.; Verpoest, I. In situ polymerization of thermoplastic composites based on cyclic oligomers. *Polym. Compos.* 2005, 26, 60–65.
17. Zingraff, L.; Bourban, P.E.; Wakeman, M.D.; Kohler, M.; Manson, J.A.E. Reactive processing and forming of polyamide 12 thermoplastic composites. In *Proceedings of the 23rd SAMPE Europe International Conference*, Paris, France, 9–11 April 2002.
18. Michaud, V.; Zingraff, L.; Verrey, J.; Bourban, P.E.; Manson, J.A.E. Resin transfer molding of anionically polymerized polyamide 12. In *Proceedings of the 7th International Conference on Flow Processes in Composite Materials (FPCM-7)*, Newark, DE, USA, 7–9 July 2004.
19. Zingraff, L.; Bourban, P.E.; Michaud, V.; Manson, J.A.E. Liquid composite moulding of anionically polymerised polyamide 12. In *Proceedings of the 14th International Conference on Composite Materials (ICCM-14)*, San Diego, CA, USA, 14–18 July 2003.
20. Verrey, J.; Michaud, V.; Manson, J.A.E. Complex Parts with Thermoplastic RTM Techniques. In *Proceedings of the 24th International SAMPE Europe Conference*, Paris, France, 1–3 April 2003.
21. Mairtin, P.; McDonnell, P.; Connor, M.T.; Eder, R.; O'Bradaigh, C.M. Process investigation of a liquid PA-12/carbon fibre moulding system. *Compos. Part A Appl. Sci. Manuf.* 2001, 32, 915–923.
22. Zingraff, L.; Michaud, V.; Bourban, P.E.; Manson, J.A. Resin transfer moulding of anionically polymerised polyamide 12. *Compos. Part A Appl. Sci. Manuf.* 2005, 36, 1675–1686.
23. Rosso, P.; Friedrich, K.; Wollny, A.; Mulhaupt, R. A novel polyamide 12 polymerization system and its use for a LCM-process to produce CFRP. *J. Thermoplast. Compos. Mater.* 2005, 18, 77–90.
24. Parton, H.; Baets, J.; Lipnik, P.; Devaux, J.; Verpoest, I. Liquid moulding of textile reinforced thermoplastics. In *Proceedings of the 11th European Conference on Composite Materials (ECCM-11)*, Rhodes, Greece, 31 May–3 June 2004.
25. Parton, H.; Verpoest, I. Reactive processing of textile reinforced thermoplastics. In *Proceedings of the 14th International Conference on Composite Materials (ICCM-14)*, San Diego, CA, USA, 14–18 July 2003.
26. Parton, H.; Verpoest, I. Thermoplastic liquid composite molding: Production and characterization of composites based on cyclic oligomers. In *Proceedings of the 7th International Conference on Flow Processes in Composite Materials (FPCM-7)*, Newark, NJ, USA, 7–9 July 2004.
27. Verrey, J.; Michaud, V.; Manson, J.A.E. Capillary effects in liquid composite moulding with non-crimp fabrics. In *Proceedings of the 14th International Conference on Composite Materials (ICCM-14)*, San Diego, CA, USA, 14–18 July 2003.
28. Weyrauch, F.; Stadtfeld, H.C.; Mitschang, P. Simulation and control of the LCM-process with future resin systems. In *Proceedings of the 7th International Conference on Flow Processes in Composite Materials (FPCM-7)*, Newark, DE, USA, 7–9 July 2004.
29. Otaigbe, J.U.; Harland, W.G. Studies in the properties of nylon 6-glass fiber composites. *J. Appl. Polym. Sci.* 1988, 36, 165–175.
30. Potter, K. *Resin Transfer Molding*; Chapman & Hall: London, UK, 1997.
31. Zhong, Y.; Liu, P.; Pei, Q.; Sorkin, V.; Louis Commillus, A.; Su, Z.; Guo, T.; Thitsartarn, W.; Lin, T.; He, C.; et al. Elastic properties of injection molded short glass fiber reinforced thermoplastic composites. *Compos. Struct.* 2020, 254, 112850.
32. Zainudin, E.S.; Sapuan, S.M.; Sulaiman, S. Fiber Orientation of Short Fiber Reinforced Injection Molded Thermoplastic Composites: A Review. *J. Inject. Molding Technol.* 2002, 6, 1–10.
33. Fu, S.Y.; Lauke, B.; Mader, E.; Hu, X.; Yue, C.Y. Fracture Resistance of Short-Glass-Fiber-Reinforced and Short-Carbon-Fiber-Reinforced Polypropylene under Charpy Impact Load and Its Dependence on Processing. *J. Mater. Process. Technol.* 1999, 89, 501–507.
34. Coll, S.; Murtagh, A.; O'Bradaigh, C. Resin film infusion of cyclic PBT composites consolidation analysis. In *Proceedings of the 7th International Conference on Flow Processes in Composite Materials (FPCM-7)*, Newark, DE, USA, 7–9 July 2004.
35. Pillay, S.; Vaidya, U.K.; Janowski, G.M. Liquid molding of carbon fabric-reinforced nylon matrix composite laminates. *J. Thermoplast. Compos. Mater.* 2005, 18, 509–527.
36. Van Rijswijk, K.; Koppes, K.; Bersee, H.E.N.; Beukers, A. Processing window for vacuum infusion of fiber-reinforced anionic polyamide-6. In *Proceedings of the 7th International Conference of Flow Processes in Composite Materials (FPCM-7)*, Newark, DE, USA, 7–9 July 2004.

37. Van Rijswijk, K.; Vlasveld, D.P.N.; Bersee, H.E.N.; Picken, S.J. Vacuum injection of anionic polyamide 6. In Proceedings of the 4th International Conference on Composite Structures and Technology (ICCST-4), Durban, South Africa, 21–23 January 2003.
38. Van Rijswijk, K.; Vlasveld, D.P.N.; van Rhijn, P.; Bersee, H.E.N.; Beukers, A.; Picken, S.J. Process considerations for liquid molding of composites based on anionic polyamide 6. In Proceedings of the 14th International Conference on Composite Materials (ICCM-14), San Diego, CA, USA, 14–18 July 2003.
39. Van Rijswijk, K.; Joncas, S.; Bersee, H.E.N.; Bergsma, O.K.; Beukers, A. Sustainable vacuum-infused thermoplastic composites for MW-size wind turbine blades—Preliminary design and manufacturing issues. *J. Sol. Energy Eng. Trans. ASME* 2005, 127, 570–580.
40. Kotelnikov, V.A.; Surin, N.N.; Cherepanov, S.G.; Persits, I.E.; Danilevskaya, L.B.; Konova, I.O.; Gavrilenko, V.V.; Chekulaeva, L.A. Synthesis of cross-linked nylon RIM block copolyamides. *Polym. Sci.* 1995, 37, 1198–1205.
41. Toldy, A. Recyclable-by-Design Thermoset Polymers and Composites. *Express Polym. Lett.* 2012, 15, 1113.
42. Kovács, Z.; Pomázi, Á.; Toldy, A. The flame retardancy of polyamide 6—Prepared by in situ polymerisation of ϵ -caprolactam—For T-RTM applications. *Polym. Degrad. Stab.* 2022, 195, 109797.
43. Pal, K. Új Technológiák Könnyűszerkezetes Autóelemek Gyártására. *Műsz. Feld.* 2014, 6. Available online: <https://quattroplast.hu/muanyagipariszemle/2014/06/uj-technologiak-konnyuszerkezetes-autoelemek-gyartasara-02.pdf> (accessed on 24 April 2022).

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